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FINAL REPORT

NASA GRANT: NSG-1414, Suppl. 2

THE DYNAMICS AND CONTROL OF LARGE  
FLEXIBLE SPACE STRUCTURES-III

PART A: SHAPE AND ORIENTATION CONTROL OF  
A PLATFORM IN ORBIT USING POINT  
ACTUATORS

(NASA-CR-163253) THE DYNAMICS AND CONTROL  
OF LARGE FLEXIBLE SPACE STRUCTURES, 3. PART  
A: SHAPE AND ORIENTATION CONTROL OF A  
PLATFORM IN ORBIT USING POINT ACTUATORS  
Final Report (Howard Univ.) 179 p

N80-27419

HC A09/MF A01

Unclass

G3/18 28005



HOWARD UNIVERSITY  
SCHOOL OF ENGINEERING  
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WASHINGTON, D.C. 20059

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THE DYNAMICS AND CONTROL OF LARGE  
FLEXIBLE SPACE STRUCTURES-III

PART A: SHAPE AND ORIENTATION CONTROL OF  
A PLATFORM IN ORBIT USING POINT  
ACTUATORS

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June 1980

## ABSTRACT

The dynamics and attitude and shape control of a large thin flexible square platform in orbit are studied. Attitude and shape control is assumed to result from actuators placed perpendicular to the main surface and one edge and their effect on the rigid body and elastic modes is modelled to first order. The equations of motion are linearized about three different nominal orientations: (1) the platform following the local vertical with its major surface perpendicular to the orbital plane; (2) the platform following the local horizontal with its major surface normal to the local vertical; and (3) the platform following the local vertical with its major surface perpendicular to the orbit normal. The stability of the uncontrolled system is investigated analytically. Once controllability is established for a set of actuator locations, control law development is based on decoupling, pole placement, and linear optimal control theory. Frequencies and elastic modal shape functions are obtained using a finite element computer algorithm and two different approximate analytical methods and the results of the three methods compared.



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## I. INTRODUCTION

The present grant represents a continuation of the effort attempted in the previous grant years (May 1977 - May 1979) and reported in Refs. 1 - 4\*. Attitude control techniques for the pointing and stabilization of very large, inherently flexible spacecraft systems are being investigated in this research. First the attitude dynamics and control of a long, homogeneous flexible beam whose center of mass is assumed to follow a circular orbit have been treated <sup>1,2</sup>. In the initial phase, first-order effects of gravity-gradient were included, whereas external perturbations and related orbital station keeping maneuvers were ignored. Three mathematical models describing the system's rotations and deflections within the orbital plane have been developed--one model, which treats the beam as a number of discretized mass particles connected by massless links<sup>1</sup>, and two continuum-type models.<sup>2,3</sup> The natural (uncontrolled) dynamics of this system have been simulated. The concept of distributed modal control<sup>1</sup>, which provides a means for controlling a particular system mode independently of all other modes, has been examined, along with other types of control laws including an application of optimal control theory and the use of decoupling techniques.<sup>3</sup> The effect of varying the number of modes in our model as well as the number and location of control devices has been examined, analytically, where possible, and numerically for general cases.<sup>3</sup>

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\*For references cited in this report please see list of references at the end of each chapter.

Towards the end of the second grant year the three dimensional model of a free-free plate in orbit was developed and a limited number of computer simulations of the uncontrolled dynamics in response to initial perturbations about a specific equilibrium orientation were performed.<sup>4</sup> Frequency values associated with the basic structural modes of a square plate were obtained from energy considerations based on approximate expressions developed by Warburton.<sup>5</sup> It was suggested at the final oral grant presentation that a comparison with results obtained using finite element methods and/or other analytical approaches should be examined to guarantee accuracy, particularly for higher order modes.

With this background and in accordance with our proposal to NASA dated January 25, 1979<sup>6</sup>, a plan of study was developed and has been extended to include the current grant year as outlined in Table I. The items indicated by a check mark have been completed by the end of the third grant year while those indicated by "IP" are currently in progress.

In this part of the 1979-80 final report (Part A) the control of an orbiting square shaped platform based on the continuum model of Ref. 2 with point actuators taken at selected locations on the platform surfaces is examined. A paper to be presented at the following conference forms the basis of Chapter II:

1980 AIAA/AAS Astrodynamics Conference, Danvers, Mass.,

Aug. 11-13, 1980 (only the contributions by A.S.S.R. Reddy,

P.M. Bainum, and R. Krishna are included here).

In Chapter III the results of two approximate analytical methods for predicting modal frequencies and modal shape functions are compared with the results obtained using a finite element computer algorithm using the homogeneous plate as an example.

TABLE I - STUDY PLAN 1977-1980

1. MODEL DEVELOPMENT

- ✓ A. Development of General Form of 3-Dimensional Equations for A Flexible Structure - Given the Modal Shape Functions
- ✓ B. Development of 3-Dimensional Equations of a Thin Homogenous Free-Free Beam
  - ✓ (1). The Case of No Longitudinal Vibrations: i.e.  $\phi_x^{(n)} = 0$
  - ✓ (2). The Case of No Yaw: i.e.  $\psi = 0$
- C. Determination of Modal Shape Functions and Frequencies for Different Structural Models
  - ✓ (1). Circular Homogenous Membrane
  - ✓ (2). Rectangular Homogenous Membrane
  - ✓ (3). Rectangular Homogenous Plate (and Square Plate)
  - ✓ (4). Circular Homogenous Plate
  - ✓ (5). Shallow Spherical Shell Structure
- D. Implementation of One or More of the Structural Models for Digital Simulation
  - ✓ (1). Rectangular Homogenous Plate
  - ✓ (2). Thin-Homogenous Beam with Stabilizing Dumbbell (Local Horizontal Orientation)
  - (3). Square Plate with Stabilizing Dumbbell (Local Horizontal Orientation)
  - ✓ (4). Shallow Spherical Shell Structure with Stabilizing Dumbbell
  - ✓ (5). Circular Homogenous Plate with Stabilizing Dumbbell
- IP E. Provide Equations in a Form Suitable for Control Implementation
  - ✓ - Items completed
  - IP - Items in progress

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## 2. CONTROL CONCEPTS - LARGE FLEXIBLE SPACE STRUCTURES

### A. Model Development

- ✓ (1). Concentrated on continuum model of large flexible beam in orbit (Santini and Howard University Formulation)
- ✓ (2). Modelled control devices as point actuators at specific locations along the beam
- (3). Modelling of control devices as point or distributed actuators for other large flexible systems
  - ✓ (a) Rectangular Homogenous Plate
  - (b) Circular Homogenous Plate
  - (c) Shallow Spherical Shell Structure

### B. Control Concepts:

- ✓ (1). Modal Control - considered with discretized beam model during 1977-78

For independent control of all modes (N) retained in the model, the number of actuators (P) must be equal to N ( $P=N$ )
- ✓ (2). Establish relationship between P and N according to controllability requirements (applications of theorems developed by Balas) P can be less than N. (Applied to continuum beam model 1978-79).
- ✓ (3). Selection of control system gains - considers both position and rate feedback. (Applied to continuum beam model 1978-79)
  - ✓ a. Develop criteria for complete decoupling of linearized controlled equations using the fundamental theorem of a system of N linear equations and P unknowns

For unique solution of gains,  $P=N$  consistent with modal control; for non unique solution  $P < N$
  - ✓ b. Application of linear regulator problem to the original linearized and/or transformed equations

IP (4) Application of control concepts to more complex structures

IP C. Modelling of Sensors-the Problem of Observability

D. Treatment of Observation and Control Spillover

✓ Items completed

IP Items in progress



References are given separately for each chapter; symbols used in Chapter II are defined either in the text or in Appendix A of Chapter II, while symbols used in Chapter III are defined in the text where used.

Chapter IV describes general conclusions together with recommendations for future work.

Part B of this report, under separate cover, concentrates on the mathematical modelling and analysis of more complex structures such as beams and plates with connected gimbaled dumbbells to provide gravitational stability about the local horizontal orientation, and also the analysis of the dynamics of a shallow shell-type structure in orbit.

## I.1 References - Introduction

1. Bainum P.M. and Sellappan, R., "The Dynamics and Control of Large Flexible Space Structures," Final Report NASA Grant: NSG-1414, Part A: Discrete Model and Modal Control, Howard University, May 1978.
2. Bainum Peter M., Kumar, V.K., and James, Paul K., "The Dynamics and Control of Large Flexible Space Structures," Final Report, NASA Grant: NSG-1414. Part B: Development of Continuum Model and Computer Simulation, Howard University, May 1978.
3. Bainum, P.M. and Reddy, A.S.S.R., "The Dynamics and Control of Large Space Structures II," Final Report, NASA Grant NSG-1414, Suppl. 1, Part A: Shape and Orientation Control Using Point Actuators, Howard University, June 1979.
4. Bainum, P.M., James P.K., Krishna, R., and Kumar, V.K., "The Dynamics and Control of Large Flexible Space Structures II" Final Report, NASA Grant NSG-1414, Suppl. 1., Part B: Model Development and Computer Simulation, Howard University, June 1979.
5. Warburton, G.B., "The Vibration of Rectangular Plates," Proc. Institute of Mechanical Engineers, Vol. 168, No. 12, 1954, pp. 371-394.
6. Bainum, P.M., "Proposal for Research Grant on: The Dynamics and Control of Large Flexible Space Structures-III," Howard University, (Submitted to NASA), Jan. 25, 1979.

## II. CONTROL OF A LARGE FLEXIBLE PLATE IN ORBIT

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### Abstract

The dynamics and attitude and shape control of a large thin flexible platform in orbit are studied. Attitude and shape control is assumed to result from actuators placed perpendicular to the main surface and one edge and their effect on the rigid body and elastic modes is modeled to first order. The equations of motion are linearized about nominal orientations where the undeformed plate follows either the local vertical or local horizontal. The stability of the uncontrolled system is investigated analytically. Once controllability is established for a set of actuator locations, control law development is based on pole placement, decoupling, and linear optimal control theory.

### 1. Introduction

Large, flexible spacecraft systems have been proposed for future applications in widespread communications, electronic orbitally based mail systems, and as possible collectors of solar energy for transmittal to earth-based receiving stations.<sup>1,2</sup> For such missions the size of the orbiting system may be several times larger than that of the earth-based receiving station(s), and both orientation and shape control of the orbiting system will be required.

In order to gain insight into the dynamics of such a large flexible system the equations of motion of a long, flexible free-free beam in orbit were developed<sup>3</sup> using a slightly modified version of the general formulation of the dynamics of a general flexible orbiting body formulated by Santini.<sup>4</sup> This specific example considered only the inplane rotations and deformations of the uncontrolled beam and demonstrated the possibility of instability for very small values of the ratio of the fundamental flexural frequency to the orbit angular velocity. Two related papers treated the modeling of point actuators located at specific points along the beam with the associated criteria for controllability<sup>5</sup> and also the problem of selecting control law feedback gains based on decoupling techniques and application of the linear regulator problem.<sup>6</sup> Also included were numerical results showing the effects of control spillover on the uncontrolled modes when the number of controllers is less than the number of modes in the model, and the effects of inaccurate knowledge of

the control influence coefficients which lead to errors in the calculated feedback gains.<sup>6</sup>

In the present paper the two dimensional model considered in Refs. 3, 5, and 6 is extended to three dimensions by developing the equations of motion for a large flexible rectangular plate (platform) in orbit. These equations include three rigid body equations plus the generic mode elastic equations.

### 2. Model Development

In the present paper three different nominal orientations of the platform in orbit are assumed about which attitude and shape control are to be achieved. These are:

- Case (i) the platform following the local vertical with its larger surface perpendicular to the plane of the orbit (Fig. 1a);
- Case (ii) the platform following the local horizontal with its larger surface area normal to the local vertical (Fig. 1b);
- Case (iii) the platform following the local vertical with its larger surface perpendicular to the orbit normal (Fig. 1c).

From the general formulation of Refs. 3 and 4, the equations of motion of the structure are obtained:

#### A. Rotational Equations of Motion:

$$\begin{aligned}\ddot{\omega}_x &= \frac{I_y - I_z}{I_x} \omega_y \omega_z + \frac{G_x}{I_x} + \frac{T_x}{I_x} + \frac{C_x}{I_x} \\ \ddot{\omega}_y &= \frac{I_z - I_x}{I_y} \omega_x \omega_z + \frac{G_y}{I_y} + \frac{T_y}{I_y} + \frac{C_y}{I_y} \\ \ddot{\omega}_z &= \frac{I_x - I_y}{I_z} \omega_x \omega_y + \frac{G_z}{I_z} + \frac{T_z}{I_z} + \frac{C_z}{I_z}\end{aligned}\quad (1)$$

Using Euler angles to represent rigid body orientations relative to the local vertical (horizontal) system, the transformation from Euler angular rates to body rates is given by:

$$\begin{aligned}\omega_x &= \dot{\psi} + (\dot{\theta} + \omega_c) \sin\theta \\ \omega_y &= (\dot{\theta} + \omega_c) \cos\theta \cos\psi + \dot{\phi} \sin\psi \\ \omega_z &= \dot{\phi} \cos\psi - (\dot{\theta} + \omega_c) \sin\theta \cos\psi\end{aligned}\quad (2)$$

(Note: Symbols used are defined in Appendix A.)

$G_{\bar{x}}, G_{\bar{y}}, G_{\bar{z}}$  represent the gravity-gradient torques about the principal undeformed body axes and can be evaluated as:

$$\begin{aligned} G_{\bar{x}} &= 3\omega_c^2(I_x - I_y)(-c\psi s\theta + s\psi c\theta)(s\psi s\theta + c\psi c\theta) \\ G_{\bar{y}} &= 3\omega_c^2(I_x - I_z)(s\psi s\theta + c\psi c\theta)c\theta c\phi \\ G_{\bar{z}} &= 3\omega_c^2(I_y - I_z)(-c\psi s\theta + s\psi c\theta)c\theta c\phi \end{aligned} \quad (3)$$

where  $s(\cdot) = \sin(\cdot)$  and  $c(\cdot) = \cos(\cdot)$ .

### B. Generic Mode Equations

The generic modal equations may be obtained for each of the three nominal orientations considered in terms of the modal amplitude  $(A_r)^{3,4}$

#### For Case (i)

$$\ddot{A}_r + [\omega_r^2 - (\omega_x^2 + \omega_y^2) - M_{xx}] A_r = E_r/M_r \quad (4a)$$

where

$$M_{xx} = \omega_c^2 [3(s^2\psi s^2\theta + c^2\psi s^2\theta + 2s\psi s\theta c\theta c\psi s\theta) - 1]$$

#### For Case (ii)

$$\ddot{A}_r + [\omega_r^2 - (\omega_x^2 + \omega_z^2) - M_{xx}] A_r = E_r/M_r \quad (4b)$$

where

$$M_{xx} = \omega_c^2 [3c^2\theta c^2\phi - 1]$$

#### For Case (iii)

$$\ddot{A}_r + [\omega_r^2 - (\omega_x^2 + \omega_z^2) - M_{yy}] A_r = E_r/M_r \quad (4c)$$

where

$$M_{yy} = \omega_c^2 [3(c^2\psi s^2\theta + s^2\psi s^2\theta - 2c\psi s\theta c\psi s\theta) - 1]$$

### C. Linearization

With the assumption of small amplitudes, the rotational equations of motion given by Eq. (1) become:

$$\begin{aligned} \ddot{\psi} &= \omega_c^2 \left[ \frac{I_y - I_z}{I_x} - 1 \right] \psi - \omega_c^2 \left( \frac{I_y - I_z}{I_x} \right) \psi + \frac{T_x}{I_x} + \frac{C_x}{I_x} \\ \ddot{\phi} &= \omega_c^2 \left[ \frac{I_x - I_z}{I_z} + 1 \right] \phi + 4\omega_c^2 \left( \frac{I_x - I_z}{I_z} \right) \phi + \frac{T_z}{I_z} + \frac{C_z}{I_z} \\ \ddot{\theta} &= 3\omega_c^2 \left( \frac{I_x - I_z}{I_y} \right) \theta + \frac{T_y}{I_y} + \frac{C_y}{I_y} \end{aligned} \quad (5)$$

For the present analysis, the platform is assumed to be square, thin and homogeneous, such that the following relationships among the principal moments of inertia are valid:

$$\begin{aligned} \text{Case (i): } I_x &= I_y \text{ and } I_z = 2I_x = 2I_y \\ \text{Case (ii): } I_y &= I_z \text{ and } I_x = 2I_y = 2I_z \\ \text{Case (iii): } I_x &= I_z \text{ and } I_y = 2I_x = 2I_z \end{aligned} \quad (6)$$

For small amplitude angles the generic mode equations become:

$$\begin{aligned} \text{Case (i): } \ddot{A}_r + \omega_r^2 A_r &= E_r/M_r \\ \text{Case (ii): } \ddot{A}_r + (\omega_r^2 - 3\omega_c^2) A_r &= E_r/M_r \end{aligned} \quad (7)$$

$$\text{Case (iii): } \ddot{A}_r + (\omega_r^2 - \omega_c^2) A_r = E_r/M_r$$

### D. Modelling of Point Actuators

For an actuator which can generate a force of the type

$$\vec{F} = f_x \hat{i} + f_y \hat{j} + f_z \hat{k} \quad (8)$$

and placed at a location  $(x, y, z)$ , the resultant control torque is given by

$$\vec{T} = \vec{r} \times \vec{F} \quad (9)$$

where  $\vec{r} = x\hat{i} + y\hat{j} + z\hat{k}$  describes the position of the actuator on the surface (or edge) of the plate. Actuators can be placed perpendicular to the XY, YZ or XZ planes of the plate, so for an actuator whose force axis is perpendicular to the XY plane the torque is given by (since  $f_x = f_y = 0$ )

$$\vec{T} = y f_z \hat{i} - x f_z \hat{j} \quad (10)$$

For an actuator whose force axis is perpendicular to the YZ plane, the torque is given by (since  $f_y = f_z = 0$ )

$$\vec{T} = x f_x \hat{j} - y f_x \hat{k} \quad (11)$$

For an actuator perpendicular to the XZ plane, the torque is given by (since  $f_x = f_z = 0$ ).

$$\vec{T} = -x f_y \hat{i} + y f_y \hat{k} \quad (12)$$

The generic force due to the  $i$ th actuator on the  $r$ th mode is given by<sup>3,4</sup>

$$\begin{aligned} E_r &= \iint W_r(x, y) \hat{k} \cdot \delta(x - x_i, y - y_i) f_i(t) \hat{k} dx dy \\ &= W_r(x_i, y_i) f_i(t) \end{aligned} \quad (13)$$

where  $W_r(x, y)$  is the  $r$ th modal (spatial) function of the deformed plate with vibrations assumed to occur along the Z direction, whose amplitudes are assumed to be much smaller than a characteristic plate length.

For  $n$  actuators placed on the XY plane of the plate with force axes normal to that deformed surface, the generic force on  $r$ th mode is given by

$$E_r = \sum_{i=1}^n W_r(x_i, y_i) f_i \quad (14)$$

where  $x_i, y_i$  are the coordinates of the  $i$ th actuator. An actuator placed normal to the XY plane won't produce a torque about the Z-axis; in order to obtain a direct torque about the Z-axis, actuators may have to be located on the other surfaces (edges) of the plate.

### E. Modelling of Distributed Actuators

If the force is distributed along the surfaces of the plate, the force can be represented by

$$\begin{aligned} \vec{F} &= f_x(x, y, z, t) \hat{i} + f_y(x, y, z, t) \hat{j} \\ &+ f_z(x, y, z, t) \hat{k} \end{aligned} \quad (15)$$

where the force components are now both spatially and time dependent.

The torque due to such an actuator is given by

$$\bar{T} = \bar{R}x\bar{f} \quad (16)$$

The total torque is given by

$$\bar{T} = \int (\bar{R}x\bar{f}) dx dy dz \quad (17)$$

Using series expansions and separation of variables between spatially and time dependent functions, one can very accurately represent (e.g. for the x component),

$$f_x(x, y, z, t) = \sum_{n=1}^L f_{x_n}(x, y, z) g_{x_n}(t) \quad (18)$$

The integral for the torque is then given by

$$T = \int \left[ \sum_{i=1}^N y f_{z_i}(x, y, z) g_{z_i}(t) - \sum_{m=1}^M z f_{y_m}(x, y, z) g_{y_m}(t) + \sum_{n=1}^L x f_{x_n}(x, y, z) g_{x_n}(t) - \sum_{l=1}^L x f_{z_l}(x, y, z) g_{z_l}(t) \right] dx dy dz \quad (19)$$

The resulting generic force is then obtained in the same manner as in Eq. (13) with the result,

$$F_x = \int [W_x(x, y)] \left[ \sum_{i=1}^N f_{z_i}(x, y, z) g_{z_i}(t) \right] dx dy dz \quad (20)$$

### 3. Uncontrolled Motion-Numerical Example

The platform is assumed to have the following physical properties:

$$a = 100 \text{ m} \quad (\text{side of square plate})$$

$$M = 276800 \text{ kg}$$

$$\text{Minimum Moment of Inertia} = 2.354 \times 10^7 \text{ kg-m}^2$$

$$\text{Maximum Moment of Inertia} = 4.7088 \times 10^7 \text{ kg-m}^2$$

For an assumed orbital altitude of 250 n.mi. (circular)

$$\omega_c = 1.25 \times 10^{-3} \text{ rad/sec.}$$

The modal frequencies of the elastic modes have been obtained using a finite element computer algorithm.<sup>7</sup> For the first three flexible modes:

$$\omega_1 = 2.0931947 \times 10^{-2} \text{ rad/sec}$$

$$\omega_2 = 3.0404741 \times 10^{-2} \text{ rad/sec}$$

$$\omega_3 = 3.9088122 \times 10^{-2} \text{ rad/sec}$$

The uncontrolled motion of the linear system through small amplitude deviations with respect to each of the three nominal orientations will now be considered.

$$\text{Case (i): } I_x = I_y, I_z = 2I_x = 2I_y$$

The rotational equations of motion and the generic modal equations are non-dimensionalized by the orbital period and the length variable ( $\tau = \omega_c t$ ,  $Z_r = A_r/a$ ,  $\phi' = d\phi/d\tau$ , etc)

$$\psi'' = [(I_y - I_z - I_x)/\omega_c I_x] \phi' - [(I_y - I_z)/I_x] \psi \quad (21)$$

$$\phi'' = [(I_x - I_y + I_z)/\omega_c I_z] \psi' + [(I_x - I_y)/I_z] \phi \quad (22)$$

$$\theta'' = 3\theta \quad (23)$$

The generic mode equations become:

$$Z_r'' = -(\omega_r/\omega_c)^2 Z_r \quad (24)$$

The pitch and the generic mode equations are decoupled from roll and yaw. The pitch and generic modes exhibit simple harmonic motions. After substituting inertia values into the roll and yaw equations,

$$\psi'' = -(2/\omega_c) \phi' + \phi \quad (25)$$

$$\phi'' = \psi'/\omega_c \quad (26)$$

The characteristic equation for the system (25) and (26) is,  $s^2(s^2 - 1 + 2/\omega_c^2) = 0$

It can be seen that the roll and yaw motion has a double pole at the origin and thus the uncontrolled roll/yaw motion is unstable. The analytical solution is obtained using Laplace transform techniques. A typical response for initial perturbations in both roll and yaw rate(s) is shown in Fig. 2.

$$\text{Case (ii): } I_y = I_z \text{ and } I_x = 2I_y$$

The rotational equations of motion are

$$\psi'' = -(1/\omega_c) \phi' \quad (27)$$

$$\phi'' = (2/\omega_c) \psi' + \phi \quad (28)$$

$$\theta'' = 3\theta \quad (29)$$

The generic mode equations can be represented by,

$$Z_r'' = -[(\omega_r/\omega_c)^2 - 3] Z_r \quad (30)$$

From Eq. (29) the pitch amplitude increases exponentially in response to an initial displacement, whereas from Eq. (30), for  $\omega_r/\omega_c > \sqrt{3}$  the generic modal amplitudes exhibit simple harmonic motion.

The characteristic equation for the combined roll/yaw motion is:

$$s^2(s^2 - 4 + 2/\omega_c^2) = 0 \quad (31)$$

The roll/yaw motion is characterized by a double pole at the origin and is thus unstable.

$$\text{Case (iii): } I_x = I_z \text{ and } I_y = 2I_x = 2I_z$$

The rotational equations of motion are

$$\psi'' = -\psi; \phi'' = -4\phi; \theta'' = 0 \quad (32)$$

while the generic mode equations can be expressed by,

$$Z_r'' = -[(\omega_r/\omega_c)^2 - 1] Z_r \quad (33)$$

In this case, roll, yaw, pitch and the generic modes are decoupled from each other. The generic modes, roll and yaw exhibit simple harmonic motion, while the pitch amplitude increases linearly with time for a given initial pitch rate.

#### 4. Controlled Motion

The rotational equations of motion are combined with the generic modal equations using the nondimensional orbital time and length variables and then recast into conventional state space form:

$$\dot{X}' = AX + BU \quad (34)$$

where the state vector,  $X$ , is defined as

$$X = (x_1, x_2, x_3, \dots, x_{1+3}, \dots, x_{n+6+1}, \dots, x_{2n+6})^T$$

and

$$x_1 = \phi; x_2 = \psi; x_3 = \theta; x_{1+3} = \dot{\phi}; x_{2+3} = \dot{\psi}; x_{3+3} = \dot{\theta};$$

$$i = 1, 2, \dots, n \text{ generic modes}$$

$$x_{n+6} = \phi'; x_{n+5} = \psi'; x_{n+6} = \theta'$$

$$x_{n+6+1} = \dot{\phi}' = \dot{\phi}_{1+3}, i = 1, 2, \dots, n$$

For the examples to be considered in this paper it is assumed that the system can be modelled by three rigid body rotational modes and the first three generic (flexible) modes.

The general A matrix

$$[A] = \begin{bmatrix} \text{6x6} & \begin{bmatrix} 1 \\ 1 \end{bmatrix} \\ \text{diagonal} & \begin{bmatrix} 0 & \Lambda_{78} & \dots & 0 \\ \Lambda_{78} & 0 & \dots & 0 \\ 0 & 0 & \dots & 0 \end{bmatrix} \\ \Lambda & \end{bmatrix} \quad (35)$$

The non-zero and non-unity elements appearing in A are;

$$\Lambda_{7,1} = 4(I_x - I_y)/I_z; \Lambda_{8,2} = -(I_y - I_z)/I_x;$$

$$\Lambda_{9,3} = 3(I_x - I_z)/I_y; \Lambda_{10,4} = -(\omega_1/\omega_c)^2;$$

$$\Lambda_{11,5} = (\omega_2/\omega_c)^2; \Lambda_{12,6} = -(\omega_3/\omega_c)^2;$$

$$\Lambda_{8,7} = (I_y - I_z - I_x)/\omega_c I_x; \Lambda_{7,8} = (I_x - I_y + I_z)/\omega_c I_z$$

The general B matrix:

$$B = \begin{bmatrix} O_{6 \times 6} \\ B_{6 \times 6} \end{bmatrix}$$

where the lower part of the B matrix depends on actuator locations.

#### Control Law Selection

Control laws are developed using 3 different techniques. They are: (a) decoupling of the original state equations using state variable feedback; (b) stabilizing the system by clustering the poles on a line parallel to the imaginary axis and in the negative s-plane using the control law of the type  $U = -KX$ ; (c) applying the linear regular theory to the original system equations;

#### (a) Decoupling of Original State Equations Using State Variable Feedback

The equations of motion of the platform can be written as

$$\ddot{X} = A\dot{X} + CX + BU \quad (36)$$

where  $X = (x_1, x_2, \dots, x_{n+3})$

After selecting  $U = K_p \dot{X} + K_d X$  we can rewrite the controlled motion equations as

$$\ddot{X} = (A + BK_p)\dot{X} + (C + BK_d)X \quad (37)$$

$K_p$  and  $K_d$  are evaluated such that  $(A + BK_p)$  and  $(C + BK_d)$  are diagonalized and thus yield required damping and frequency of the controlled modes. The number of modes must be equal to the number of actuators to avoid the use of pseudo-inverse matrices.

Two sets of actuator locations have been assumed for each of the three nominal orientations previously described. For all orientations, (i)-(iii), it is assumed that five actuators are located on the larger surface (with force axis normal to it) and a sixth actuator along an edge. The body coordinates of the six actuators are taken as

Case (i)

First Location  $a = 100m$

$$x_1(-a/6, -a/6, 0); x_2(a/6, -a/6, 0); x_3(-a/6, 0, 0)$$

$$x_4(a/6, 0, 0); x_5(-a/6, a/6, 0); x_6(a/2, a/6, 0)$$

Second Location  $a = 100m$

$$x_1(-a/2, -a/2, 0); x_2(a/2, -a/2, 0); x_3(-a/2, a/2, 0)$$

$$x_4(a/2, a/2, 0); x_5(-a/2, 0, 0); x_6(a/2, a/2, 0)$$

Case (ii)

First Location  $a = 100m$

$$x_1(0, -a/6, -a/6); x_2(0, -a/6, a/6); x_3(0, 0, -a/6)$$

$$x_4(0, 0, a/6); x_5(0, a/6, -a/6); x_6(0, a/6, a/2)$$

Second Location  $a = 100m$

$$x_1(0, -a/2, -a/2); x_2(0, -a/2, a/2); x_3(0, a/2, -a/2)$$

$$x_4(0, a/2, a/2); x_5(0, 0, -a/2); x_6(0, a/2, a/2)$$

Case (iii)

First Location  $a = 100m$

$$x_1(-a/6, 0, -a/6); x_2(-a/6, 0, a/6); x_3(0, 0, -a/6)$$

$$x_4(0, 0, a/6); x_5(a/6, 0, -a/6); x_6(a/6, 0, a/2)$$

Second Location  $a = 100m$

$$x_1(-a/2, 0, -a/2); x_2(-a/2, 0, a/2); x_3(a/2, 0, -a/2)$$

$$x_4(a/2, 0, a/2); x_5(0, 0, -a/2); x_6(a/2, 0, a/2)$$

Actuator positions for the two different sets of locations are illustrated in Fig. 3. The system A and B matrices corresponding to different combinations of the three platform orientations and the two sets of actuator location are listed as follows.

Case (i) Platform Following Local Vertical  
With Major Surface Normal to the Orbit Plane.

The non zero elements of the A matrix are:

$$\begin{aligned} A_{1,1+6} &= 1 \text{ for } i = 1, \dots, 6; A_{7,8} = 800; \\ A_{8,7} &= -1600; A_{8,2} = 1; A_{9,3} = -3; \\ A_{10,4} &= -277.414, A_{11,5} = -588.647; \\ A_{12,6} &= -976.844 \end{aligned}$$

Location I (Lower Part of B matrix)

0.0	0.0	0.0	0.0	0.0	-0.22643
-0.4329	-0.4329	0.0	0.0	0.4329	0.0
0.4329	-0.4329	0.4329	-0.4329	0.4329	0.0
-0.003126	-0.003126	0.0	0.0	-0.003126	0.0
0.0	0.0	-0.003084	-0.003084	0.0	0.0
-0.008786	-0.008786	-0.0115	-0.0115	-0.008786	0.0

Location II (Lower Part of B matrix)

0	0	0	0	0	-0.6796
-1.3592	-1.3592	1.3592	1.3592	0	0.0
1.3592	-1.3592	1.3592	-1.3592	1.3592	0.0
0.023	-0.023	-0.023	0.023	0.0	0.0
0.0	0.0	0.0	0.0	-0.023	0.0
0.023	0.023	0.023	0.023	0.023	0.0

Case (ii) Platform Along Local Horizontal

The elements of the A matrix that are different from Case (ii) are:

$$\begin{aligned} A_{7,1} &= 4; A_{7,8} = 1600; A_{8,2} = 0; A_{8,7} = -800; \\ A_{9,3} &= 3. \end{aligned}$$

Location I (Lower Part of B matrix)

0.4329	0.4329	0.0	0.0	-0.4329	0.0
0.0	0.0	0.0	0.0	0.0	0.22643
-0.4329	0.4329	-0.4329	0.4329	-0.4329	0.0
0.003126	-0.003126	0.0	0.0	-0.003126	0.0
0.0	0.0	-0.003084	-0.003084	0.0	0.0
-0.008786	-0.008786	-0.0115	-0.0115	-0.008786	0.0

Location II (Lower Part of B matrix)

1.3592	1.3592	-1.3592	-1.3592	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.6796
-1.3592	1.3592	-1.3592	1.3592	-1.3592	0.0
0.023	-0.023	-0.023	0.023	0.0	0.0
0	0.0	0.0	0.0	-0.023	0.0
0.023	0.023	0.023	0.023	0.023	0.0

Case (iii) Major Surface in Orbit Plane

The elements of the A matrix that are different from Case (ii) are:

$$\begin{aligned} A_{7,1} &= -4; A_{7,8} = 0; A_{8,2} = -1; A_{8,7} = 0; \\ A_{9,3} &= 0. \end{aligned}$$

Location I (Lower Part of B matrix)

-0.4329	-0.4329	0.0	0.0	0.4329	0.0
0.4329	-0.4329	-0.4329	-0.4329	0.4329	0.0
0.0	0.0	0.0	0.0	0.0	-0.22643
-0.003126	-0.003126	0.0	0.0	-0.003126	0.0
0.0	0.0	-0.003084	-0.003084	0.0	0.0
-0.008786	-0.008786	-0.0115	-0.0115	-0.008786	0.0

Location II (Lower Part of B matrix)

-1.3592	-1.3592	1.3592	1.3592	0.0	0.0
1.3592	-1.3592	1.3592	-1.3592	1.3592	0.0
0.0	0.0	0.0	0.0	0.0	-0.6796
0.023	-0.023	-0.023	0.023	0.0	0.0
0.0	0.0	0.0	0.0	-0.023	0.0
0.023	0.023	0.023	0.023	0.023	0.0

For all combinations considered above the gains are selected so as to produce 20% of critical damping in each of the rigid body modes and the first generic mode, and 10% of critical damping in the second and third generic modes. In order to provide a better transient response in the lower frequency fundamental elastic mode, the percentage of critical damping is selected to be twice that in the remaining flexible modes. The time response of the rigid body modes and the generic modal amplitudes for all combinations considered and for equal initial position displacements in all components of the state is illustrated in Fig. 4a.

As an example of the time history of the required control forces, Fig. 4b. shows such a time response for the exterior (II nd) location of the actuators with the platform nominally following the local vertical and the major surface area of the platform in the orbital plane. A complete summary of the maximum force amplitudes required for all combinations of actuator locations and platform orientations is given in Table I. In interpreting the results of Table I, it should be pointed out that, in the process of achieving both orientation and shape control, the maximum force(s) required of any actuator will vary with both the moment arm about the principal body axes and the value of the modal shape function at the particular actuator location for all modes contained within the mathematical model.

(b) Stabilizing the System by Pole Clustering

The equations of motion of the platform when recast in state space format can be written as

$$\dot{X} = AX + BU \quad (38), \quad X \rightarrow 2(n+3)x_1$$

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Table 1 Maximum Force Amplitudes (Newtons) for Different Combinations of Cases with Actuator Locations

Force	Location I (interior)			Location II (exterior)			
	Case 1	Case 11	Case 111	Case 1	Case 11	Case 111	
$f_1$	-807.8	270.63	270.6	57.6	62.56	47.4	Indicates maximum level of control force required for each case.
$f_2$	270.0	136.2	-133.3	28.19	26.20	-17.2	
$f_3$	<u>1141.0</u>	<u>387.3</u>	<u>-425.0</u>	-65.89	-49.5	30.0	
$f_4$	527.9	195.6	163.7	17.10	-30.90	25.08	
$f_5$	489.09	-253.3	153.0	-44.6	-44.67	-44.67	
$f_6$	-264.58	-272.0	4.4	<u>88.16</u>	<u>-88.06</u>	1.47	

The control,  $U = -KX$  is selected by using a digital computer algorithm<sup>8</sup> such that  $(A-BK)$  has the required identical negative real part in each of its eigenvalues. Although the number of actuators can be less than the number of modes (one half of the dimensionality of the state vector), a limitation of this algorithm is that the gains are selected such that all of the closed-loop poles lie on a line parallel to the imaginary axis. However this algorithm is useful when it is important that each mode in the system satisfy some minimum damping characteristics.

As an example of this technique we consider the system with four actuators and six modes where control about the first orientation (Case 1) is desired. Three of the actuators are assumed to provide forces perpendicular to the major surface with the remaining actuator thrusting normal to an edge. The actuator coordinates in the body system (Fig. 1a) are:  $f_1(-a/6, -a/6, 0)$ ;  $f_2(a/6, -a/6, 0)$ ;  $f_3(-a/6, 0, 0)$ ; and  $f_4(a/2, a/6, 0)$  where  $a = 100m$ . It is assumed that the minimum damping requirement on the system has a time constant of (13.33 min or  $(1/2\pi)$  dimensional orbital time). The control influence matrix is then calculated based on the assumed coordinates of the four actuators. The control  $U = -KX$  can be calculated by the ORACLS pole clustering algorithm. Based on these gains time histories of the required control forces are then obtained.

The control influence matrix (lower part), closed loop poles, and maximum force amplitudes required are summarized as follows:

B matrix (Lower Part)

0.0	0.0	0.0	-0.22645
-0.4529	-0.4529	0.0	0.0
0.4529	-0.4529	0.0	0.0
0.003126	-0.003126	0.0	0.0
0.0	0.0	-0.0030844	0.0
-0.008786	-0.008786	-0.0115	0.0

Closed Loop Poles (Nondimensionalized)

The real part is -1.0 and the imaginary parts are +0.000485, +0.993, +16.82, +24.26, +31.33 and +1131.37. The Maximum force amplitudes (Newtons) are calculated as

$$|f_1| = 78.5, |f_2| = 36.4, |f_3| = 169.5, \text{ and } |f_4| = 35.3.$$

An interesting comparison can now be made between this result and that shown in Table I for case (1) and the first (I) location of the six actuators considered there. It can be seen that by using fewer actuators, appropriately placed, that better transient response characteristics can be obtained with smaller maximum force amplitudes. However a disadvantage of this method is that some of the controlled frequencies may be orders of magnitude greater than the highest frequency of the uncontrolled system (for this example compare 1131 with  $\sqrt{976} = 31.24$ ). Depending on the nature of the expected disturbance forces this result could be very undesirable.

(c) Application of the Linear Regulator Theory

The control law,  $U = -KX$ , is selected such that the following performance index is minimized

$$J = \int_0^{\infty} (X^T Q X + U^T R U) dt \quad (39)$$

where  $Q$  and  $R$  are positive definite penalty matrices. The steady state solution of the matrix Riccati equation of dimension equal to the state has to be solved in order to evaluate the gain matrix,  $K$ .

A computer algorithm within the ORACLS<sup>8</sup> software package is used to obtain the gain matrices  $K$  for different combinations of the  $Q$  and  $R$  penalty matrices. This algorithm utilizes the Newton Raphson method of solving the Riccati equation. In the examples considered here four actuators are assumed with the system represented by three rigid body and three flexible modes. The locations of the four actuators are taken to be the same as in Section (b), and control about the first nominal orientation (1) is considered.

The weighting matrix,  $Q$ , is selected based on the following considerations. For the example considered here it can be seen from Eq. (34), (35), and the B matrix that the uncontrolled system dynamics is either described by sets of uncoupled harmonic oscillators, or (in the case of roll/yaw motion) by a coupled two dimensional harmonic oscillator. The latter motion can be represented by

$$\begin{bmatrix} \ddot{w}_z \\ \ddot{w}_x \end{bmatrix} = \begin{bmatrix} 0 & a \\ -b & 0 \end{bmatrix} \begin{bmatrix} w_z \\ w_x \end{bmatrix} \quad (40)$$

where the system oscillates at the frequency  $\Omega = \sqrt{ab}$ . It is desired that the control remove a maximum "transverse" angular rate,  $\dot{w}_{\text{max}}$  =  $\max \sqrt{\dot{w}_z^2 + \dot{w}_x^2} = \sqrt{\dot{w}_z^2(0) + \dot{w}_x^2(0)}$



so that a strategy for selecting the elements of  $Q$  could be<sup>9,10</sup>

$$Q = \begin{bmatrix} f & 0 \\ 0 & f \end{bmatrix} \quad \text{where } f = \Omega^2/\omega_T^2 \quad (41)$$

when the control penalty matrix is fixed. The remaining equations for any of the uncoupled oscillators can also be expressed by

$$\begin{bmatrix} \ddot{z}_1 \\ \ddot{z}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -(\omega_1/\omega_c)^2 & 0 \end{bmatrix} \begin{bmatrix} z_1 \\ z_2 \end{bmatrix} \quad (42)$$

in the same format as Eq. (39), and thus the weights can be obtained in a similar manner.

The  $Q$  matrix for the case considered here (control about nominal orientation (1) with actuator locations as given in Section (b)) is obtained using the relations given by Eq. (41) and is a diagonal matrix,  $Q_0$ , with the following elements:

$$\begin{aligned} Q_{1,1} &= 4.324 \times 10^9, \quad Q_{2,2} = 8.539 \times 10^9, \\ Q_{3,3} &= Q_{9,9} = 3.0 \times 10^4, \quad Q_{4,4} = Q_{10,10} = \\ &2.77414 \times 10^6, \quad Q_{5,5} = Q_{11,11} = 5.88647 \times 10^6, \\ Q_{6,6} &= Q_{12,12} = 9.74844 \times 10^6, \quad Q_{7,7} = Q_{8,8} = \\ &2.222 \times 10^3. \end{aligned}$$

The  $R_0$  matrix is chosen as an identity matrix. A parametric study is done using various multiples of the  $Q_0$  ( $Q = \alpha Q_0$ ) and  $R_0$  matrices obtained above which are plotted against the negative real part of the least damped mode of the controlled system in Fig. 5. All the loci of the negative real part of the least damped mode approach unity and no significant improvement is observed by increasing the state penalty,  $Q = \alpha Q_0$ , any further. Thus one wishes to operate on the horizontal line between the points (1) and (2). The maximum amplitude of the forces for  $R = I$  and  $R = 1000 I$  are calculated and plotted in Fig. 6. The closed loop poles of the controlled system at points (1) and (2) are virtually the same and are given as follows (nondimensionalized):

$$\begin{aligned} &-1.0043, -1.8 \pm i16.64, -2.16 \pm i24.20, -17.18 \pm i19.79, \\ &-26.23, -36.22, -137.64 \text{ and } -38.66 \pm i1132.11 \end{aligned}$$

The maximum force amplitudes as shown in Fig. 6 are less than those corresponding to Case (1) - Location I of Table 1 for comparable transient responses, whereas these are high as compared to the forces obtained using the pole clustering technique (Section (b)). This is due to the large negative real parts of the other modes in the linear regulator case when compared to the pole clustering technique where all the poles have an equal negative real part (-1.0). Both the linear regulator and pole clustering technique have the drawback that the controlled frequencies can be quite high compared to the uncontrolled frequencies. On the otherhand, these techniques have the advantage that they can be applied to situations where the number of actuators is less than the number of modes in the mathematical model, in contrast to the decoupling technique of Section (a).

### 5. Conclusions

In this paper the dynamics, stability, and control of an orbiting homogeneous, flexible square platform are considered. Three different nominal orientations of the platform are examined. When the platform is nominally following the local vertical with its larger surface perpendicular to the orbital plane and also when the platform follows the local horizontal with its larger surface normal to the local vertical, it is seen that the uncontrolled roll/yaw motion is unstable. For the case where the platform follows the local vertical with its large surface perpendicular to the orbit normal, the uncontrolled pitch motion is found to be unstable.

Three different control techniques are considered for the selection of the control laws:

- The decoupling of the original state equations using state variable feedback eliminates the need of a transformation from the original coordinates to the modal coordinates and provides a method of specifying directly the amount of damping and frequency of the individual components of the state vector. However, with this technique the number of actuators must be equal to the number of coordinates (modes) in the model.
- The pole placement algorithm (ORACLS) guarantees the over-all required damping of the system and does not restrict the number of actuators to be equal to the number of modes in the model. However, it is seen that the closed-loop frequencies may be greatly increased when compared to the open-loop values which may cause problems with externally induced periodic excitations.
- The linear regulator theory can provide acceptable performance once the state and penalty matrices are properly selected, and the number of actuators can be less than the number of modes in the model. Computer capacity and accuracy limit the number of modes that can be considered. Here, too, an undesirable increase in the closed-loop frequencies may result in order to provide satisfactory responses with maximum allowable force amplitudes.

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#### Appendix A - Nomenclature

$A_r$	$r^{\text{th}}$ modal amplitude function
$B$	Control influence matrix
$C_x, C_y, C_z$	Disturbance torques about the principal undeformed body axes
$E_r$	Generic force on $r^{\text{th}}$ mode
$f$	Force due to an actuator
$f_x, f_y, f_z$	Force components due to an actuator
$G_{R_x}, G_{R_y}, G_{R_z}$	Gravity gradient torques about the principal undeformed body axes
$I_x, I_y, I_z$	Moments of inertia about the principal axes
$K$	Gain matrix
$K_v, K_p$	Rate and position feedback gain matrices

$M_r$	$r^{\text{th}}$ modal mass
$T$	Torque due to an actuator
$T_x, T_y, T_z$	Torque components
$W_r(x, y)$	$r^{\text{th}}$ modal shape function
$Z_r$	Nondimensionalized $r^{\text{th}}$ modal amplitude function
$\omega_c$	Orbital frequency
$\omega_x, \omega_y, \omega_z$	Angular body rates
$\phi, \psi, \theta$	Roll, yaw, pitch, respectively
$\omega_1, \omega_2, \omega_3$	First three modal frequencies of the plate

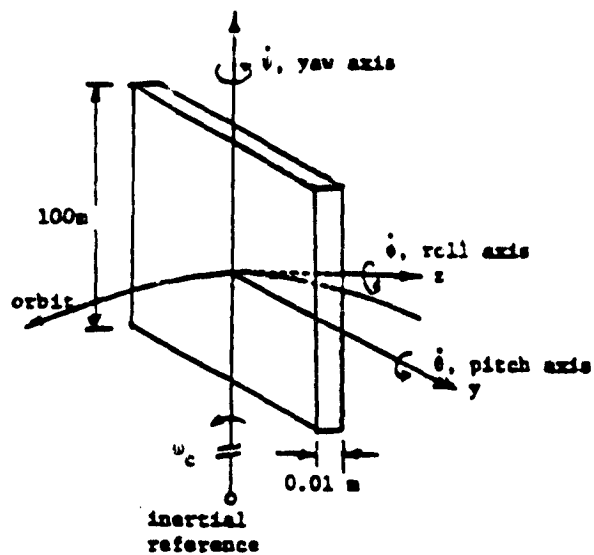


Fig. 1a. Platform following local vertical with major surface normal to the orbit plane - Case (i)

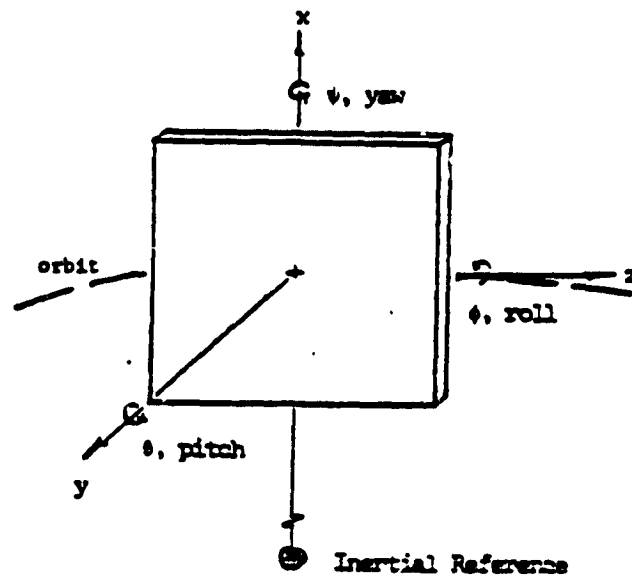


Fig. 1c. Platform following local vertical with major surface in the orbit plane - Case (iiii)

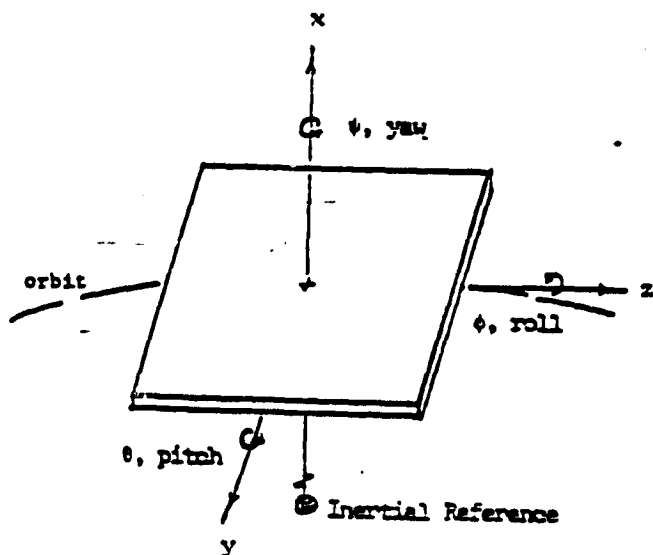


Fig. 1b. Platform along local horizontal - Case (ii)

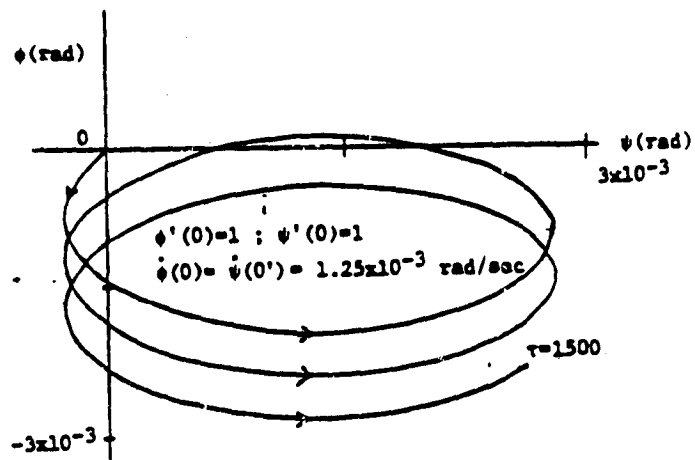


Fig. 2. Roll/yaw motion (uncontrolled) - Case (i)

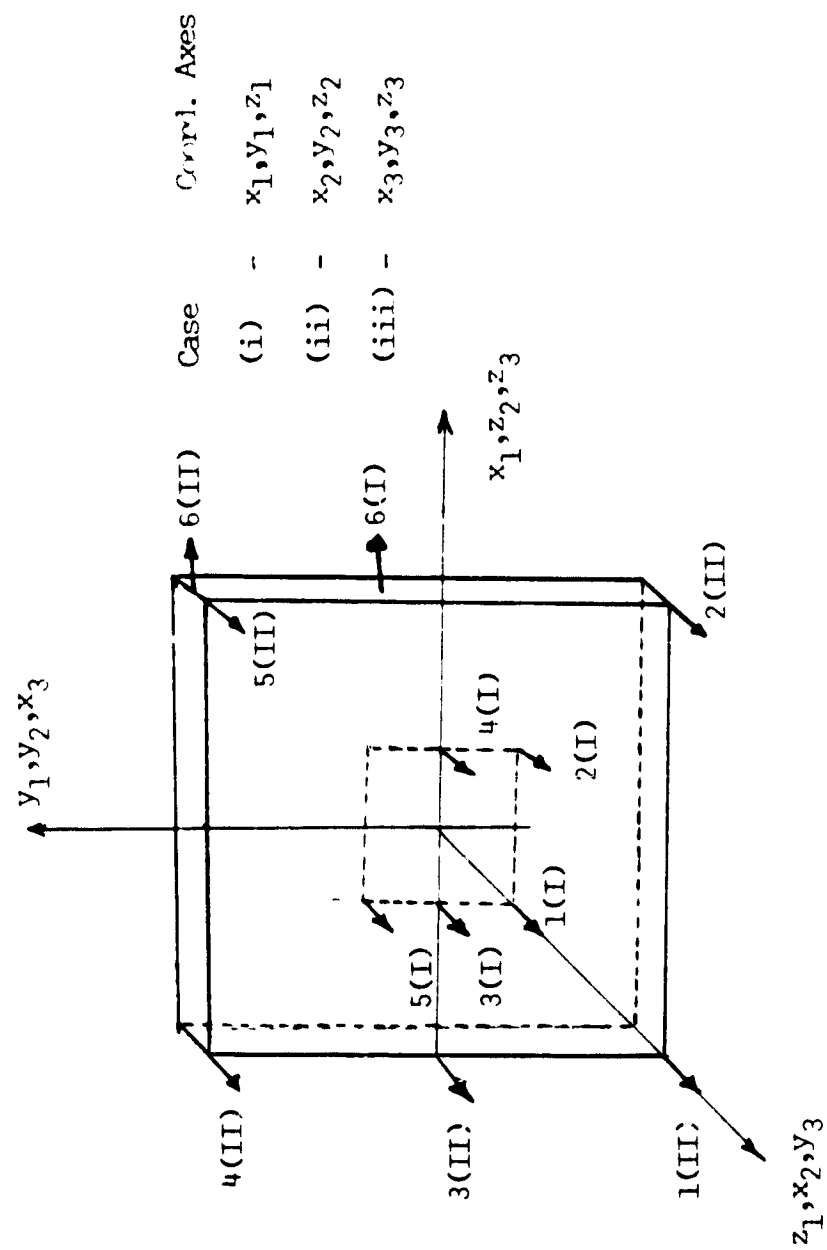


Fig 3. Location of two sets of actuators (I & II)

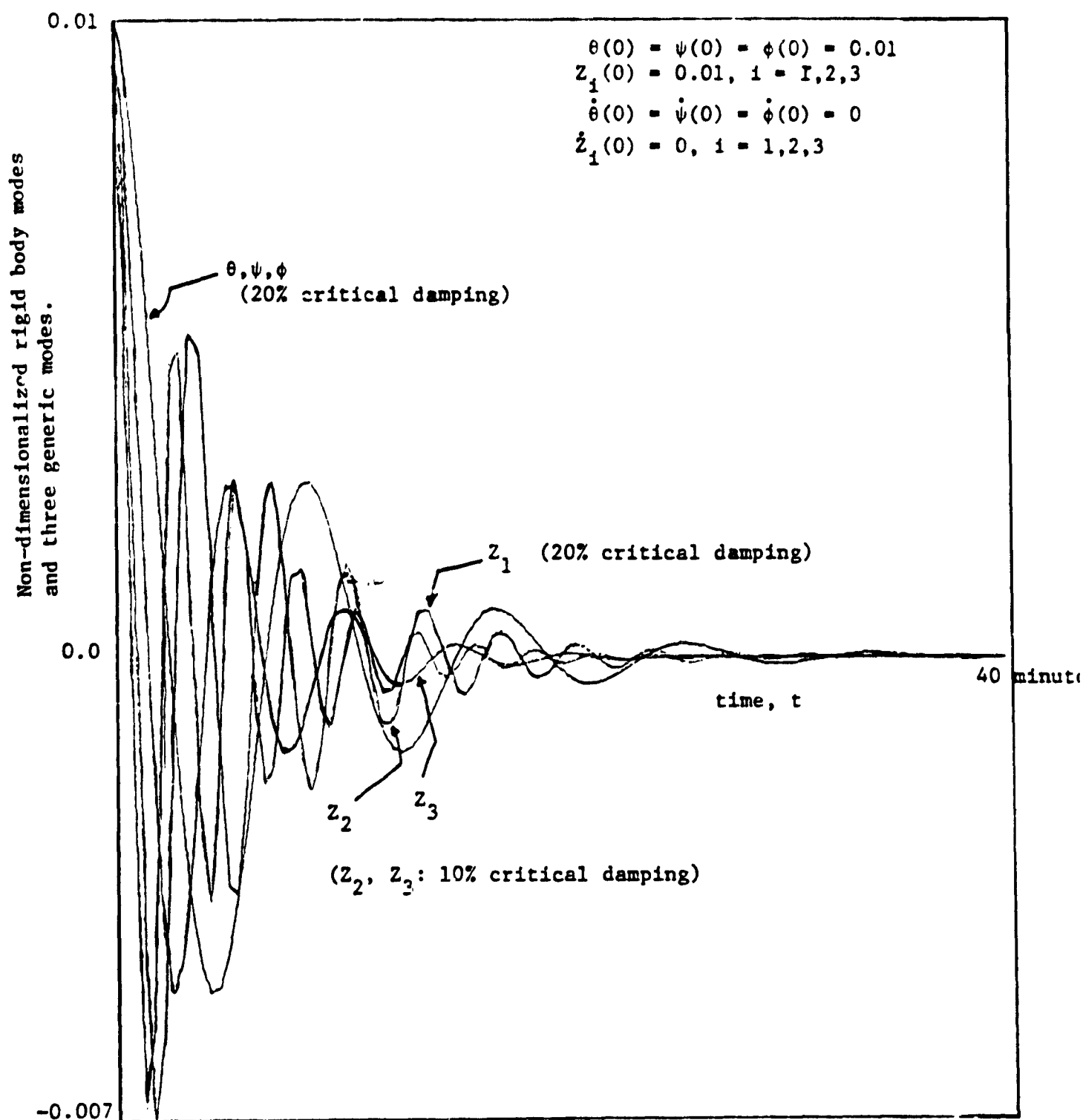


Fig 4a. Controlled state response for all combinations of orientations and actuator locations.

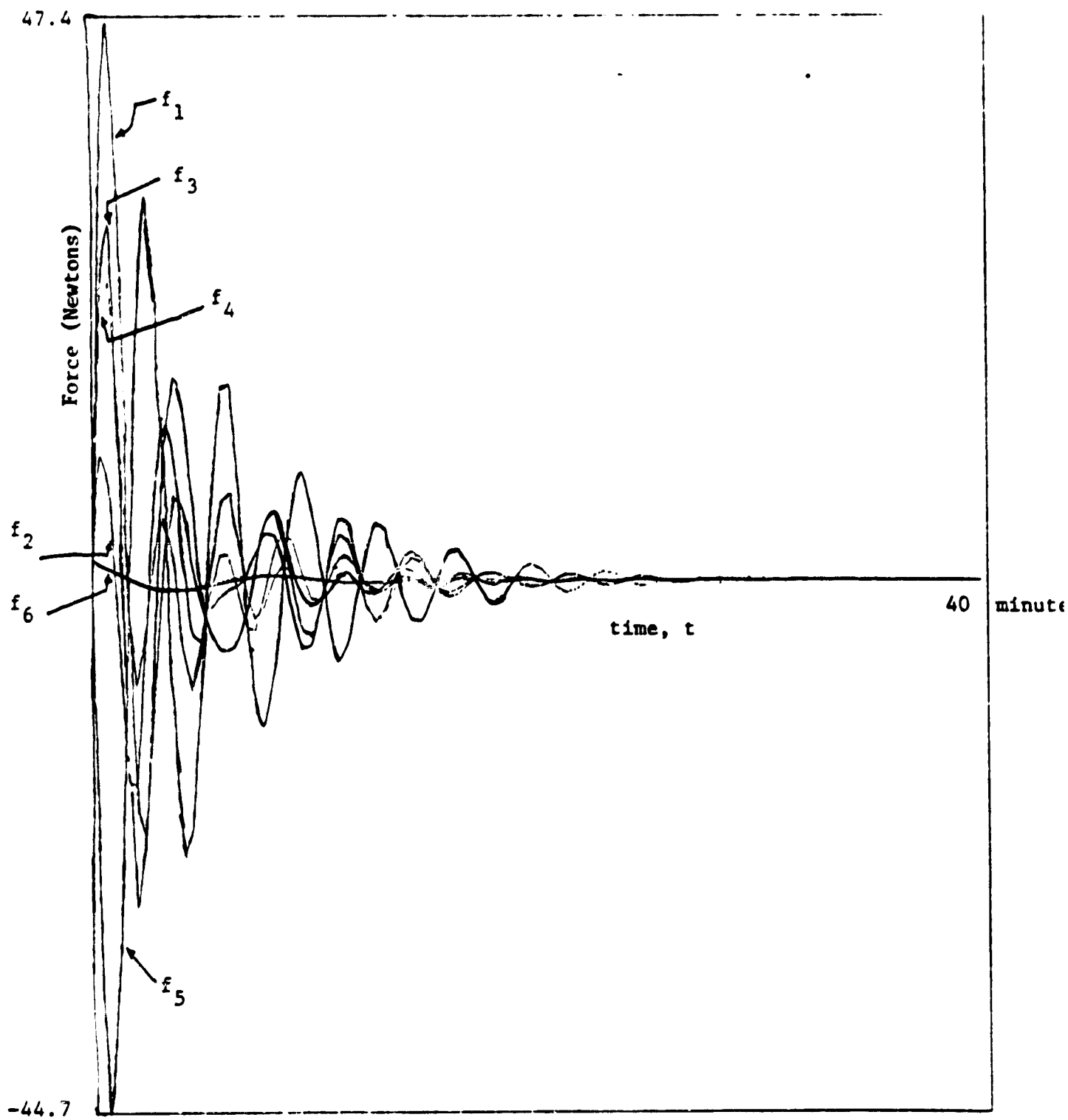


Fig 4b. Control force time history for Case (iii) - II

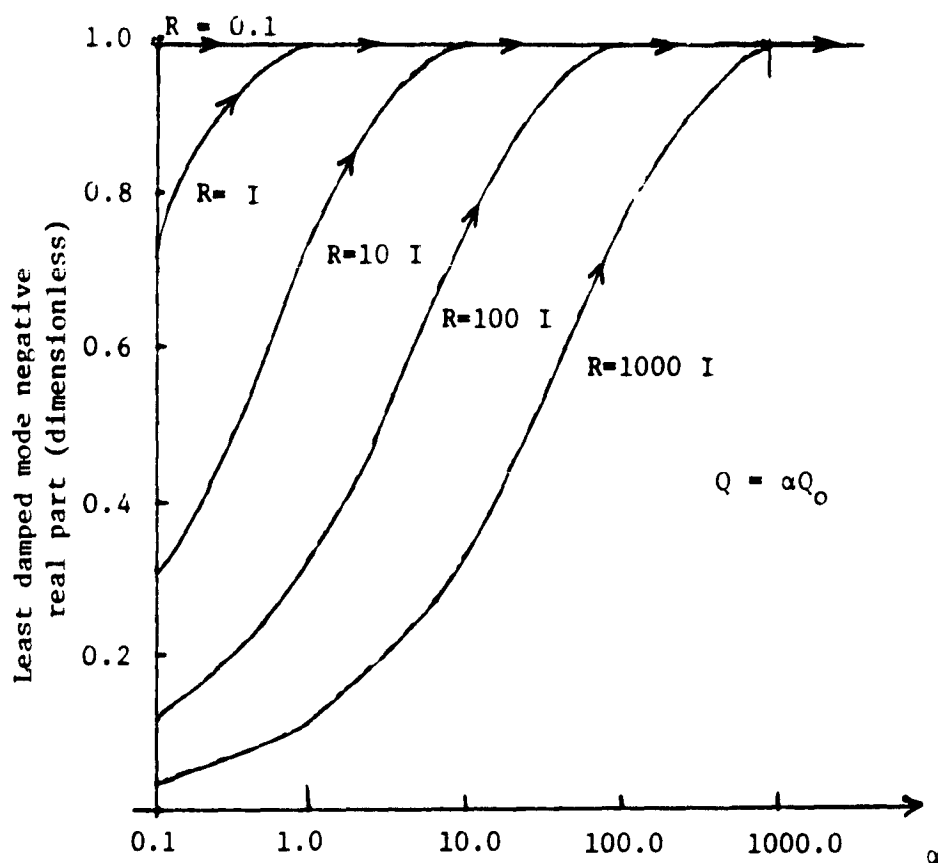


Fig. 5. Variation of least damped mode negative real part with  $\alpha$  and  $R$ .

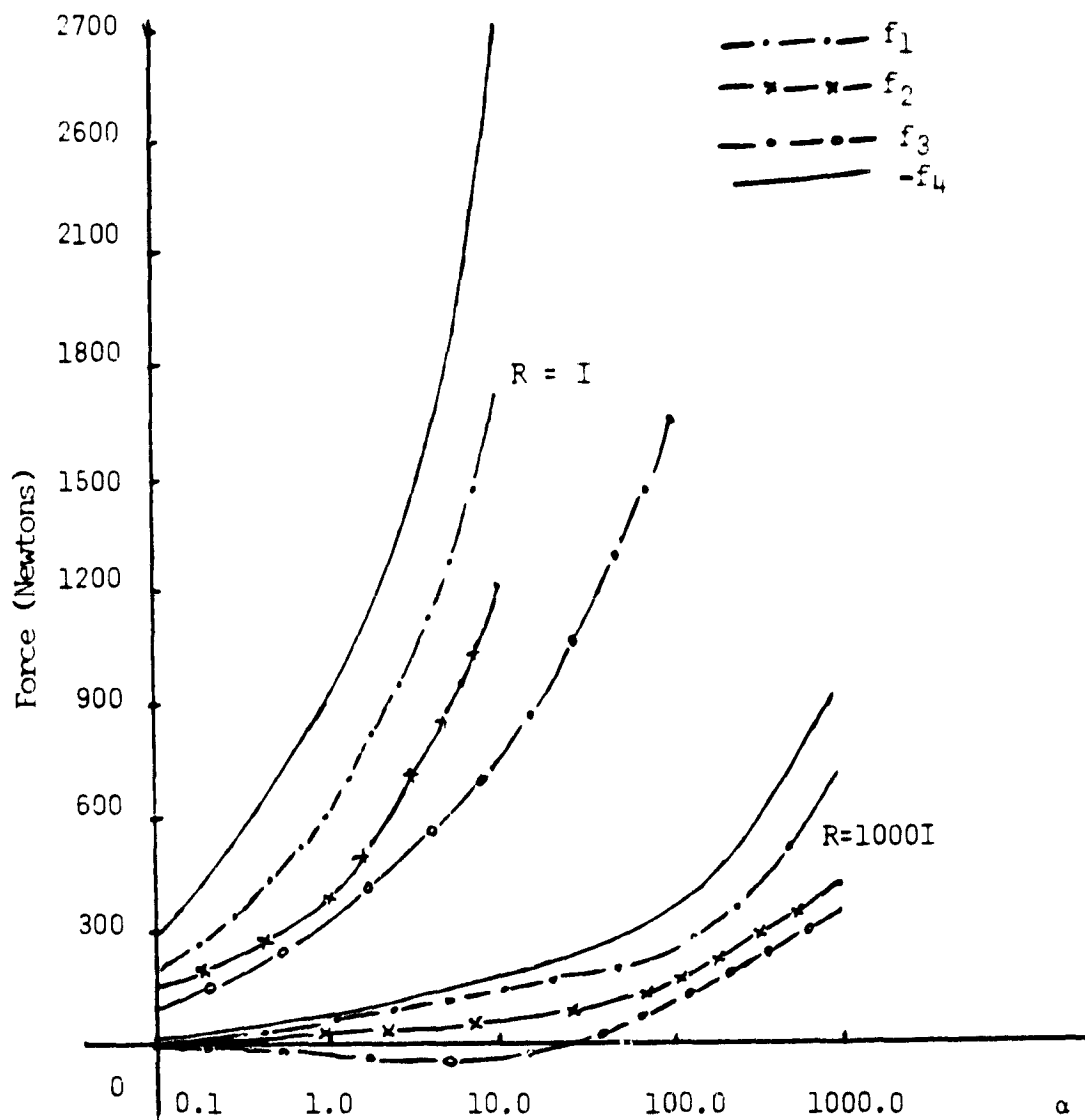


Fig 6. Maximum force amplitudes as a function of  $\alpha$  and  $R$  for all actuators - (application of linear regulator theory).



### III. FREQUENCIES AND MODE SHAPES FOR RECTANGULAR PLATES

The ability to determine accurately the frequencies and mode shapes is essential for the analysis and control of large structures in orbit. A thin rectangular plate, an important basic structure for several space applications, is considered for vibrational analysis. In the following sections the plate is assumed to be large, thin, and homogeneous, and all the edges are assumed to be free to vibrate. First, the approximate frequencies and mode shapes of a rectangular plate obtained by Warburton<sup>1</sup> is discussed. This analysis also includes the special case of a square plate. Next, the analytical results for a square plate using the method of Lemke<sup>2</sup> is considered. For a specific example of a square plate both analytical results are applied to determine the frequencies and mode shapes. An available finite element computer program<sup>3</sup> is also used to obtain the frequencies and mode shapes of this plate. The results of both analytical methods and the computer routine are compared and discussed.

#### 1. Formulation by Warburton

The approximate frequency formula is derived by applying the Raleigh method. The details of this method are given in the earlier contract report.<sup>4</sup> The basic equation used was the plate vibrational equation in the cartesian co-ordinate system (x,y), with the length and width of the plate taken along the x and y directions, respectively, and is given as

$$\frac{\partial^4 W}{\partial x^4} + 2 \frac{\partial^4 W}{\partial x^2 \partial y^2} + \frac{\partial^4 W}{\partial y^4} + \frac{12\rho(1-\sigma^2)}{Egh^2} \frac{\partial^2 W}{\partial t^2} = 0 \quad (\text{III-1})$$

where  $\rho, \sigma$  and  $E$  are the density, Poisson's ratio and Young's modulus of the plate material, respectively,  $h$  is the plate thickness, and  $g$  is the acceleration due to gravity. The displacement,  $w$ , at any point  $(x,y)$  at time  $t$  is given by

$$w = W \sin \omega t = A \theta(x) \phi(y) \sin \omega t \quad (\text{III-2})$$

$\theta(x)$  and  $\phi(y)$  can be taken as the beam functions orthogonal to each other and can be used to approximate plate behavior. After taking the appropriate free-free beam functions for  $\theta(x)$  and  $\phi(y)$ , the frequency expressions for a rectangular plate was derived as<sup>1</sup>

$$\lambda^2 = \frac{\rho a^4 (2\pi f)^2}{\pi^4 E h^2 g} \frac{12(1-\sigma^2)}{\quad} \quad (\text{III-3})$$

$$\text{and } \lambda^2 = G_x^4 + G_y^4 \frac{a^4}{b^4} + 2 \frac{a^2}{b^2} [\sigma H_x H_y + (1-\sigma) J_x J_y] \quad (\text{III-4})$$

where  $\lambda$  is a non-dimensional frequency factor,  $a$  and  $b$  are the length and width of the plate, and  $G_x, H_x, J_x, G_y, H_y,$  and  $J_y$  are functions associated with the number of nodal lines,  $m$  and  $n$ , parallel to  $x$  and  $y$ , respectively, for the beam functions  $\theta(x)$  and  $\phi(y)$ , and are given in Table III-1. From Eq. (III-3), the frequency is obtained as

$$f = \frac{\lambda h \pi}{a^2} \left[ \frac{E g}{48 \rho (1-\sigma^2)} \right]^{\frac{1}{2}} \quad (\text{cps}) \quad (\text{III-5})$$

Eq. (III-5) is valid for thin rectangular plates. However, for square plates,  $(m,n) \pm (n,m)$  types of modes exist, and for these cases  $\lambda$  in Eq. (III-5) must be modified. These cases are discussed in detail in Ref. 1 and a few relevant results are given here.

Modes (m,0) + (0,m), m is even

$$\lambda^2 = (m-\frac{1}{2})^4 + 2 \sigma (m-\frac{1}{2})^2 \frac{8}{\pi^2}$$

Modes (m,1) + (1,m), for m = 3,5,7,...

(III-6)

$$\lambda^2 = (\pi-\frac{1}{2})^4 + 2(1-\sigma) (m-\frac{1}{2})^2 \left[ 1 + \frac{6}{(m-\frac{1}{2})\pi} \right] \frac{12}{\pi^2} \\ + 2 \sigma (m-\frac{1}{2})^2 \frac{24}{\pi^2} \left[ 1 - \frac{2}{(m-\frac{1}{2})\pi} \right]^2 + 2(1-\sigma) \frac{192}{\pi^4}$$

For any mode of vibration the nodal pattern is defined by m and n, the number of nodal lines in the x and y directions, respectively. The mode shapes are obtained by using the corresponding modal frequencies in the beam functions and then evaluating the product,  $\theta(x) \cdot \phi(y)$ , numerically.

## 2. Formulation by Lemke<sup>2</sup>

The frequencies and mode shapes were computed for a square plate using the Raleigh-Ritz method. The results are readily available only for six of the modes obtained by Warburton's method. Lemke uses displacement functions of the type,

$$W = \sum A_{m,n} \theta_m(x) \phi_n(y) \quad (III-7)$$

where  $\theta_m(x)$  and  $\phi_n(y)$  are the free beam functions given as

$$\theta_m(x) = \frac{\cosh k_m \cos k_m x + \cos k_m \cosh k_m \bar{x}}{\sqrt{\cosh^2 k_m + \cos^2 k_m}} \quad (m \text{ even}) \\ = \frac{\sinh k_m \sin k_m x + \sin k_m \sinh k_m \bar{x}}{\sqrt{\sinh^2 k_m - \sin^2 k_m}} \quad (m \text{ odd}) \quad (III-8)$$

$\phi_n(y)$  is obtained from Eq. (III-8) by replacing x by y and m by n.

The values,  $k_m$ , are the roots of the equations

$$\tan k_m + \tanh k_m = 0 \quad (m \text{ even})$$

$$\tan k_m - \tanh k_m = 0 \quad (m \text{ odd})$$

which result from the spatial boundary conditions. Further, it was shown by an energy principle that <sup>2,4</sup>

$$\omega^2 = \frac{U_{\max}}{\frac{\rho h}{2g} \int_a^b \int_0^b W^2 dx dy} \quad (\text{III-9})$$

where  $U_{\max}$  is the maximum potential energy due to bending. The coefficients,  $A_{mn}$ , in Eq. (III-7) are determined to make  $\omega^2$  in Eq. (III-9) a minimum. Lemke obtained the coefficients,  $A_{mn}$ , by taking six or more terms in the series (III-7) and using four different values of Poisson's ratio. Expressions for six mode shapes and frequencies along with the coefficients,  $A_{mn}$ , are tabulated in Ref. 2. As an example the expression for the first mode is given here.

$$\begin{aligned} W(x,y) = & x_1 y_1 + 0.0325 (x_1 y_3 + x_3 y_1) - .005 x_3 y_3 \\ & - .00257 (x_1 y_5 + x_5 y_1) + .00121 (x_3 y_5 + x_5 y_3) \\ & - .000365 x_5 y_5 + \dots \end{aligned}$$

and 
$$\omega = \frac{13.086}{a^2} \sqrt{\frac{E h^3}{12 \rho (1-\sigma^2)}} \quad \text{for } \sigma = .343$$

### 3. Finite Element Computer Program

The computer program used is the Structural Design Language (STRUDL) which uses the finite element method to determine the mode shapes and the frequencies of vibration. The input to the computer routine is given by specifying the type of structure and supplying other physical properties and dimensions of the structure. For a rectangular plate, the finite elements can be specified as rectangular elements and the number of elements into which the plate should be divided depends upon the accuracy required. STRUDL gives deflections at each corner of the elements for all the modes from which the mode shapes can be determined. Further, a set of frequencies corresponding to the modes generated is obtained. In general, the accuracies of the frequencies and mode shapes will improve if the plate is modelled with a higher number of elements. However, computational errors due to truncation and round-off errors may predominate as the order of the elements increases beyond a limit. Further, the limitations of the computers will restrict the number of elements into which the plate can be divided to obtain more accurate results.

### 4. Discussion of Numerical Results

A square plate of sides 100 meters each and thickness 0.01 meters is considered to obtain the numerical results. The material of the plate is assumed to be aluminium with the following properties.

$$\text{density} = 2768.0 \text{ kg/m}^3$$

$$\text{Young's modulus} = 0.7441 \times 10^{10} \text{ kg/m}^2$$

$$\text{Poisson's ratio} = 0.33$$

Using Warburton's results, Eq. (III-4), Eq. (III-5), Table (III-1), and expressions for  $\theta(x)$  and  $\phi(y)$ , frequencies and mode shapes are calculated for different combinations of the number of nodal lines,  $m$  and  $n$ , starting with combinations of  $m=0$  and  $n=1$ , through  $m=3$  and  $n=3$ . The first three combinations of nodal line numbers,  $(0,0)$ ,  $(1,0)$  and  $(0,1)$ , represent rigid body motion. The first fundamental flexural frequency is seen to be due to a combination of  $m=1$  and  $n=1$ . The corresponding mode shape for the plate is obtained by multiplying the beam functions,  $\theta(x)$  and  $\phi(y)$ , for (beam) mode numbers 1 and 1, respectively (Fig. 1). Since the plate is approximated by sets of orthogonal beams in the  $x$  and  $y$  directions, the nodal pattern is also obtained by plotting the nodal points of these beams for their first modes. The next two higher frequencies are obtained by combinations of  $m=0$  and  $n=2$ , but the nodal patterns (Figs. 2,4) can not be visualized as before. This is because these frequencies are of a special type resulting from a combination of the  $(2,0)$  and  $(0,2)$  plate modes. It can be seen that when the mode corresponding to  $(2,0)$  (Fig. 3(a)) is superimposed on the mode -  $(0,2)$  (Fig. 3(b)) the mode shape depicted in Fig. 2 results. Similarly by superimposing the  $(2,0)$  and  $(0,2)$  modes the third mode shape (Fig. 4) is obtained. The two combinations of nodal patterns  $m=1$  and  $n=2$ , give identical frequencies for the fourth and fifth mode and the corresponding shapes (Fig. 5) are as expected. The next two higher frequencies are also identical and result from combinations of the  $(3,0)$  and  $(0,3)$  modes. The eighth frequency is obtained from  $m=2$  and  $n=2$  and the mode shape obtained is shown in Fig. 7.

However, the ninth and tenth mode shapes obtained by the (3,1) and (1,3) combinations, are once again of a special type. The ninth mode shape is obtained by superimposing the (1,3) and (3,1) patterns (Fig. 8) and the tenth mode shape is obtained by superimposing (1,3) and (3,1) nodal patterns (Fig. 9). The next higher frequencies are obtained from combinations of the (3,2), (2,3) and (3,3) modes, respectively. The frequencies and nodal patterns obtained for all these modes are shown in Table 2.

Frequencies and mode shapes are also obtained by using the expressions for the six modes given by Lemke.<sup>2</sup> The first three frequencies and mode shapes obtained agree with the frequencies and mode shapes computed from Warburton's formulas (Table 1). However, the next three frequencies obtained by Lemke's method correspond to higher frequencies and mode shapes obtained by Warburton's method. Also the nodal patterns obtained by Lemke's method compare approximately with the nodal patterns obtained by Warburton's method although the frequencies do not correspond in all cases. The results obtained by Lemke do not show the four intermediate frequencies corresponding to the fourth, fifth, sixth and seventh modes obtained by Warburton's method. The frequencies and nodal pattern obtained by Lemke's method are shown in Table 2.

For implementation of the computer program STRUDL, first the plate is divided into four elements. The first six modes (in terms of increasing frequencies) as predicted by STRUDL are also apparent from Warburton's results. The plate is assumed to be divided into 9, 16, 36 and 64 elements, respectively. The results of STRUDL are tabulated in Table 2. It can be seen that STRUDL frequencies approach the frequencies obtained by Warburton's method as the number of plate elements is increased.

However, in the cases of 36 and 64 elements some of the frequencies show a tendency to oscillate about an average value. This probably is due to the computational round off errors which begin to dominate with the increasing computations associated with larger number of elements. Thus, the advantage of taking a large number of elements may not be fully realized due to numerical accuracy limitations. Computation with more elements requires more computation time and a larger computer memory. For the 64 elements case, it was not possible to obtain the mode shapes due to memory limitations. It was also observed that the convergence of the frequencies, with an increase in the number of elements, is faster than the convergence of the mode shapes. It can be seen from Table 2, that the numerical results of STRUDL using 36 elements correlate with the results of Warburton both in frequency and mode shapes.

Table 3 and Table 4 compare non-dimensionalized deflections at the nodes (corners of elements) obtained by the three methods for the second mode (Fig. 2). For locations where deflections exist and do not correspond to maximum amplitude ( $\pm 1.0$ ) in all cases the results predicted by STRUDL lie in between the results obtained by the analytical methods of Lemke and Warburton.

The results of this comparative study give an indication of the types of modelling errors that would be expected in the estimation of the frequencies and mode shapes of the fundamental and lower order flexural modes of a large platform type structure in orbit. As an extension to this study the use of more powerful (and accurate) finite element computer algorithms, not currently available at Howard University, is recommended.



## 5. References

1. Warburton, G.B., "The Vibration of Rectangular Plates," Proc. Inst. Mech. Engrs., Vol. 168, No. 12, 1954, pp. 371-394.
2. Leissa, A.W., "Vibration of Plates", NASA SP-160, NASA, Washington, D.C., 1969, pp. 87-110.
3. ICES-STRU DL-II, Engineering Users Manual, Volume II, 1972.
4. Bainum, P.M. and James, P.K., "The Dynamics and Control of Large Flexible Space Structures - II. PART B: Model Development and Computer Simulation," June 1979.

TABLE III-1. Evaluation of Parameters in Frequency Expression (Warburton)

m	$G_x$	$H_x$	$J_x$	n	$G_y$	$H_y$	$J_y$
0	0	0	0	0	0	0	0
1	0	0	$\frac{12}{\pi^2}$	1	0	0	$\frac{12}{\pi^2}$
2	1.506	1.248	5.017	2	1.506	1.248	5.017
3 4 5 ⋮	$m - \frac{1}{2}$	$(m - \frac{1}{2})^2 P$	$(m - \frac{1}{2})^2 Q$	3 4 5 ⋮	$(n - \frac{1}{2})$	$(n - \frac{1}{2})^2 P$	$(n - \frac{1}{2})^2 Q$

$$P = [1 - 2/(m - 0.5)\pi]$$

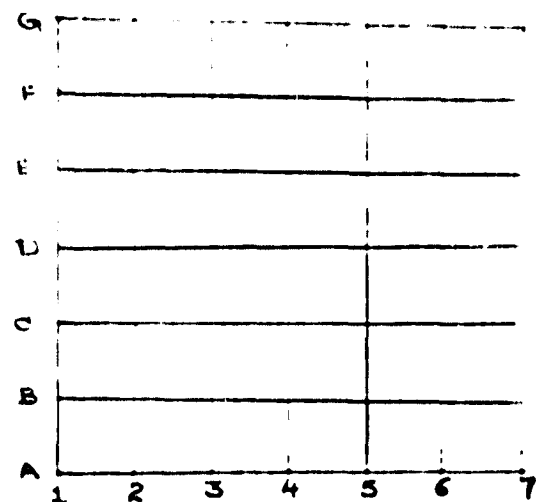
$$Q = [1 + 6/(m - 0.5)\pi]$$

STRUDL					WARBURTON			LIFE		
	NUMBER OF ELEMENTS				Nodal Pattern	Freq. (cps)	(m,n)	Nodal Pattern	Freq. (cps)	Nodal Pattern
	4	9	16	36						
1	.003165	.003284	.003315	.003314	.003358	.003471	(1,1)		.003287	
2	.004291	.004664	.004776	.004839	.004856	.004846	(2,0)-(0,2)		.004921	
3	.005549	.006133	.006221	.006221	.006207	.006175	(2,0)+(0,2)		.006175	
4	.007619	.008453	.008632	.008690	.008692	.009000	(2,1)		.015744	
5	.007619	.008453	.008632	.008690	.008692	.009000	(1,2)		.017167	
6	.013223	.01512	.01600	.01596	.01579	.01542	(3,0)		.01944	
7		.01512	.01600	.01596	.01579	.01542	(0,3)			
8		.01584	.01618	.01615	.01607	.01656	(2,2)			
9		.01630	.01727	.01750	.01746	.01715	(3,1)-(1,3)			
10		.01843	.02022	.02031	.02005	.0208	(1,3)+(3,1)			
11		.02465	.02693	.02693	.02700	.02726	(3,2)			
12		.02465	.02673	.02643	.02700	.02726	(2,3)			
13		.03362	.03029	.03162	.03104	.03941	(3,3)			

TABLE-III-2. Frequencies and Nodal Patterns Obtained by the Three Methods.

Case 1: 4 Elements

LOCATION	STRUDEL	LEMKE	WARBURTON
A1	0	0	0
A2	1.0	1.0	1.0
B1	-1.0	-1.0	-1.0
B2	0	0	0



grid used for 36 elements

Case 2: 9 Elements

LOCATION	STRUDEL	LEMKE	WARBURTON	STRUDEL	LEMKE	WARBURTON
A1	0	0	0	0	0	0
A2	1.0	1.0	1.0	.7014	.7327	.6837
A3	1.0	1.0	1.0	1.0	1.0	1.0
B1	-1.0	-1.0	-1.0	-.7014	-.7327	-.6837
B2	0	0	0	0	0	0
B3	0	0	0	.2862	.2673	.3163
C1	-1.0	-1.0	-1.0	-1.0	-1.0	-1.0
C2	0	0	0	-.2862	-.2673	-.3163
C3	0	0	0	0	0	0

Case 3: 16 Elements

TABLE-III-3. Normalized Deflections at the Nodal Points Obtained by the Three Methods - Second Mode.

Case 4: 36 Elements

LOCATION	STRUDEL	WARBU- RTON	LEMKE	LOCATION	STRUDEL	WARBU- RTON	LEMKE
A <sub>1</sub>	0	0	0	C <sub>1</sub>	-.8590	-.8524	-.9793
A <sub>2</sub>	.4874	.4733	.5346	C <sub>2</sub>	-.3595	-.3792	-.3447
A <sub>3</sub>	.8590	.8524	.9793	C <sub>3</sub>	0	0	0
A <sub>4</sub>	1.0	1.0	1.0	C <sub>4</sub>	.1334	.1475	.1207
B <sub>1</sub>	-.4873	-.4733	-.5346	D <sub>1</sub>	-1.0	-1.0	-1.0
B <sub>2</sub>	0	0	0	D <sub>2</sub>	-.4938	-.5267	-.4654
B <sub>3</sub>	.3594	.3792	.3447	D <sub>3</sub>	-.1334	-.1475	-.1207
B <sub>4</sub>	.4933	.5267	.4654	D <sub>4</sub>	0	0	0

TABLE III-4. Normalized Deflections at the Nodal Points Obtained by the Three Methods - Second Mode.



Fig. 1 First Mode

(1,1)

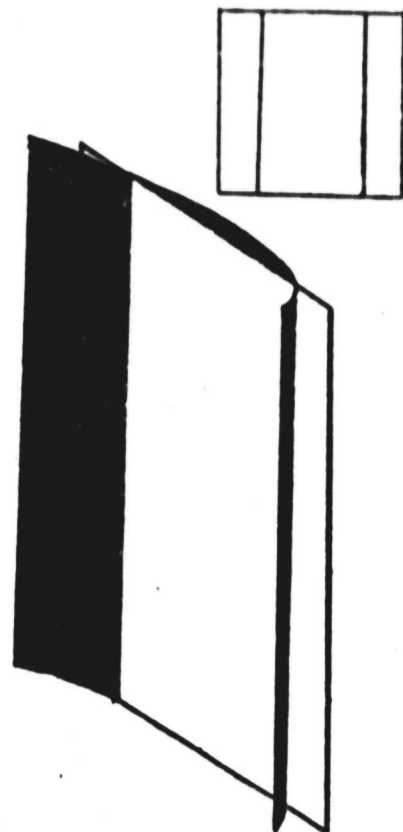


Fig. 3(a) (2,0) Mode

(2,0)

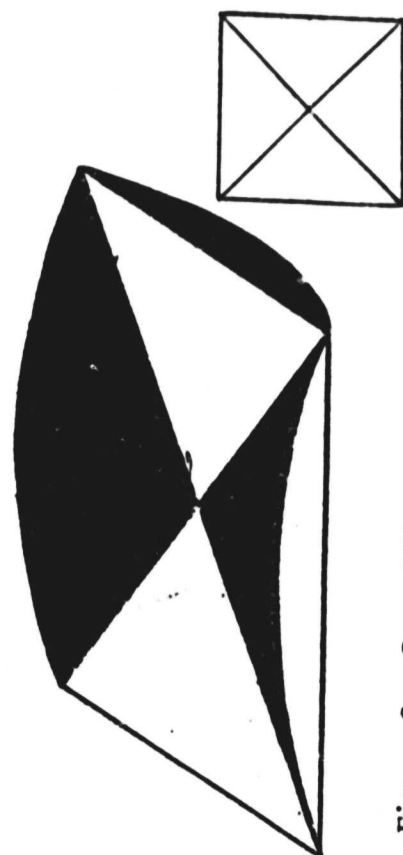


Fig. 2 Second Mode

(2,0)-(0,2)



Fig 3(b) (0,2) Mode

(0,2)

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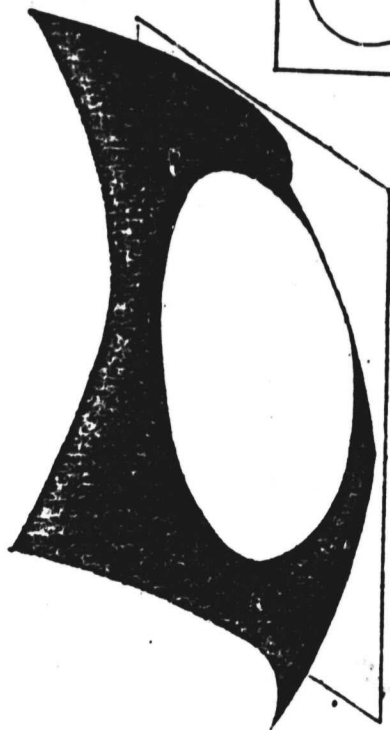
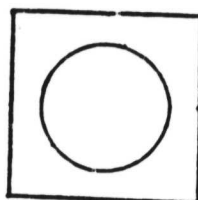


Fig. 4: Third Mode



$(2,0) + (0,2)$

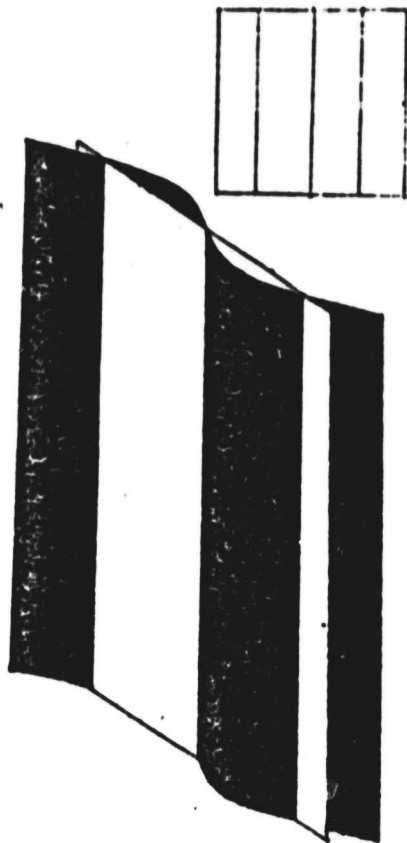


Fig. 6: Sixth Mode



$(3,0)$

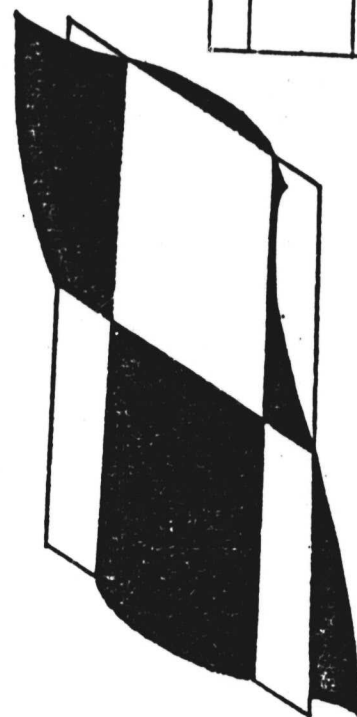
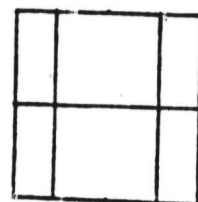


Fig. 5: Fourth Mode



$(2,1)$

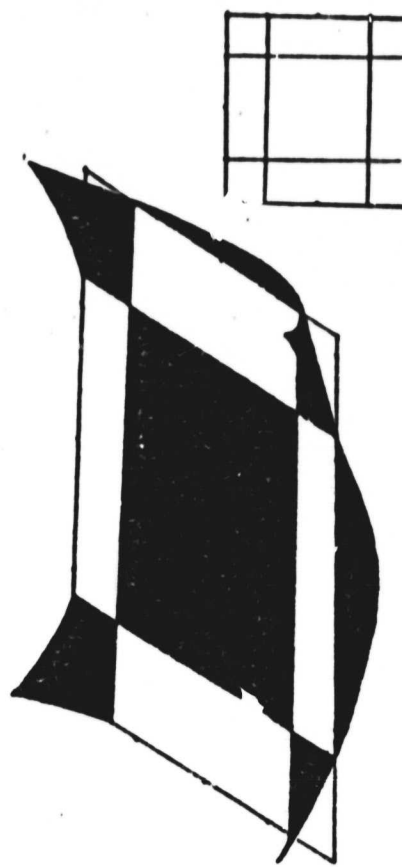
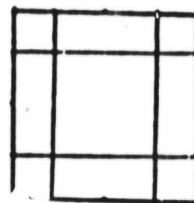
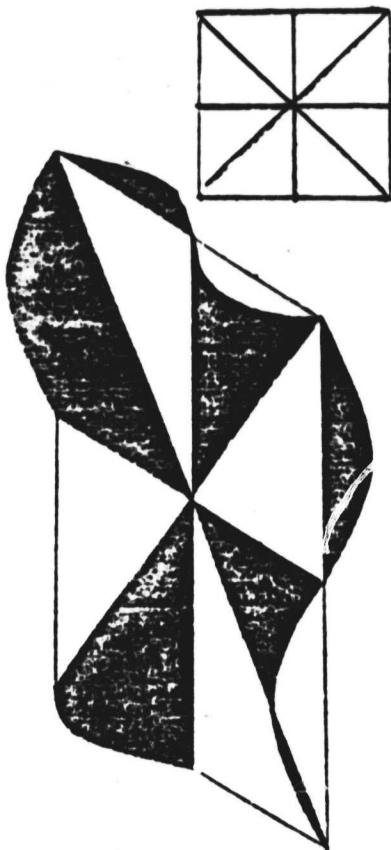


Fig. 7: Eighth Mode



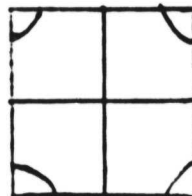
$(2,2)$

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(1,3)-(3,1)

Fig. 8: Ninth Mode



(1,3)+(3,1)

Fig. 9: Tenth Mode



#### IV. GENERAL CONCLUSIONS AND RECOMMENDATIONS

A model is developed for predicting the dynamics of a large flexible free-free thin platform in orbit under the influence of control devices which are considered to be placed at specific locations on the major surface and one of the edges. Control about three different nominal orientations is considered. In the absence of control, for the case of a completely homogeneous platform instability in at least some of the modes is indicated for small amplitude motion about each of the three orientations. Once controllability is established, for a set of actuator locations, three different techniques are employed for the selection of actuator control laws:

- (1) the decoupling of the original state equations using state variable feedback;
- (2) a pole placement algorithm; and
- (3) an application of the linear regulator theory

It is seen that each of the three techniques have certain distinct advantages and also specific limitations), which are discussed in detail in Chapter II. For systems involving multi-degrees of freedom (such as in this application), the implementation of these techniques requires the extensive usage of computer algorithms.

As a logical extension to the present study which assumes perfect instantaneous knowledge of the state, the modelling of the sensor dynamics and related problem of observability should be considered, once specific information on the types of sensors required for monitoring the performance of large flexible systems is available.

The problems caused by both observation and control spillover could also be treated, perhaps by beginning with the simpler model of the control of a long, flexible beam in orbit and then extending this analysis to the three dimensional model of the platform.

A model of the uncontrolled dynamics of a large flexible shallow spherical shell (representative of an antenna dish or large radiometer) in orbit has been developed during the present grant year (see Part B this report). It is suggested that the effect of control devices be included in this model and that control laws could then be developed using different algorithms already in existence.

## APPENDIX

### Modifications to ORACLS Software Package

The ORACLS<sup>8</sup> Software Package that was developed at Langley which operates on the Control Data Cyber Computer System was modified to suit the IBM 370/165 Computer System that is available at Howard University.

The major modifications that were done are described below:

- (1) As the single precision accuracy on the CDC is approximately equal to the double precision on the IBM/370 System, the entire package was converted into double precision.
- (2) Some of the machine dependent constants were changed accordingly.
- (3) As the IBM System accepts only six letters for a subroutine/function name all the names that exceeded six letters were changed and the list of those subroutines is given below:

<u>Old Name</u>	<u>New Name</u>
(1) TESTSTA	TESTSA
(2) VARANCE	VARANC
(3) TRANSIT	TRNSIT
(4) DISCREG	DISREG
(5) CNTNREG	CNTREG
(6) RICTNWT	RICNWT
(7) ASYMREG	ASMREG
(8) ASYMFIL	ASMFIL
(9) EXPMDFL	EXPMDF
(10) IMPMDFL	IMPMDF

- (4) Some of the additional supporting subroutines/functions required were added and the names of these subroutines are given here:

- (1) PNCH
- (2) DIMAG
- (3) DREAL
- (4) BLOCK DATA

(5) None of the arguments of the subroutines were changed

The listing of the modified ORACLS package is given in the following pages. These routines have to be used in conjunction with Ref. (8). The numbers that appear in front of the FORTRAN statements are line numbers and have to be omitted.

1	SUBROUTINE RDTITLE	RDT00010
2	IMPLICIT REAL*8 (A-H,O-Z)	RDT00020
3	COMMON/LINES/TITLE(10),TIL(3),NLP,LIN	RDT00030
4	COMMON/FORM/FMT1(2),FMT2(2),NEPR	RDT00040
5	COMMON/TOL/EPSSAM,EPSSBM,IACM	RDT00050
6	COMMON/CONV/SUMCV,RICTCV,SERCV,MAXSUM	RDT00060
7	NLP = NO. LINES/PAGE VARIES WITH THE INSTALLATION	RDT00070
8	READ(5,100,END=90,ERR=91) TITLE	RDT00080
9	100 FORMAT(10A8)	RDT00090
10	CALL LNCNT(100)	RDT00100
11	RETURN	RDT00110
12	90 CONTINUE	RDT00120
13	STOP 1	RDT00130
14	91 CONTINUE	RDT00140
15	STOP 2	RDT00150
16	END	RDT00160

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	SUBROUTINE LNCNT (N)	LNC00010
	IMPLICIT REAL*8 (A-H,O-Z)	LNC00020
2	COMMON/LINES/TITLE(10),TIL(3),NLP,LIN	LNC00030
	LIN=LIN+N	LNC00040
	IF (LIN.LE.NLP) GO TO 20	LNC00050
5	WRITE(6,1010) TITLE,TIL	LNC00060
6	1010 FORMAT(1H1,10A8,3A8/)	LNC00070
	LIN=2+N	LNC00080
	IF (N.GT.NLP) LIN=2	LNC00090
9	20 RETURN	LNC00100
	END	LNC00110

1	SUBROUTINE READ(I,A,NA,B,NB,C,NC,D,ND,E,NE)	REA00010
2	IMPLICIT REAL*8 (A-H,O-Z)	REA00020
3	DIMENSION A(1),B(1),C(1),D(1),E(1)	REA00030
4	DIMENSION NA(2),NB(2),NC(2),ND(2),NE(2),NZ(2)	REA00040
5	READ(5,100) LAB, NZ(1), NZ(2)	REA00050
6	CALL READ1(A, NA,NZ, LAB)	REA00060
7	IF(I .EQ. 1) GO TO 999	REA00070
8	READ(5,100) LAB, NZ(1), NZ(2)	REA00080
9	CALL READ1(B, NB,NZ, LAB)	REA00090
10	IF(I .EQ. 2) GO TO 999	REA00100
11	READ(5,100) LAB, NZ(1), NZ(2)	REA00110
12	CALL READ1(C, NC,NZ, LAB)	REA00120
13	IF(I .EQ. 3) GO TO 999	REA00130
14	READ(5,100) LAB, NZ(1), NZ(2)	REA00140
15	CALL READ1(D, ND,NZ, LAB)	REA00150
16	IF(I .EQ. 4) GO TO 999	REA00160
17	READ(5,100) LAB, NZ(1), NZ(2)	REA00170
18	CALL READ1(E, NE,NZ, LAB)	REA00180
19	100 FORMAT(A4,4X,2I4)	REA00190
20	999 RETURN	REA00200
21	END	REA00210

1	SUBROUTINE PRNT(A,NA,NAM,IOP)	PRN00010
2	IMPLICIT REAL*8 (A-H,O-Z)	PRN00020
3	DIMENSION A(1),NA(2)	PRN00030
4	COMMON /FORM/FMT1(2),FMT2(2),NEPR	PRN00040
5	COMMON/LINES/TITLE(10),TIL(3),NLP,LIN	PRN00050
6	C- NOTE NLP NO. LINES/PAGE VARIES WITH THE INSTALLATION.	PRN00060
7	DATA KZ,KW,K8 /1H0,1H1,1H /	PRN00070
8	NAME = NAM	PRN00080
9	II = IOP	PRN00090
10	NR = NA(1)	PRN00100
11	NC = NA(2)	PRN00110
12	NLST = NR * NC	PRN00120
13	IF( NLST .LT. 1 .OR. NR .LT. 1 ) GO TO 16	PRN00130
14	IF(NAME .EQ. 0) NAME = K8	PRN00140
15	C- SKIP HEADLINE IF REQUESTED.	PRN00150
16	GO TO (11,10,132,12), II	PRN00160
17	10 CALL LNCNT(100)	PRN00170
18	11 CALL LNCNT(2)	PRN00180
19	3 WRITE(6,177) KZ,NAME,NR,NC	PRN00190
20	177 FORMAT(A1,5X,A4,8H MATRIX,5X,I3,5H ROWS,5X,I3,8H COLUMNS)	PRN00200
21	GO TO 13	PRN00210
22	12 CALL LNCNT(100)	PRN00220
23	GO TO 13	PRN00230
24	132 CALL LNCNT(2)	PRN00240
25	WRITE (6,891)	PRN00250
26	891 FORMAT (1H0)	PRN00260
27	C- BELOW COMPUTE NR OF LINES/ ROW --DECIDE IF 1 EXTRA BLANK LINE	PRN00270
28	13 J=(NC-1)/NEPR+1	PRN00280
29	C- WHY ALWAYS ADD 1 LINE- BECAUSE IF MULTIPLE, USE 1 BLK LINE EXTRA.	PRN00290
30	NLPW=J	
31	JST=1	
32	C COMPUTE LAST ROW POSITION -1 BELOW	PRN00330
33	NLST = NLST -NR	PRN00340
34	MN=NC	PRN00350
35	IF (NC.GT.NEPR) MN=NEPR	PRN00360
36	KLST=NR*(MN-1)	PRN00370
37	CONTINUE	PRN00380
38	DO 912 J = JST, NR	PRN00390
39	CALL LNCNT(NLPW)	PRN00400
40	KLST = KLST +1	PRN00410
41	WRITE (6,FMT1) (A(N), N=J,KLST,NR)	PRN00420
42	IF (NC.LE.NEPR) GO TO 912	PRN00430
43	NLST = NLST +1	PRN00440
44	KNR=KLST+NR	PRN00450
45	WRITE (6,FMT2) (A(N), N=KNR,NLST,NR)	PRN00460
46	912 CONTINUE	PRN00470
47	RETURN	
48	16 CALL LNCNT(1)	PRN00490
49	WRITE (6,916) NAM,NA	PRN00500
50	916 FORMAT (' ERROR IN PRNT MATRIX ',A4,' HAS NA=',2I6)	PRN00510
51	RETURN	PRN00520
52	END	



	SUBROUTINE EQUATE(A,NA,R,NR)	EQU00010
	IMPLICIT REAL*4 (A-H,O-Z)	EQU00020
2	DIMENSION A(1),B(1),NA(2),NB(2)	EQU00030
3	NR(1) = NA(1)	EQU00040
4	NR(2) =NA(2)	EQU00050
5	L=NA(1)+NA(2)	EQU00060
6	IF( NA(1) .LT. 1 .OR. L .LT. 1 ) GO TO 999	EQU00070
	DO 300 I=1,L	EQU00080
	300 B(I)=A(I)	EQU00090
9	1000 RETURN	EQU00100
10	999 CALL LNCNT (1)	EQU00110
11	WRITE (6,50) NA	EQU00120
12	50 FORMAT (' DIMENSION ERROR IN EQUATE NA=',2I6)	EQU00130
13	RETURN	EQU00140
14	END	EQU00150

```

SUBROUTINE TRANP(A,NA,R,NB)
IMPLICIT REAL*8 (A-H,O-Z)
DIMENSION A(1),B(1),NA(2),NB(2)

```

```

NB(1)=NA(2)

```

```

NB(2)=NA(1)

```

```

NR=NA(1)

```

```

NC=NA(2)

```

```

L=NR+NC

```

```

IF( NR .LT. 1 .OR. L .LT. 1 ) GO TO 999

```

```

IR=0

```

```

DO 300 I=1,NR

```

```

IJ=I-NR

```

```

DO 300 J=1,NC

```

```

IJ=IJ+NR

```

```

IR=IR+1

```

```

300 B(IR)=A(IJ)

```

```

RETURN

```

```

999 CALL LNCNT(1)

```

```

WRITE (6,50) NA

```

```

50 FORMAT (' DIMENSION ERROR IN TRANP  NA=',2I6)

```

```

RETURN

```

```

END

```

```

TRA00010
TRA00020
TRA00030
TRA00040
TRA00050
TRA00060
TRA00070
TRA00080
TRA00090
TRA00100
TRA00110
TRA00120
TRA00130
TRA00140
TRA00150
TRA00160
TRA00170
TRA00180
TRA00190
TRA00200
TRA00210
TRA00220

```

```

SUBROUTINE SCALE (A, NA, H, NB, S)
IMPLICIT REAL*8 (A-H,O-Z)
DIMENSION A(1),B(1),NA(2),NB(2)
NB(1) = NA(1)
NB(2) = NA(2)
L = NA(1)*NA(2)
IF( NA(1) .LT. 1 .OR. L .LT. 1 ) GO TO 999
DO 300 I=1,L
300 B(I)=A(I)*S
1000 RETURN
999 CALL LNCNT(1)
WRITE (6,50) NA
50 FORMAT (' DIMENSION ERROR IN SCALE NA=',2I6)
RETURN
END

```

```

SCA00010
SCA00020
SCA00030
SCA00040
SCA00050
SCA00060
SCA00070
SCA00080
SCA00090
SCA00100
SCA00110
SCA00120
SCA00130
SCA00140
SCA00150

```

0	SUBROUTINE UNITY(A,NA)	UNI00010
1	IMPLICIT REAL*8 (A-H,O-Z)	UNI00020
2	DIMENSION A(1),NA(2)	UNI00030
3	IF(NA(1).NE.NA(2)) GO TO 999	UNI00040
4	L=NA(1)+NA(2)	UNI00050
5	DO 100 IT=1,L	UNI00060
6	100 A(IT)=0.0	UNI00070
7	J = NA(1)	UNI00080
8	NAX = NA(1)	UNI00090
9	DO 300 I=1,NAX	UNI00100
10	J=NAX +J+1	UNI00110
11	300 A(J)=1.	UNI00120
12	GO TO 1000	UNI00130
13	999 CALL LNCNT (1)	UNI00140
14	WRITE(6, 50)(NA(I),I=1,2)	UNI00150
15	50 FORMAT (' DIMENSION ERROR IN UNITY NA=',2I6)	UNI00160
16	1000 RETURN	UNI00170
17	END	UNI00180

0	SUBROUTINE NULL(A,NA)	NUL00010
1	IMPLICIT REAL*8 (A-H,O-Z)	NUL00020
2	DIMENSION A(1)	NUL00030
3	DIMENSION NA(2)	NUL00040
4	N=NA(1)*NA(2)	NUL00050
5	IF( NA(1) .LT. 1 .OR. N .LT. 1 ) GO TO 999	NUL00060
6	DO 10 I=1,N	NUL00070
7	10 A(I) = 0.0	NUL00080
8	RETURN	NUL00090
9	C	NUL00100
10	999 CONTINUE	NUL00110
11	WRITE (6,50) NA	NUL00120
12	50 FORMAT(' DIMENSION ERROR IN NULL NA =',2I6)	NUL00130
13	RETURN	NUL00140
14	END	NUL00150

0	SUBROUTINE TRCE (A,NA,TR)	TRC00010
1	IMPLICIT REAL*8 (A-M,O-Z)	TRC00020
2	DIMENSION A(1)	TRC00030
3	DIMENSION NA(2)	TRC00040
4	IF (NA(1).NE.NA(2)) GO TO 600	TRC00050
5	N=NA(1)	TRC00060
6	TR=0.0	TRC00070
7	IF( N .LT. 1 ) GO TO 600	TRC00080
8	DO 10 I=1,N	TRC00090
9	M=I+N*(I-1)	TRC00100
10	10 TR=TR+A(M)	TRC00110
	RETURN	TRC00120
11	600 CALL LNCNT(1)	TRC00130
12	WRITE (6,1600) NA	TRC00140
13	1600 FORMAT (' TRACE REQUIRES SQUARE MATRIX NA=',2I6)	TRC00150
14	RETURN	TRC00160
15	END	TRC00170

0	SUBROUTINE ADD (A,NA,B,NB,C,NC)	ADD000010
	IMPLICIT REAL*8 (A-H,O-Z)	ADD000020
	DIMENSION A(1),B(1),C(1),NA(2),NB(2),NC(2)	ADD000030
3	IF( (NA(1) .NE. NB(1)) .OR. (NA(2) .NE. NB(2)) ) GO TO 999	ADD000040
4	NC(1)=NA(1)	ADD000050
5	NC(2)=NA(2)	ADD000060
6	L=NA(1)*NA(2)	ADD000070
7	IF( NA(1) .LT. 1 .OR. L .LT. 1 ) GO TO 999	ADD000080
	DO 300 I=1,L	ADD000090
300	C(I)=A(I)+B(I)	ADD000100
10	GO TO 1000	ADD000110
999	CALL LNCNT (1)	ADD000120
	WRITE(6,50) NA,NB	ADD000130
13	50 FORMAT (' DIMENSION ERROR IN ADD      NA=',2I6,5X,'NB=',2I6)	ADD000140
14	1000 RETURN	ADD000150
	END	ADD000160

	SUBROUTINE SUBT(A,NA,B,NB,C,NC)	SUB00010
	IMPLICIT REAL*8 (A-H,O-Z)	SUB00020
2	DIMENSION A(1),B(1),C(1),NA(2),NB(2),NC(2)	SUB00030
3	IF((NA(1).NE.NB(1)).OR.(NA(2).NE.NB(2))) GO TO 999	SUB00040
	NC(1)=NA(1)	SUB00050
	NC(2)=NA(2)	SUB00060
6	L=NA(1)*NA(2)	SUB00070
	IF( NA(1) .LT. 1 .OR. L .LT. 1 ) GO TO 999	SUB00080
	DO 300 I=1,L	SUB00090
9	300 C(I)=A(I)-B(I)	SUB00100
10	GO TO 1000	SUB00110
11	999 CALL LNCNT (1)	SUB00120
12	WRITE(6,50) NA,NB	SUB00130
13	50 FORMAT (' DIMENSION ERROR IN SUBT    NA=',2I6,5X,'NB=',2I6)	SUB00140
	1000 RETURN	SUB00150
	END	SUB00160



0	SUBROUTINE MULT(A,NA,B,NB,C,NC)	MUL0001
1	IMPLICIT REAL*8 (A-H,O-Z)	MUL0002
2	DIMENSION A(1),B(1),C(1),NA(2),NB(2),NC(2)	MUL0003
3	NC(1) = NA(1)	MUL0004
4	NC(2) = NB(2)	MUL0005
5	IF(NA(2).NE.NB(1)) GO TO 999	MUL0006
6	NAR = NA(1)	MUL0007
7	NAC = NA(2)	MUL0008
8	NBC = NB(2)	MUL0009
9	NAA=NAR*NAC	MUL0010
10	NBB=NAR*NBC	MUL0011
11	IF ( NAR .LT. 1 .OR. NAA .LT. 1 .OR. NBB .LT. 1 ) GO TO 999	MUL0012
12	IR = 0	MUL0013
13	IK=NAC	MUL0014
14	DO 350 K=1,NBC	MUL0015
15	IK = IK + NAC	MUL0016
16	DO 350 J=1,NAR	MUL0017
17	IR=IR+1	MUL0018
18	IB=IK	MUL0019
19	JI=J+NAR	MUL0020
20	V1=0.0	MUL0021
21	DO 300 I=1,NAC	MUL0022
22	JI = JI + NAR	MUL0023
23	IB=IB+1	MUL0024
24	V3=A(JI)	MUL0025
25	V4=B(IB)	MUL0026
26	V2=V3+V4	MUL0027
27	V1=V1+V2	MUL0028
28	300 CONTINUE	MUL0029
29	C(IR)=V1	MUL0030
30	350 CONTINUE	MUL0031
31	GO TO 1000	MUL0032
32	999 CALL LNCNT (1)	MUL0033
33	WRITE(6,500) (NA(I),I=1,2),(NB(I),I=1,2)	MUL0034
34	500 FORMAT (' DIMENSION ERROR IN MULT NA=',2I6,5X,'NB=',2I6)	MUL0035
35	1000 RETURN	MUL0036
36	END	MUL0037

0	SUBROUTINE MAXEL(A,NA,ELMAX)	MAX0001
1	IMPLICIT REAL*8 (A-H,O-Z)	MAX0002
2	DIMENSION A(1),NA(2)	MAX0003
3 C		MAX0004
4	N = NA(1)*NA(2)	MAX0005
5 C		MAX0006
6	ELMAX = DABS( A(1) )	MAX0007
7	DO 100 I = 2,N	MAX0008
8	ELMAXI = DABS( A(1) )	MAX0009
9	IF( ELMAXI.GT.ELMAX) ELMAX=ELMAXI	
10	100 CONTINUE	MAX0011
11 C		MAX0012
12	RETURN	MAX0013
13	END	MAX0014

0	SUBROUTINE NORMS(MAXROW,M,N,A,IOPT,RLNORM)	NOR0001
1	IMPLICIT REAL*8 (A-H,O-Z)	NOR0002
2	DIMENSION A(1)	NOR0003
3	C	NOR0004
4	C INITIALIZATION	NOR0005
5	C	NOR0006
6	RLNORM=0.	NOR0007
7	SUM=0.	NOR0008
8	I=MAXROW	NOR0009
9	C	NOR0010
10	C TRANSFER TO APPROPRIATE LOOP TO COMPUTE THE DESIRED NORM	NOR0011
11	C	NOR0012
12	IF(IOPT-2)5,20,30	NOR0013
13	C	NOR0014
14	C THIS LOOP COMPUTES THE ONE-NORM	NOR0015
15	C	NOR0016
16	5 DO 15 K=1,N	NOR0017
17	I=I+MAXROW	NOR0018
18	DO 10 J=1,M	NOR0019
19	L=I+J	NOR0020
20	10 SUM=0ABS(A(L))+SUM	NOR0021
21	IF(SUM.GT.RLNORM)RLNORM=SUM	NOR0022
22	15 SUM=0.	NOR0023
23	RETURN	NOR0024
24	C	NOR0025
25	C THIS LOOP COMPUTES THE EUCLIDEAN NORM	NOR0026
26	C	NOR0027
27	20 DO 25 K=1,N	NOR0028
28	I=I+MAXROW	NOR0029
29	DO 25 J=1,M	NOR0030
30	L=I+J	NOR0031
31	SUM=A(L)	NOR0032
32	25 RLNORM=SUM*SUM+RLNORM	NOR0033
33	RLNORM=DSQRT(RLNORM)	NOR0034
34	RETURN	NOR0035
35	C	NOR0036
36	C THIS LOOP COMPUTES THE INFINITY-NORM	NOR0037
37	C	NOR0038
38	30 DO 40 J=1,M	NOR0039
39	L=I+J	NOR0040
40	DO 35 K=1,N	NOR0041
41	L=L+MAXROW	NOR0042
42	35 SUM=0ABS(A(L))+SUM	NOR0043
43	IF(SUM.GT.RLNORM)RLNORM=SUM	NOR0044
44	40 SUM=0.0	NOR0045
45	RETURN	NOR0046
46	END	NOR0047

0	SUBROUTINE JUXTC(A,NA,B,NB,C,NC)	JUX0001
1	IMPLICIT REAL*8 (A-H,O-Z)	JUX0002
2	DIMENSION A(1),B(1),C(1),NA(2),NB(2),NC(2)	JUX0003
3	IF (NA(1).NE.NB(1)) GO TO 600	JUX0004
4	NC(1)=NA(1)	JUX0005
5	NC(2)=NA(2)+NB(2)	JUX0006
6	L=NA(1)+NA(2)	JUX0007
7	NNC=NC(1)+NC(2)	JUX0008
8	IF( NA(1) .LT. 1 .OR. L .LT. 1 ) GO TO 600	JUX0009
9	IF( NC(2) .LT. 1 ) GO TO 600	JUX0010
10	MS=NA(1)+NA(2)	JUX0011
11	DO 10 I=1,MS	JUX0012
12	10 C(I)=A(I)	JUX0013
13	MBS=NA(1)+NB(2)	JUX0014
14	DO 20 I=1,MBS	JUX0015
15	J=MS+I	JUX0016
16	20 C(J)=B(I)	JUX0017
17	RETURN	JUX0018
18	600 CALL LNCNT(1)	JUX0019
19	WRITE (6,1600) NA,NB	JUX0020
20	1600 FORMAT (' DIMENSION ERROR IN JUXTC, NA=',2I6,5X,'NB=',2I6)	JUX0021
21	RETURN	JUX0022
22	END	JUX0023

0	SUBROUTINE JUXTR(A,NA,B,NB,C,NC)	JUX0001
1	IMPLICIT REAL*8 (A-H,O-Z)	JUX0002
2	DIMENSION A(1),B(1),C(1),NA(2),NB(2),NC(2)	JUX0003
3	IF(NA(2).NE.NB(2))GO TO 600	JUX0004
4	NC(2)=NA(2)	JUX0005
5	NC(1)=NA(1)+NB(1)	JUX0006
6	L=NA(1)+NA(2)	JUX0007
7	IF( NA(1) .LT. 1 .OR. L .LT. 1 ) GO TO 600	JUX0008
8	IF( NC(2) .LT. 1 ) GO TO 600	JUX0009
9	MCA=NA(2)	JUX0010
10	MRA=NA(1)	JUX0011
11	MRB=NB(1)	JUX0012
12	MRC=NC(1)	JUX0013
13	DO 10 I=1,MCA	JUX0014
14	DO 10 J=1,MRA	JUX0015
15	K=J+MRA*(I-1)	JUX0016
16	L=J+MRC*(I-1)	JUX0017
17	10 C(L)=A(K)	JUX0018
18	DO 20 I=1,MCA	JUX0019
19	DO 20 J=1,MRB	JUX0020
20	K=J+MRB*(I-1)	JUX0021
21	L=MRA+J+MRC*(I-1)	JUX0022
22	20 C(L)=B(K)	JUX0023
23	RETURN	JUX0024
24	600 CALL LNCNT(1)	JUX0025
25	WRITE(6,1600) NA,NB	JUX0026
26	1600 FORMAT(' DIMENSION ERROR IN JUXTR, NA=',2I6,5X,'NB=',2I6)	JUX0027
27	RETURN	JUX0028
28	END	JUX0029

0	SUBROUTINE FACTOR(Q,NQ,D,ND,IOP,IAC,DUMMY)	FAC0001
1	IMPLICIT REAL*8 (A-H,O-Z)	FAC0002
2	DIMENSION Q(1),D(1),DUMMY(1)	FAC0003
3	DIMENSION NQ(2),ND(2),NDUM(2)	FAC0004
4	IOP = 2	FAC0005
5	N = NQ(1)	FAC0006
6	M = N**2	FAC0007
7	N1 = M + 1	FAC0008
8	N2 = N1 + N	FAC0009
9	C	FAC0010
10	CALL EQUATE(Q,NQ,DUMMY,NQ)	FAC0011
11	CALL SNVDEC(IOP,N,N,N,N,DUMMY,NOS,B,IAC,ZTEST,DUMMY(N1),D,IRANK,	FAC0012
12	1PLUS,IERR)	FAC0013
13	IF( IERR .EQ. 0 ) GO TO 200	FAC0014
14	CALL LNCNT(5)	FAC0015
15	IF( IERR .GT. 0 ) PRINT 100,IERR	FAC0016
16	IF( IERR .EQ. -1) PRINT 150,ZTEST,IRANK	FAC0017
17	100 FORMAT(//,' IN FACTOR , SNVDEC HAS FAILED TO CONVERGE TO THE ',I4,	FAC0018
18	1' SINGULAR VALUE AFTER 30 ITERATIONS')	FAC0019
19	150 FORMAT(//,' IN FACTOR, THE MATRIX Q SUBMITTED TO SNVDEC IS CLOSE TO	FAC0020
20	10 A MATRIX OF LOWER RANK USING ZTEST = ',D16.8,/,', IF THE ACCURACY	FAC0021
21	2 IS REDUCED THE RANK MAY ALSO BE REDUCED',/,', CURRENT RANK = ',I4)	FAC0022
22	NDUM(1)=N	FAC0023
23	NDUM(2)=1	FAC0024
24	IF(IERR .EQ. -1) CALL PRNT(DUMMY(N1),NDUM,4H\$NVL,1)	FAC0025
25	IF( IERR .GT. 0 ) RETURN	FAC0026
26	C	FAC0027
27	200 CONTINUE	FAC0028
28	NDUM(1) = N	FAC0029
29	C	FAC0030
30	DO 250 J = 1,N	FAC0031
31	M1 = (J-1)*N + 1	FAC0032
32	M2 = J*N	FAC0033
33	DO 250 I = M1,M2	FAC0034
34	K = N2+I-1	FAC0035
35	L = N1+J-1	FAC0036
36	IF( DUMMY(L) .EQ. 0.0) GO TO 300	FAC0037
37	DUMMY(K) = DSQRT(DUMMY(L))*DUMMY(I)	FAC0038
38	250 CONTINUE	FAC0039
39	NDUM(2)=N	FAC0040
40	GO TO 350	FAC0041
41	C	FAC0042
42	300 NDUM(2) = J - 1	FAC0043
43	350 CONTINUE	FAC0044
44	IF( DUMMY(N2) .LT. 0.0 ) CALL SCALE(DUMMY(N2),NDUM,DUMMY(N2),NDUM,	FAC0045
45	1-1.0)	FAC0046
46	CALL TRANP(DUMMY(N2),NDUM,D,ND)	FAC0047
47	C	FAC0048
48	IF( IOP .EQ. 0 ) RETURN	FAC0049
49	CALL LNCNT(4)	FAC0050
50	PRINT 400	FAC0051
51	400 FORMAT(//,' FACTOR Q AS (D TRANSPOSE)XD ',/)	FAC0052
52	CALL PRNT(Q,NQ,4H Q ,1)	FAC0053
53	CALL PRNT(D,ND,4H D ,1)	FAC0054
54	CALL MULT(DUMMY(N2),NDUM,D,ND,DUMMY,NQ)	FAC0055
55	CALL PRNT(DUMMY,NQ,4HDTXD,1)	FAC0056
56	C	FAC0057
57	RETURN	FAC0058
58	END	FAC0059

0		SUBROUTINE EIGEN(MAX, N, A, ER, EI, ISV, ILV, V, WK, IERR)	EIG0001
1		IMPLICIT REAL*8 (A-H,O-Z)	EIG0002
2		DIMENSION A(MAX,N),ER(N),EI(N),V(MAX,1),WK(N,1)	EIG0003
3		INTEGER INT(20)	EIG0004
4		LOGICAL*1 SELECT(25)	EIG0005
5	C		EIG0006
6	C	PRELIMINARY REDUCTION	EIG0007
7	C		EIG0008
8		CALL BALANC (MAX,N,A,LOW,IGH,WK)	EIG0009
9		CALL ELMHES (MAX,N,LOW,IGH,A,INT(1))	EIG0010
10		IV = ISV + ILV	EIG0011
11		IF (IV .NE. 0) GO TO 10	EIG0012
12	C		EIG0013
13	C	COMPUTE ALL EIGENVALUES AND NO EIGENVECTORS	EIG0014
14	C		EIG0015
15		CALL HQR (MAX,N,LOW,IGH,A,ER,EI,IERR)	EIG0016
16		IF (IERR .NE. 0) GO TO 260	EIG0017
17		DO 5 I=1,N	EIG0018
18		WK(I,1) = ER(I)	EIG0019
19		WK(I,2) = EI(I)	EIG0020
20		WK(I,3) = ER(I)**2 + EI(I)**2	EIG0021
21	5	CONTINUE	EIG0022
22		IC = 0	EIG0023
23		GO TO 190	EIG0024
24	10	CONTINUE	EIG0025
25	C		EIG0026
26	C	SAVE A MATRIX FOR INVERSE ITERATION AND INITIALIZE WK(I,4)	EIG0027
27	C	ARRAY WHICH WILL BE A LOGICAL ARRAY IN CALLED SUBROUTINES	EIG0028
28	C		EIG0029
29		DO 20 I=1,N	EIG0030
30		SELECT(I)=.FALSE.	EIG0031
31		JS = 1	EIG0032
32		IF (I .GE. 3) JS = I-1	EIG0033
33		DO 20 J=JS,N	EIG0034
34		WK(I,J+5) = A(I,J)	EIG0035
35	20	CONTINUE	EIG0036
36	C		EIG0037
37	C	COMPUTE ALL EIGENVALUES (UNORDERED)	EIG0038
38	C		EIG0039
39		CALL HQR (N,N,LOW,IGH,WK(1,6),ER,EI,IERR)	EIG0040
40		IF (IERR .NE. 0) GO TO 260	EIG0041
41		DO 30 I=1,N	EIG0042
42		WK(I,3) = ER(I)**2 + EI(I)**2	EIG0043
43	30	CONTINUE	EIG0044
44		IF (ILV .EQ. 0) GO TO 60	EIG0045
45	C		EIG0046
46	C	FIND LARGEST ILV EIGENVALUES AND FLAG THEM	EIG0047
47	C		EIG0048
48		DO 50 I=1,ILV	EIG0049
49		P = -1.00	EIG0050
50		DO 40 J=1,N	EIG0051
51		IF (WK(J,3) .LE. P) GO TO 40	EIG0052
52		K = J	EIG0053
53		P = WK(J,3)	EIG0054
54	40	CONTINUE	EIG0055
55		SELECT(K)=.TRUE.	EIG0056
56		WK(K,3) = -WK(K,3)	EIG0057
57	50	CONTINUE	EIG0058
58		IF (EI(K) .EQ. 0.) GO TO 60	EIG0059
59		IF (EI(K) .GT. 0.) GO TO 55	EIG0060
60		IF (SELECT(K-1))GO TO 60	EIG0061
61		ILV = ILV+1	EIG0062
62		SELECT(K-1)=.TRUE.	EIG0063

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53		GO TO 60	EIG0064
54	55	CONTINUE	EIG0065
55		IF (.NOT.SELECT(K+1)) ILV = ILV+1	EIG0066
56	60	CONTINUE	EIG0067
57		IF (ISV .EQ. 0) GO TO 90	EIG0068
58	C		EIG0069
59	C	FIND SMALLEST ISV EIGENVALUES AND FLAG THEM	EIG0070
70	C		EIG0071
71		DO 65 I=1,N	EIG0072
72		WK(I,3) = DARS(WK(I,3))	EIG0073
73	65	CONTINUE	EIG0074
74		DO 80 I=1,ISV	EIG0075
75		P = 1.074	EIG0076
76		DO 70 J=1,N	EIG0077
77		IF (WK(J,3) .GE. P) GO TO 70	EIG0078
78		K = J	EIG0079
79		P = WK(J,3)	EIG0080
80	70	CONTINUE	EIG0081
81		SELECT(K)=.TRUE.	EIG0082
82		WK(K,3) = 1.074	EIG0083
83	80	CONTINUE	EIG0084
84		IF (EI(K) .EQ. 0.) GO TO 90	EIG0085
85		IF (EI(K) .GT. 0.) GO TO 85	EIG0086
86		IF (SELECT(K-1)) GO TO 90	EIG0087
87		ISV = ISV+1	EIG0088
88		SELECT(K-1)=.TRUE.	EIG0089
89		GO TO 90	EIG0090
90	85	CONTINUE	EIG0091
91		IF (.NOT.SELECT(K+1)) ISV = ISV+1	EIG0092
92	90	CONTINUE	EIG0093
93	C		EIG0094
94	C	FIND EIGENVECTORS FOR FLAGGED EIGENVALUES	EIG0095
95	C		EIG0096
96		CALL INVIT (MAX,N,A,ER,EI,SELECT,N,M,V,IERR,WK(1,6),WK(1,3),	EIG0097
97	1	WK(1,5))	EIG0098
98	C		EIG0099
99	C	BACK TRANSFORM EIGENVECTORS TO ORIGINAL MATRIX	EIG0100
100	C		EIG0101
101		CALL ELMBAK (MAX,LOW,IGH,A,INT(1),M,V)	EIG0102
102		CALL BALBAK (MAX,N,LOW,IGH,WK,M,V)	EIG0103
103	C		EIG0104
104	C	SEPARATE FLAGGED EIGENVALUES FROM UNFLAGGED EIGENVALUES	EIG0105
105	C		EIG0106
106		IV = ISV + ILV	EIG0107
107		IF (IV .LE. N) GO TO 100	EIG0108
108		ILV = N-ISV	EIG0109
109		IV = N	EIG0110
110	100	CONTINUE	EIG0111
111		IC = 0	EIG0112
112		JC = IV	EIG0113
113		DO 150 I=1,N	EIG0114
114		IF (SELECT(I)) GO TO 120	EIG0115
115		IF (EI(I) .GE. 0.) GO TO 110	EIG0116
116		IF (SELECT(I-1)) GO TO 120	EIG0117
117	110	CONTINUE	EIG0118
118		JC = JC+1	EIG0119
119		WK(JC,1) = ER(I)	EIG0120
120		WK(JC,2) = EI(I)	EIG0121
121		KC = JC	EIG0122
122		GO TO 130	EIG0123
123	120	CONTINUE	EIG0124
124		IC = IC+1	EIG0125
125		WK(IC,1) = ER(I)	EIG0126



126		WK(IC,2) = EI(I)	EIG012
127		KC = IC	EIG012
128	130	CONTINUE	EIG012
129		WK(KC,3) = ER(I)**2 + EI(I)**2	EIG013
130	150	CONTINUE	EIG013
131	C		EIG013
132	C	NORMALIZE VECTORS TO UNIT LENGTH AND STORE FOR REORDERING	EIG013
133	C		EIG013
134		J = 0	EIG013
135	151	CONTINUE	EIG013
136		J = J+1	EIG013
137		IF (WK(J,2) .NE. 0.) GO TO 154	EIG013
138		SUM = 0.	EIG013
139		DO 152 I=1,N	EIG014
140		SUM = SUM + V(I,J)**2	EIG014
141	152	CONTINUE	EIG014
142		IF (SUM .EQ. 0.) GO TO 158	EIG014
143		SUM = DSQRT(SUM)	EIG014
144		DO 153 I=1,N	EIG014
145		WK(I,J+4) = V(I,J)/SUM	EIG014
146	153	CONTINUE	EIG014
147		GO TO 158	EIG014
148	154	CONTINUE	EIG014
149		JP1 = J+1	EIG015
150		SUM = 0.	EIG015
151		DO 155 I=1,N	EIG015
152		SUM = SUM + V(I,J)**2 + V(I,JP1)**2	EIG015
153	155	CONTINUE	EIG015
154		IF (SUM .EQ. 0.) GO TO 157	EIG015
155		SUM = DSQRT(SUM)	EIG015
156		DO 156 I=1,N	EIG015
157		WK(I,J+4) = V(I,J)/SUM	EIG015
158		WK(I,J+5) = V(I,JP1)/SUM	EIG015
159	156	CONTINUE	EIG016
160	157	CONTINUE	EIG016
161		J = JP1	EIG016
162	158	CONTINUE	EIG016
163		IF (J .LT. IV) GO TO 151	EIG016
164		IC = 0	EIG016
165		LC = 0	EIG016
166		IF (ISV .EQ. 0) GO TO 190	EIG016
167	C		EIG016
168	C	ORDER SMALLEST ISV EIGENVALUES AND EIGENVECTORS FOR OUTPUT	EIG016
169	C		EIG017
170		DO 190 I=1,ISV	EIG017
171		P = 1.D74	EIG017
172		DO 160 J=1,IV	EIG017
173		IF (WK(J,3) .GE. P) GO TO 160	EIG017
174		K = J	EIG017
175		P = WK(J,3)	EIG017
176	160	CONTINUE	EIG017
177		IC = IC+1	EIG017
178		LC = LC+1	EIG017
179		ER(IC) = WK(K,1)	EIG018
180		EI(IC) = WK(K,2)	EIG018
181		DO 170 J=1,N	EIG018
182		V(J,LC) = WK(J,K+4)	EIG018
183	170	CONTINUE	EIG018
184		WK(K,3) = 1.D74	EIG018
185	180	CONTINUE	EIG018
186	190	CONTINUE	EIG018
187		IF (IV .EQ. N) GO TO 220	EIG018
188	C		EIG018

89	C	ORDER UNFLAGGED EIGENVALUES FOR OUTPUT	EIG0190
90	C		EIG0191
91		IV1 = IV+1	EIG0192
92		IUF = N - IV	EIG0193
93		DO 210 I=1,IUF	EIG0194
94		P = 1.074	EIG0195
95		DO 200 J=IV1,N	EIG0196
96		IF (WK(J,3) .GE. P) GO TO 200	EIG0197
97		K = J	EIG0198
98		P = WK(J,3)	EIG0199
99	200	CONTINUE	EIG0200
100		IC = IC+1	EIG0201
201		ER(IC) = WK(K,1)	EIG0202
202		EI(IC) = WK(K,2)	EIG0203
103		WK(K,3) = 1.074	EIG0204
104	210	CONTINUE	EIG0205
205	220	CONTINUE	EIG0206
106		IF (ILV .EQ. 0) GO TO 260	EIG0207
107	C		EIG0208
208	C	ORDER LARGEST ILV EIGENVALUES AND EIGENVECTORS FOR OUTPUT	EIG0209
209	C		EIG0210
110		DO 250 I=1,ILV	EIG0211
211		P = 1.074	EIG0212
212		DO 230 J=1,IV	EIG0213
113		IF (WK(J,3) .GE. P) GO TO 230	EIG0214
114		K = J	EIG0215
215		P = WK(J,3)	EIG0216
116	230	CONTINUE	EIG0217
117		IC = IC+1	EIG0218
218		LC = LC+1	EIG0219
219		ER(IC) = WK(K,1)	EIG0220
120		EI(IC) = WK(K,2)	EIG0221
221		DO 240 J=1,N	EIG0222
222		V(J,LC) = WK(J,K+4)	EIG0223
123	240	CONTINUE	EIG0224
124		WK(K,3) = 1.074	EIG0225
225	250	CONTINUE	EIG0226
226	260	CONTINUE	EIG0227
127		RETURN	EIG0228
128		END	EIG0229

0	SUBROUTINE SYMPOD (MAXN,N,A,NRHS,B,IOP,IFAC,DETERM,ISCALE,P,IERR)	SYM0000
1	IMPLICIT REAL*8 (A-H,O-Z)	SYM0000
2	DIMENSION A(MAXN,N),B(MAXN,NRHS),P(N)	SYM0000
3 C		SYM0000
4	DATA R1,R2/1.00+75,1.00-75/	SYM0000
5 C		SYM0000
6 C	TEST FOR A SCALAR MATRIX (IF COEFFICIENT MATRIX IS A	SYM0000
7 C	SCALAR-- SOLVE AND COMPUTE DETERMINANT IF DESIRED)	SYM0000
8	IERR = 0	SYM0000
9	NM1 = N-1	SYM0001
10	IF (NM1 .GT. 0) GO TO 20	SYM0001
11 C		SYM0001
12	IF( A(1,1) .LE. 0.0 ) IERR = 1	SYM0001
13	ISCALE = 0	SYM0001
14	DETERM = A(1,1)	SYM0001
15	P(1) = 1.0/A(1,1)	SYM0001
16	DO 10 J=1,NRHS	SYM0001
17	B(1,J) = B(1,J)/DETERM	SYM0001
18	10 CONTINUE	SYM0001
19	RETURN	SYM0002
20 C		SYM0002
21 C	TEST TO DETERMINE IF CHOLESKY DECOMPOSITION OF COEFFICIENT	SYM0002
22 C	MATRIX IS DESIRED	SYM0002
23	20 IF (IFAC .EQ. 1) GO TO 160	SYM0002
24 C		SYM0002
25 C	INITIALIZE DETERMINANT EVALUATION PARAMETERS	SYM0002
26	DETERM=1.0	SYM0002
27	ISCALE=0	SYM0002
28 C		SYM0002
29 C	'LOOP' TO PERFORM CHOLESKY DECOMPOSITION ON THE COEF-	SYM0003
30 C	FICIENT MATRIX A (I.E. MATRIX A WILL BE DECOMPOSED INTO	SYM0003
31 C	THE PRODUCT OF A UNIT LOWER TRIANGULAR MATRIX (L), A	SYM0003
32 C	DIAGONAL MATRIX (D), AND THE TRANSPOSE OF L (LTRANSPOSE.)	SYM0003
33 C		SYM0003
34	30 DO 150 I=1,N	SYM0003
35	IM1 = I-1	SYM0003
36 C		SYM0003
37	DO 150 J=1,I	SYM0003
38	X = A(J,I)	SYM0003
39 C		SYM0004
40 C	DETERMINE IF ELEMENTS ARE ABOVE OR BELOW THE DIAGONAL	SYM0004
41	IF (I .GT. J) GO TO 110	SYM0004
42 C		SYM0004
43 C	USING THE DIAGONAL ELEMENTS OF MATRIX A, THIS SECTION	SYM0004
44 C	COMPUTES DIAGONAL MATRIX AND DETERMINES IF MATRIX A IS	SYM0004
45 C	SYMMETRIC POSITIVE DEFINITE	SYM0004
46	IF (IM1 .EQ. 0) GO TO 50	SYM0004
47	DO 40 K=1,IM1	SYM0004
48	Y = A(I,K)	SYM0004
49	A(I,K) = Y*P(K)	SYM0005
50	X = X - Y*A(I,K)	SYM0005
51	40 CONTINUE	SYM0005
52 C		SYM0005
53 C	TEST IF COEFFICIENT MATRIX IS POSITIVE DEFINITE	SYM0005
54	50 IF( X .LE. 0.0 ) IERR = 1	SYM0005
55 C		SYM0005
56 C	COMPUTE INVERSE OF DIAGONAL MATRIX D**-1 = 1/P	SYM0005
57	P(I) = 1.0 / X	SYM0005
58 C		SYM0005
59 C	TEST TO SEE IF DETERMINANT IS TO BE EVALUATED	SYM0006
60	IF (IOP .EQ. 0) GO TO 150	SYM0006
61 C		SYM0006
62 C		SYM0006

6	C	SCALE THE DETERMINANT (COMPUTE THE DETERMINANT EVALUATION	SYM0064
64	C	PARAMETERS DETERM AND ISCALE)	SYM0065
65		PIVOTI=X	SYM0066
66		60 IF(DABS(DETERM),LT,R1) GO TO 70	SYM0067
67		DETERM = DETERM*R2	SYM0068
68		ISCALE = ISCALE+1	SYM0069
69		GO TO 60	SYM0070
70		70 IF(DABS(DETERM),GT,R2) GO TO 80	SYM0071
71		DETERM = DETERM*R1	SYM0072
72		ISCALE = ISCALE-1	SYM0073
73		GO TO 70	SYM0074
74		80 IF(DABS(PIVOTI),LT,R1) GO TO 90	SYM0075
75		PIVOTI = PIVOTI*R2	SYM0076
76		ISCALE = ISCALE+1	SYM0077
77		GO TO 80	SYM0078
78		90 IF(DABS(PIVOTI),GT,R2) GO TO 100	SYM0079
79		PIVOTI = PIVOTI*R1	SYM0080
80		ISCALE = ISCALE-1	SYM0081
81		GO TO 90	SYM0082
82		100 DETERM = DETERM*PIVOTI	SYM0083
83		GO TO 150	SYM0084
84	C		SYM0085
85	C		SYM0086
86	C	USING THE LOWER TRIANGULAR ELEMENTS OF MATRIX A, THIS	SYM0087
87	C	SECTION COMPUTES THE UNIT LOWER TRIANGULAR MATRIX	SYM0088
88		110 JM1 = J-1	SYM0089
89		IF (JM1 .EQ. 0) GO TO 140	SYM0090
90		DO 120 K=1,JM1	SYM0091
91		X = X - A(I,K)*A(J,K)	SYM0092
92		120 CONTINUE	SYM0093
93	C		SYM0094
94		140 A(I,J) = X	SYM0095
95	C		SYM0096
96		150 CONTINUE	SYM0097
97	C		SYM0098
98	C	SECTION TO APPLY BACK SUBSTITUTION TO SOLVE L*Y = B FOR	SYM0099
99	C	UNIT LOWER TRIANGULAR MATRIX AND CONSTANT COLUMN VECTOR B	SYM0100
100	C		SYM0101
101		160 IF( IFAC .EQ. 2 ) RETURN	SYM0102
102		DO 180 I=2,N	SYM0103
103		IM1=I-1	SYM0104
104	C		SYM0105
105		DO 180 J=1,NRHS	SYM0106
106		X = B(I,J)	SYM0107
107	C		SYM0108
108		DO 170 K=1,IM1	SYM0109
109		X = X - A(I,K)*B(K,J)	SYM0110
110		170 CONTINUE	SYM0111
111	C		SYM0112
112		B(I,J) = X	SYM0113
113		180 CONTINUE	SYM0114
114	C		SYM0115
115	C	SECTION TO SOLVE (LTRANSPOSE)*X = (D**=-1)*Y FOR TRANSPOSE	SYM0116
116	C	OF UNIT LOWER TRIANGULAR MATRIX AND INVERSE OF DIAGONAL	SYM0117
117	C	MATRIX	SYM0118
118	C		SYM0119
119		Y = P(N)	SYM0120
120		DO 190 J=1,NRHS	SYM0121
121		B(N,J) = B(N,J)*Y	SYM0122
122		190 CONTINUE	SYM0123
123	C		SYM0124
124		200 I = NM1+1	SYM0125
125		Y = P(NM1)	SYM0126

126 C		SYM012
127	DO 220 J=1,NRMS	SYM012
128	X = A(NM1,J)*Y	SYM012
129 C		SYM013
130	DO 210 K=1,N	SYM013
131	X = X - A(K,NM1)*B(K,J)	SYM013
132	210 CONTINUE	SYM013
133 C		SYM013
134	B(NM1,J) = X	SYM013
135	220 CONTINUE	SYM013
136 C		SYM013
137 C		SYM013
138 C	TEST TO DETERMINE IF SOLUTIONS HAVE BEEN DETERMINED FOR	SYM013
139 C	ALL COLUMN VECTORS	SYM014
140	NM1 = NM1+1	SYM014
141	IF (NM1 .GT. 0) GO TO 200	SYM014
142 C		SYM014
143	RETURN	SYM014
144	END	SYM014

0	SUBROUTINE GELIM(NMAX,N,A,NRHS,B,IPIVOT,IFAC,WK,IERR)	GEL000
1	IMPLICIT REAL*4 (A-H,O-Z)	GEL000
2	DIMENSION A(NMAX,1),B(NMAX,1),IPIVOT(1),WK(1)	GEL000
3	IERR=0	GEL000
4 C		GEL000
5 C	TEST FOR L/U FACTORIZATION	GEL000
6 C		GEL000
7	IF(IFAC.EQ.1)GO TO 10	GEL000
8	CALL DETFAC(NMAX,N,A,IPIVOT,IFAC,DETERM,ISCALE,WK,IERR)	GEL000
9	IF(IERR.GT.0)RETURN	GEL001
10	IF (IFAC.EQ.2) DETA=DETERM*(10.**((100*ISCALE)))	
11	10 NM1=N-1	GEL001
12 C		GEL001
13 C	TEST FOR SCALAR A MATRIX	GEL001
14 C		GEL001
15	IF(NM1.GT.0)GO TO 40	GEL001
16	IF(A(1,1).EQ.0.)GO TO 30	GEL001
17	DO 20 I=1,NRHS	GEL001
18	20 B(1,I)=B(1,I)/A(1,1)	GEL001
19	IF (IFAC.EQ.2) WK(1)=DETA	
20	RETURN	GEL001
21	30 IERR=1	GEL002
22	RETURN	GEL002
23 C		GEL002
24	40 DO 100 M=1,NRHS	GEL002
25 C		GEL002
26 C	PIVOT THE M-TH COLUMN OF B MATRIX	GEL002
27 C		GEL002
28	DO 50 I=1,NM1	GEL002
29	KI=IPIVOT(I)	GEL002
30	P=B(KI,M)	GEL002
31	B(KI,M)=B(I,M)	GEL003
32	50 B(I,M)=P	GEL003
33 C		GEL003
34 C	FORWARD SUBSTITUTION	GEL003
35 C		GEL003
36	WK(1)=B(1,M)	GEL003
37 C		GEL003
38	DO 70 I=2,N	GEL003
39	IM1=I-1	GEL003
40	P=0.0	GEL003
41	DO 60 K=1,IM1	GEL004
42	60 P=P+A(I,K)*WK(K)	GEL004
43	70 WK(I)=B(I,M)-P	GEL004
44 C		GEL004
45 C	BACK SUBSTITUTION	GEL004
46 C		GEL004
47	B(N,M)=WK(N)/A(N,N)	GEL004
48 C		GEL004
49	DO 90 J=1,NM1	GEL004
50	I=N-J	GEL004
51	IP1=I+1	GEL005
52	P=WK(I)	GEL005
53	DO 80 K=IP1,N	GEL005
54	80 P=P-A(I,K)*B(K,M)	GEL005
55	90 B(I,M)=P/A(I,I)	GEL005
56 C		GEL005
57	100 CONTINUE	GEL005
58	IF (IFAC.EQ.2) WK(1)=DETA	
59	RETURN	GEL005
60	END	GEL005

0	SUBROUTINE SNVDEC(IOP,MD,ND,M,N,A,NOS,R,IAC,ZTEST,Q,V,IRANK,APLUS,	SNV000
1	IERR)	SNV000
2	IMPLICIT REAL*8 (A-H,O-Z)	SNV000
3	LOGICAL WITHU,WITHV	SNV000
4	DIMENSION A(MD,N),V(ND,N),Q(N),E(150)	SNV000
5	DIMENSION B(MD,NOS),APLUS(ND,M)	SNV000
6	C	SNV000
7	C	SNV000
8	C TEST FOR SCALAR OR VECTOR A	SNV000
9	C	SNV001
10	IF( N .GE. 2 ) GO TO 3000	SNV001
11	C	SNV001
12	IERR = 0	SNV001
13	ZTEST = 10.**(-IAC)	SNV001
14	SUM = 0.0	SNV001
15	DO 1000 I=1,M	SNV001
16	SUM = SUM + A(I,1)*A(I,1)	SNV001
17	1000 CONTINUE	SNV001
18	SUM = DSQRT(SUM)	SNV001
19	IRANK = 0	SNV002
20	IF( SUM .GT. ZTEST ) IRANK = 1	SNV002
21	Q(1) = SUM	SNV002
22	C	SNV002
23	IF( IOP .EQ. 1 ) RETURN	SNV002
24	V(1,1) = 1.0	SNV002
25	IF( IRANK .EQ. 0 ) GO TO 1200	SNV002
26	DO 1100 I = 1,M	SNV002
27	A(I,1) = A(I,1)/SUM	SNV002
28	1100 CONTINUE	SNV002
29	GO TO 1300	SNV003
30	1200 CONTINUE	SNV003
31	A(1,1) = 1.0	SNV003
32	1300 CONTINUE	SNV003
33	C	SNV003
34	IF( IOP .EQ. 2 ) RETURN	SNV003
35	IF( IOP .EQ. 4 ) GO TO 1850	SNV003
36	IF( IRANK .EQ. 0 ) GO TO 1600	SNV003
37	DO 1500 J = 1,NOS	SNV003
38	Z = 0	SNV003
39	DO 1400 I = 1,M	SNV004
40	Z = Z + A(I,1)*B(I,J)/SUM	SNV004
41	1400 CONTINUE	SNV004
42	B(1,J) = Z	SNV004
43	1500 CONTINUE	SNV004
44	GO TO 1800	SNV004
45	1600 CONTINUE	SNV004
46	DO 1700 J = 1,NOS	SNV004
47	B(1,J) = 0.0	SNV004
48	1700 CONTINUE	SNV004
49	1800 CONTINUE	SNV005
50	C	SNV005
51	IF( IOP .EQ. 3 ) RETURN	SNV005
52	1850 CONTINUE	SNV005
53	IF( IRANK .EQ. 0 ) GO TO 2000	SNV005
54	DO 1900 I = 1,M	SNV005
55	APLUS(1,I) = A(I,1)/SUM	SNV005
56	1900 CONTINUE	SNV005
57	RETURN	SNV005
58	2000 CONTINUE	SNV005
59	DO 2100 I=1,M	SNV006
60	APLUS(1,I) = 0.0	SNV006
61	2100 CONTINUE	SNV006
62	RETURN	SNV006

63 C		SNV006
64 C		SNV006
65	3000 CONTINUE	SNV006
66 C		SNV006
67 C		SNV006
68 C		SNV006
69	TOL=1.0D-60	SNV007
70	SIZE=0.0	SNV007
71	NPI=N+1	SNV007
72 C		SNV007
73 C	COMPUTE THE E-NORM OF MATRIX A AS ZERO TEST FOR SINGULAR VALUES.	SNV007
74 C		SNV007
75	SUM=0.0	SNV007
76	DO 500 I=1,M	SNV007
77	DO 500 J=1,N	SNV007
78	500 SUM = SUM + A(I,J)**2	SNV007
79	ZTEST = DSQRT(SUM)	SNV008
80	ZTEST = ZTEST*10.**(-IAC)	SNV008
81 C		SNV008
82	510 IF (IOP.NE.1) GO TO 515	SNV008
83	WITHU=.FALSE.	SNV008
84	WITHV=.FALSE.	SNV008
85	GO TO 520	SNV008
86	515 WITHU=.TRUE.	SNV008
87	WITHV=.TRUE.	SNV008
88	520 CONTINUE	SNV008
89	G = 0.0	SNV009
90	X = 0.0	SNV009
91	DO 30 I = 1,N	SNV009
92 C		SNV009
93 C	HOUSEHOLDER REDUCTION TO BIDIAGONAL FORM.	SNV009
94 C		SNV009
95	E(I) = G	SNV009
96	S = 0.0	SNV009
97	L = I+1	SNV009
98 C		SNV009
99 C	ANNIHILATE THE I-TH COLUMN BELOW DIAGONAL.	SNV010
100 C		SNV010
101	DO 3 J = I,M	SNV010
102	3 S = S + A(J,I)**2	SNV010
103	G = 0.0	SNV010
104	IF(S.LT. TOL) GO TO 10	SNV010
105	G = DSQRT(S)	SNV010
106	F = A(I,I)	SNV010
107	IF(F.GE. 0.0) G = -G	SNV010
108	H = F*G - S	SNV010
109	A(I,I) = F+G	SNV011
110	IF(I.EQ. N) GO TO 10	SNV011
111	DO 9 J = L,N	SNV011
112	S = 0.0	SNV011
113	DO 7 K = I,M	SNV011
114	7 S = S + A(K,I)*A(K,J)	SNV011
115	F = S/H	SNV011
116	DO 8 K = I,M	SNV011
117	8 A(K,J) = A(K,J) + F*A(K,I)	SNV011
118	9 CONTINUE	SNV011
119	10 G(I) = G	SNV012
120	IF(I.EQ. N) GO TO 20	SNV012
121 C		SNV012
122 C	ANNIHILATE THE I-TH ROW TO RIGHT OF SUPER-DIAG.	SNV012
123 C		SNV012
124	S = 0.0	SNV012
125	DO 11 J = L,N	SNV012



26	11	S = S + A(I,J)**2	SNV012
27		G = 0.0	SNV012
128		IF (S .LT. TOL) GO TO 20	SNV012
29		G = DSQRT(S)	SNV013
30		F = A(I,I+1)	SNV013
31		IF(F .GE. 0.0) G = -G	SNV013
132		H = F*G - S	SNV013
33		A(I,I+1) = F - G	SNV013
34		DO 15 J = L,N	SNV013
135	15	E(J) = A(I,J)/H	SNV013
36		DO 19 J = L,M	SNV013
37		S = 0.0	SNV013
138		DO 16 K = L,N	SNV013
139	16	S = S + A(J,K) * A(I,K)	SNV014
40		DO 17 K = L,N	SNV014
41	17	A(J,K) = A(J,K) + S*E(K)	SNV014
142	19	CONTINUE	SNV014
43	20	Y = DARS(Q(I)) + DARS(E(I))	SNV014
44		IF(Y .GT. SIZE) SIZE = Y	SNV014
145	30	CONTINUE	SNV014
146		IF(.NOT. WITHV) GO TO 41	SNV014
147	C		SNV014
148	C	ACCUMULATION OF RIGHT TRANSFORMATIONS.	SNV014
149	C		SNV015
50		DO 40 II = 1,N	SNV015
51		I = NP1 - II	SNV015
152		IF(I .EQ. N) GO TO 39	SNV015
153		IF(G .EQ. 0.0) GO TO 37	SNV015
154		H = A(I,I+1)*G	SNV015
155		DO 32 J = L,N	SNV015
156	32	V(J,I) = A(I,J)/H	SNV015
157		DO 36 J = L,N	SNV015
158		S = 0.0	SNV015
159		DO 33 K = L,N	SNV016
160	33	S = S + A(I,K)*V(K,J)	SNV016
161		DO 34 K = L,N	SNV016
162	34	V(K,J) = V(K,J) + S*V(K,I)	SNV016
163	36	CONTINUE	SNV016
164	37	DO 38 J = L,N	SNV016
165		V(I,J) = 0.0	SNV016
166	38	V(J,I) = 0.0	SNV016
167	39	V(I,I) = 1.0	SNV016
168		G = E(I)	SNV016
169	40	L = I	SNV017
170	41	CONTINUE	SNV017
171		IF(.NOT. WITHU) GO TO 53	SNV017
172	C		SNV017
173	C	ACCUMULATION OF LEFT TRANSFORMATIONS.	SNV017
174	C		SNV017
175		DO 52 II = 1,N	SNV017
176		I = NP1 - II	SNV017
177		L = I + 1	SNV017
178		G = Q(I)	SNV017
179		IF(I .EQ. N) GO TO 43	SNV018
180		DO 42 J = L,N	SNV018
181	42	A(I,J) = 0.0	SNV018
182	43	CONTINUE	SNV018
183		IF(G .EQ. 0.0) GO TO 49	SNV018
184		IF(I .EQ. N) GO TO 47	SNV018
185		H = A(I,I)*G	SNV018
186		DO 46 J = L,N	SNV018
187		S = 0.0	SNV018
188		DO 44 K = L,M	SNV018

189	44	S = S + A(K,I)*A(K,J)	SNV019
190		F = S/H	SNV019
191		DO 45 K = I,M	SNV019
192	45	A(K,J) = A(K,J) + F*A(K,I)	SNV019
193	46	CONTINUE	SNV019
194	47	DO 48 J = I,M	SNV019
195	48	A(J,I) = A(J,I)/G	SNV019
196		GO TO 51	SNV019
197	49	DO 50 J = I,M	SNV019
198	50	A(J,I) = 0.0	SNV019
199	51	A(I,I) = A(I,I) + 1.0	SNV020
200	52	CONTINUE	SNV020
201	53	CONTINUE	SNV020
202	C		SNV020
203	C	DIAGONALIZATION OF BIDIAGONAL FORM.	SNV020
204	C		SNV020
205		DO 100 KK=1,N	SNV020
206		K=NP1-KK	SNV020
207		ITCNT=0	SNV020
208		KP1=K+1	SNV020
209	C		SNV021
210	C	TEST F SPLITTING.	SNV021
211	C		SNV021
212	59	CONTINUE	SNV021
213		DO 60 LL=1,K	SNV021
214		L=KP1-LL	SNV021
215		IF((SIZE+DABS(E(L))),EQ,SIZE) GO TO 64	SNV021
216		LM1=L-1	SNV021
217		IF((SIZE+DABS(Q(LM1))),EQ,SIZE) GO TO 61	SNV021
218	60	CONTINUE	SNV021
219	C		SNV022
220	C	CANCELLATION OF E(L) IF L .GT. 1.	SNV022
221	C		SNV022
222	61	C=0.0	SNV022
223		S=1.0	SNV022
224		L1=L-1	SNV022
225		DO 63 I=L,K	SNV022
226		F=S+E(I)	SNV022
227		E(I)=C+E(I)	SNV022
228		IF((SIZE+DABS(F)),EQ,SIZE) GO TO 64	SNV022
229		G=Q(I)	SNV023
230		Q(I)=DSQRT(F*F+G*G)	SNV023
231		H=Q(I)	SNV023
232		C=G/H	SNV023
233		S=-F/H	SNV023
234		IF(,NOT,WITHU) GO TO 63	SNV023
235		DO 62 J=1,M	SNV023
236		Y=A(J,L1)	SNV023
237		Z=A(J,I)	SNV023
238		A(J,L1)=Y*C+Z*S	SNV023
239		A(J,I)=-Y*S+Z*C	SNV024
240	62	CONTINUE	SNV024
241	C		SNV024
242	63	CONTINUE	SNV024
243	C		SNV024
244	C	TEST F CONVERGENCE.	SNV024
245	C		SNV024
246	64	Z=Q(K)	SNV024
247		IF(L,EQ,K) GO TO 75	SNV024
248		IF(ITCNT,LE,30) GO TO 65	SNV024
249		IFRR = KK	SNV025
250		RETURN	SNV025
251	65	ITCNT = ITCNT + 1	SNV025

252 C			3NV025
253 C	SHIFT FROM LOWER 2X2.		3NV025
254 C			3NV025
255	X=Q(L)		3NV025
256	Y=Q(K-1)		3NV025
257	G=E(K-1)		3NV025
258	H=E(K)		3NV025
259	F=((Y-Z)*(Y+Z)+(G-H)*(G+H))/(2.0*M*Y)		3NV025
260	G=DSQRT(F*F+1.0)		3NV026
261	IF(F.LT.0.0) G=-G		3NV026
262	F=((X-Z)*(X+Z)+H*(Y/(F+G)-H))/X		3NV026
263 C			3NV026
264 C			3NV026
265 C	NEXT QR TRANSFORMATION.		3NV026
266 C			3NV026
267	C=1.0		3NV026
268	S=1.0		3NV026
269	LP1=L+1		3NV027
270	DO 73 I=LP1,K		3NV027
271	G=E(I)		3NV027
272	Y=Q(I)		3NV027
273	H=S*G		3NV027
274	G=C*G		3NV027
275	Z=DSQRT(F*F+H*H)		3NV027
276	E(I-1)=Z		3NV027
277	C=F/Z		3NV027
278	S=H/Z		3NV027
279	F=X*C+G*S		3NV028
280	G=-X*S+G*C		3NV028
281	H=Y*S		3NV028
282	Y=Y*C		3NV028
283	IF(.NOT.WITHV) GO TO 70		3NV028
284	DO 68 J=1,N		3NV028
285	X=V(J,I-1)		3NV028
286	Z=V(J,I)		3NV028
287	V(J,I-1)=X*C+Z*S		3NV028
288	V(J,I)=-X*S+Z*C		3NV028
289	68 CONTINUE		3NV029
290 C			3NV029
291	70 Z=DSQRT(F*F+H*H)		3NV029
292	Q(I-1)=Z		3NV029
293	C=F/Z		3NV029
294	S=H/Z		3NV029
295	F=C*G+S*Y		3NV029
296	X=-S*G+C*Y		3NV029
297	IF(.NOT.WITHU) GO TO 73		3NV029
298	DO 72 J=1,M		3NV029
299	Y=A(J,I-1)		3NV030
300	Z=A(J,I)		3NV030
301	A(J,I-1)=Y*C+Z*S		3NV030
302	A(J,I)=-Y*S+Z*C		3NV030
303	72 CONTINUE		3NV030
304 C			3NV030
305 C			3NV030
306	73 E(L) = 0.0		3NV030
307	F(K)=F		3NV030
308	Q(K)=X		3NV030
309	GO TO 59		3NV031
310 C			3NV031
311 C	CONVERGENCE.		3NV031
312 C			3NV031
313	75 CONTINUE	A-31	3NV031
314	IF(Z.GE.0.0) GO TO 100		3NV031

31	Q(K)=Z	SNV03160
31	IF(.NOT.WITHV) GO TO 100	SNV03170
31	DO 76 J=1,N	SNV03180
31	76 V(J,K)=V(J,K)	SNV03190
31	100 CONTINUE	SNV03200
32	C	SNV03210
32	IERR=0	SNV03220
32	DO 240 II=2,N	SNV03230
32	I=II-1	SNV03240
32	K=I	SNV03250
32	P=Q(I)	SNV03260
32	DO 250 J=II,N	SNV03270
32	IF (Q(J).LE.P) GO TO 250	SNV03280
32	K=J	SNV03290
32	P=Q(J)	SNV03300
32	250 CONTINUE	SNV03310
33	C	SNV03320
33	IF (K.EQ.I) GO TO 240	SNV03330
33	Q(K) = Q(I)	SNV03340
33	Q(I) = P	SNV03350
33	C	SNV03360
33	IF(IOP.EQ.1) GO TO 240	SNV03370
33	C	SNV03380
33	DO 260 J=1,N	SNV03390
33	P=V(J,I)	SNV03400
33	V(J,I)=V(J,K)	SNV03410
33	V(J,K)=P	SNV03420
33	260 CONTINUE	SNV03430
33	C	SNV03440
33	DO 270 J=1,M	SNV03450
33	P=A(J,I)	SNV03460
33	A(J,I)=A(J,K)	SNV03470
33	A(J,K)=P	SNV03480
33	270 CONTINUE	SNV03490
33	C	SNV03500
33	280 CONTINUE	SNV03510
33	C	SNV03520
33	J=N	SNV03530
33	290 IF (Q(J).GT.ZTEST) GO TO 300	SNV03540
33	Q(J)=0.0	SNV03550
33	J=J-1	SNV03560
33	GO TO 290	SNV03570
33	300 IRANK =J	SNV03580
33	TEMP = ZTEST/Q(J)	SNV03590
33	IF (TEMP.GT..0625) IERR=-1	SNV03600
33	C	SNV03610
33	IF (IOP.LT.3) RETURN	SNV03620
33	IF(IOP.GT.3) GO TO 170	SNV03630
33	DO 160 L=1,NOS	SNV03640
33	DO 130 J=1,IRANK	SNV03650
33	SUM=0.0	SNV03660
33	DO 120 I=1,M	SNV03670
33	120 SUM =SUM + A(I,J)*B(I,L)	SNV03680
33	130 E(J)= SUM/Q(J)	SNV03690
33	C	SNV03700
33	DO 150 K=1,N	SNV03710
33	SUM=0.0	SNV03720
33	DO 140 I=1,IRANK	SNV03730
33	140 SUM =SUM + V(K,I)*E(I)	SNV03740
33	150 R(K,L)=SUM	SNV03750
33	160 CONTINUE	SNV03760
33	RETURN	SNV03770
33	170 DO 200 J=1,M	SNV03780

37	DO 100 I=1,N	SNV03790
37	SUM=0.0	SNV03800
380	DO 180 K=1,IRANK	SNV03810
381	180 SUM=SUM + V(I,K)*A(J,K)/Q(K)	SNV03820
381	190 APLUS(I,J)=SUM	SNV03830
381	200 CONTINUE	SNV03840
384 C		SNV03850
381	IF( IOP .EQ.4) RETURN	SNV03860
381	DO 230 K=1,NOS	SNV03870
387	DO 220 I=1,N	SNV03880
387	SUM=0.0	SNV03890
387	DO 210 J=1,M	SNV03900
390	210 SUM=SUM+ APLUS(I,J)*B(J,K)	SNV03910
391	220 E(I)=SUM	SNV03920
391	DO 225 I=1,N	SNV03930
391	225 B(I,K)=E(I)	SNV03940
394	230 CONTINUE	SNV03950
39	RETURN	SNV03960
39	END	SNV03970

0	SUBROUTINE SUM(A,NA,B,NB,C,NC,IOP,SYM,DUMMY)	SUM00010
1	IMPLICIT REAL*4 (A-H,O-Z)	SUM00020
2	DIMENSION A(1),B(1),C(1),DUMMY(1)	SUM00030
3	DIMENSION NA(2),NB(2),NC(2)	SUM00040
4	LOGICAL SYM	SUM00050
5	COMMON/CONV/SUMCV,RICTCV,SERCV,MAXSUM	SUM00060
6	IF( IOP .EQ. 0 ) GO TO 100	SUM00070
7	PRINT 50	SUM00080
8	50 FORMAT(/, ' LINEAR EQUATION SOLVER    X = AX + B ')	SUM00090
9	CALL PRNT(A,NA,4H A ,1)	SUM00100
10	IF( SYM ) GO TO 75	SUM00110
11	CALL PRNT(C,NC,4H C ,1)	SUM00120
12	GO TO 85	SUM00130
13	75 CONTINUE	SUM00140
14	PRINT 80	SUM00150
15	80 FORMAT(/, ' C = A TRANSPOSE ',/)	SUM00160
16	85 CONTINUE	SUM00170
17	CALL PRNT(B,NB,4H B ,1)	SUM00180
18	C	SUM00190
19	100 CONTINUE	SUM00200
20	NI = 1 + NA(1)*NC(1)	SUM00210
21	I=1	SUM00220
22	200 CONTINUE	SUM00230
23	CALL MULT(A,NA,B,NB,DUMMY,NB)	SUM00240
24	CALL MULT(DUMMY,NB,C,NC,DUMMY(N1),NB)	SUM00250
25	CALL MAXEL(B,NB,WNS)	SUM00260
26	CALL MAXEL(DUMMY(N1),NB,WNOX)	SUM00270
27	IF(WNS .GE. 1.) GO TO 225	SUM00280
28	IF( WNOX/WNS .LT. SUMCV ) GO TO 300	SUM00290
29	GO TO 235	SUM00300
30	225 IF( WNOX .LT. SUMCV ) GO TO 300	SUM00310
31	235 CONTINUE	SUM00320
32	CALL ADD(R,NB,DUMMY(N1),NB,B,NB)	SUM00330
33	CALL MULT(A,NA,A,NA,DUMMY,NA)	SUM00340
34	CALL EQUATE(DUMMY,NA,A,NA)	SUM00350
35	IF( SYM ) GO TO 245	SUM00360
36	CALL MULT(C,NC,C,NC,DUMMY,NC)	SUM00370
37	CALL EQUATE(DUMMY,NC,C,NC)	SUM00380
38	GO TO 250	SUM00390
39	245 CONTINUE	SUM00400
40	CALL TRANP(A,NA,C,NC)	SUM00410
41	250 CONTINUE	SUM00420
42	I=I+1	SUM00430
43	IF( I .LE. MAXSUM ) GO TO 200	SUM00440
44	CALL LNCNT(3)	SUM00450
45	PRINT 275,MAXSUM	SUM00460
46	275 FORMAT(/, ' IN SUM, THE SEQUENCE OF PARTIAL SUMS HAS EXCEEDED STAG	SUM00470
47	1 E',15, ' WITHOUT CONVERGENCE')	SUM00480
48	300 CONTINUE	SUM00490
49	IF(IOP .EQ. 0) RETURN	SUM00500
50	CALL PRNT(B,NB,4H X ,1)	SUM00510
51	RETURN	SUM00520
52	END	SUM00530

1	SUBROUTINE BILIN(A,NA,B,NB,C,NC,IOP,BETA,SYM,DUMMY)	BIL00010
2	IMPLICIT REAL*8 (A-H,O-Z)	BIL00020
3	DIMENSION A(1),B(1),C(1),DUMMY(1)	BIL00030
4	DIMENSION NA(2),NB(2),NC(2),NDUM(2)	BIL00040
5	DIMENSION IOP(2)	BIL00050
6	LOGICAL SYM	BIL00060
7	IF( IOP(1) .EQ. 0 ) GO TO 300	BIL00070
8	IF(SYM) GO TO 100	BIL00080
9	CALL LNCNT(3)	BIL00090
10	PRINT 50	BIL00100
11	50 FORMAT(//, ' LINEAR EQUATION SOLVER    AX + XB = C ')	BIL00110
12	CALL PRNT(A,NA,4M A ,1)	BIL00120
13	CALL PRNT(B,NB,4M B ,1)	BIL00130
14	GO TO 200	BIL00140
15	100 CONTINUE	BIL00150
16	CALL LNCNT(3)	BIL00160
17	PRINT 150	BIL00170
18	150 FORMAT(//, ' LINEAR EQUATION SOLVER    ( B TRANSPOSE ) X + XB = C ')	BIL00180
19	CALL TRNP(A,NA,DUMMY,NDUM)	BIL00190
20	CALL PRNT(DUMMY,NDUM,4M B ,1)	BIL00200
21	200 CONTINUE	BIL00210
22	CALL PRNT(C,NC,4M C ,1)	BIL00220
23	300 CONTINUE	BIL00230
24	C	BIL00240
25	IOPIT = 0	BIL00250
26	N=NA(1)**2	BIL00260
27	M=NB(1)**2	BIL00270
28	C	BIL00280
29	IF( IOP(2) .EQ. 0 ) GO TO 500	BIL00290
30	C	BIL00300
31	N1 = N + 1	BIL00310
32	CALL EQUATE(A,NA,DUMMY,NA)	BIL00320
33	N2 = N1 + NA(1)	BIL00330
34	N3 = N2 + NA(1)	BIL00340
35	ISV = 0	BIL00350
36	ILV = 0	BIL00360
37	NEVL = NA(1)	BIL00370
38	CALL EIGEN(NA(1),NA(1),DUMMY,DUMMY(N1),DUMMY(N2),ISV,ILV,V,DUMMY(NBIL00380	
39	13),IERR)	BIL00390
40	IF (IERR .EQ. 0) GO TO 350	BIL00400
41	CALL LNCNT(3)	BIL00410
42	PRINT 325,IERR	BIL00420
43	325 FORMAT(//, ' IN BILIN, THE ',I4, ' EIGENVALUE OF A HAS NOT BEEN DETRIL00430	
44	TERMINED AFTER 30 ITERATIONS')	BIL00440
45	IERR=1	BIL00450
46	CALL NORMS(NEVL,NEVL,NEVL,A,IERR,BETA)	BIL00460
47	BETA=2.*BETA	BIL00470
48	GO TO 385	BIL00480
49	350 CONTINUE	BIL00490
50	J= N1 + NEVL -1	BIL00500
51	K = N2 + NEVL -1	BIL00510
52	CO = DSQRT(DUMMY(N1)**2 + DUMMY(N2)**2)	BIL00520
53	CN = DSQRT(DUMMY(J)**2 + DUMMY(K)**2)	BIL00530
54	CD = DUMMY(J)-DUMMY(N1)	BIL00540
55	IF(CD .EQ. 0.0) GO TO 365	BIL00550
56	BETA = (DUMMY(N1)*CN-DUMMY(J)*CO)/CD	BIL00560
57	IF(BETA .LE. 0.0) GO TO 365	BIL00570
58	BETA = DSQRT(BETA)	BIL00580
59	GO TO 385	BIL00590
60	C	BIL00600
61	365 CONTINUE	BIL00610
62	C	BIL00620
63	BETA = 0.0	BIL00630

67	DO 375 I = 1, NEVL	BIL00640
68	J = N1 + I - 1	BIL00650
69	K = N2 + I - 1	BIL00660
70	IF(DUMMY(J) .GE. 0.0) GO TO 375	BIL00670
71	BETA = BETA + DSQRT(DUMMY(J)**2 + DUMMY(K)**2)	BIL00680
72	375 CONTINUE	BIL00690
73	BETA = BETA/NEVL	BIL00700
74	C	BIL00710
75	385 CONTINUE	BIL00720
76	C	BIL00730
77	IF( SYM ) GO TO 500	BIL00740
78	CALL EQUATE(B,NB,DUMMY,NB)	BIL00750
79	N1=N+1	BIL00760
80	N2 = N1 + NB(1)	BIL00770
81	N3 = N2 + NB(1)	BIL00780
82	NEVL = NB(1)	BIL00790
83	CALL EIGEN(NB(1),NB(1),DUMMY,DUMMY(N1),DUMMY(N2),ISV,ILV,V,DUMMY(NB(1),	BIL00800
84	13),IERR)	BIL00810
85	IF(IERR .EQ. 0) GO TO 450	BIL00820
86	CALL LNCNT(3)	BIL00830
87	PRINT 400,IERR	BIL00840
88	400 FORMAT(/, ' IN BILIN, THE ',I4,' EIGENVALUE OF B HAS NOT BEEN FOUND	BIL00850
89	10 AFTER 30 ITERATIONS')	BIL00860
90	IERR=1	BIL00870
91	CALL NORMS(NEVL,NEVL,NEVL,B,IERR,BETA1)	BIL00880
92	BETA1=2.*BETA1	BIL00890
93	GO TO 485	BIL00900
94	450 CONTINUE	BIL00910
95	J = N1 + NEVL - 1	BIL00920
96	K = N2 + NEVL - 1	BIL00930
97	CO = DSQRT(DUMMY(N1)**2 + DUMMY(N2)**2)	BIL00940
98	CN = DSQRT(DUMMY(J)**2 + DUMMY(K)**2)	BIL00950
99	CD = DUMMY(J)-DUMMY(N1)	BIL00960
100	IF(CD .EQ. 0.0) GO TO 465	BIL00970
101	BETA1 = (DUMMY(N1)*CN - DUMMY(J)*CO)/CD	BIL00980
102	IF(BETA1 .LE. 0.0) GO TO 465	BIL00990
103	BETA1 = DSQRT(BETA1)	BIL01000
104	GO TO 485	BIL01010
105	C	BIL01020
106	465 CONTINUE	BIL01030
107	C	BIL01040
108	BETA1 = 0.0	BIL01050
109	DO 475 I = 1, NEVL	BIL01060
110	J = N1 + I - 1	BIL01070
111	K = N2 + I - 1	BIL01080
112	IF(DUMMY(J) .GE. 0.0) GO TO 475	BIL01090
113	BETA1 = BETA1 + DSQRT(DUMMY(J)**2 + DUMMY(K)**2)	BIL01100
114	475 CONTINUE	BIL01110
115	BETA1 = BETA1/NEVL	BIL01120
116	C	BIL01130
117	485 CONTINUE	BIL01140
118	BETA = (BETA + BETA1)/2.	BIL01150
119	C	BIL01160
120	500 CONTINUE	BIL01170
121	C	BIL01180
122	IF( IOP(1) .EQ. 0 ) GO TO 520	BIL01190
123	CALL LNCNT(4)	BIL01200
124	PRINT 515,BETA	BIL01210
125	515 FORMAT(/, ' BETA = ',E16.8, /)	BIL01220
126	520 CONTINUE	BIL01230
127	C	BIL01240
128	N1 = N+1	BIL01250
129		BIL01260



124	CALL EQUATE(A,NA,DUMMY,NA)	BIL01270
125	CALL EQUATE(A,NA,DUMMY(N1),NA)	BIL01280
126	CALL SCALE(DUMMY,NA,DUMMY,NA,-1.)	BIL01290
129	L = -NA(1)	BIL01300
131	NAX = NA(1)	BIL01310
131	DO 525 I=1,NAX	BIL01320
132	L = L + NAX + 1	BIL01330
133	M1 = L + N	BIL01340
134	DUMMY(L) = BETA - A(L)	BIL01350
135	DUMMY(M1) = BETA + A(L)	BIL01360
136	525 CONTINUE	BIL01370
137	N2 = N1 + N	BIL01380
138	CALL EQUATE(C,NC,DUMMY(N2),NDUM)	BIL01390
139	NDUM(2) = NDUM(2) + NA(1)	BIL01400
140	N3 = N2 + NC(1)*NC(2)	BIL01410
141	GAM = -2.*BETA	BIL01420
142	C	BIL01430
143	IF( .NOT. SYM ) GO TO 600	BIL01440
144	C	BIL01450
145	CALL UNITY(DUMMY(N3),NA)	BIL01460
146	N4 = N3 + N	BIL01470
147	NDUM(2) = NDUM(2) + NA(1)	BIL01480
148	N5 = N4 + NA(1)	BIL01490
149	IFAC = 0	BIL01500
150	CALL GELIM(NA(1),NA(1),DUMMY,NDUM(2),DUMMY(N1),DUMMY(N4),IFAC,DUMM	BIL01510
151	Y(N5),IERR)	BIL01520
152	IF( IERR .EQ. 1 ) PRINT 625	BIL01530
153	CALL EQUATE(DUMMY(N1),NA,DUMMY,NA)	BIL01540
154	CALL EQUATE(DUMMY(N2),NC,C,NC)	BIL01550
155	CALL TRANSP(DUMMY,NA,DUMMY(N1),NA)	BIL01560
156	CALL TRANSP(DUMMY(N3),NA,DUMMY(N2),NA)	BIL01570
157	CALL MULT(C,NC,DUMMY(N2),NA,DUMMY(N3),NA)	BIL01580
158	CALL SCALE(DUMMY(N3),NC,C,NC,GAM)	BIL01590
159	C	BIL01600
160	C	BIL01610
161	CALL SUM(DUMMY,NA,C,NC,DUMMY(N1),NA,IOPTT,SYM,DUMMY(N2))	BIL01620
162	GO TO 700	BIL01630
163	600 CONTINUE	BIL01640
164	N4 = N3 + NA(1)	BIL01650
165	IFAC = 0	BIL01660
166	CALL GELIM(NA(1),NA(1),DUMMY,NDUM(2),DUMMY(N1),DUMMY(N3),IFAC,DUMM	BIL01670
167	Y(N4),IERR)	BIL01680
168	IF(IERR .EQ. 1 ) PRINT 625	BIL01690
169	625 FORMAT('/', ' IN BILIN, THE MATRIX (BETA)I - A IS SINGULAR, INCREAS	BIL01700
170	1E BETA ')	BIL01710
171	CALL EQUATE(DUMMY(N1),NA,DUMMY,NA)	BIL01720
172	CALL EQUATE(DUMMY(N2),NC,C,NC)	BIL01730
173	N2 = M + N	BIL01740
174	CALL EQUATE(B,NB,DUMMY(N1),NB)	BIL01750
175	CALL EQUATE(B,NB,DUMMY(N2),NB)	BIL01760
176	CALL SCALE(DUMMY(N1),NB,DUMMY(N1),NB,-1.0)	BIL01770
177	L = NB(1)	BIL01780
178	NAX = NB(1)	BIL01790
179	DO 650 I = 1, NAX	BIL01800
180	L = L + NAX + 1	BIL01810
181	L1 = L + N	BIL01820
182	M1 = L + N2 - 1	BIL01830
183	DUMMY(L1) = BETA - B(L)	BIL01840
184	DUMMY(M1) = BETA + B(L)	BIL01850
185	650 CONTINUE	BIL01860
186	C	BIL01870
187	N3 = N2 + M	BIL01880
188	CALL TRANSP(DUMMY(N1),NB,DUMMY(N3),NB)	BIL01890

189	CALL EQUATE(DUMMY(N3),NA,DUMMY(N1),NB)	BIL01900
190	CALL TRANSP(DUMMY(N2),NB,DUMMY(N3),NB)	BIL01910
191	CALL EQUATE(DUMMY(N3),NB,DUMMY(N2),NB)	BIL01920
192	CALL TRANSP(C,NC,DUMMY(N3),NDUM)	BIL01930
193	NSDUM = NDUM(2)	BIL01940
194	NDUM(2) = NDUM(2) + NB(2)	BIL01950
195	IFAC = 0	BIL01960
196	N4 = N3 + NC(1) * NC(2)	BIL01970
197	N5 = N4 + NB(1)	BIL01980
198	CALL GELIM(NB(1),NB(1),DUMMY(N1),NDUM(2),DUMMY(N2),DUMMY(N4),IFAC,	BIL01990
199	1DUMMY(N5),IERR)	BIL02000
200	IF(IERR .EQ. 1) PRINT 675	BIL02010
201	675 FORMAT(/, 'IN BILIN, THE MATRIX (BETA)I - B IS SINGULAR, INCREASE	BIL02020
202	1 BETA ')	BIL02030
203	CALL TRANSP(DUMMY(N2),NB,DUMMY(N1),NB)	BIL02040
204	NDUM(2) = NSDUM	BIL02050
205	CALL TRANSP(DUMMY(N3),NDUM,C,NC)	BIL02060
206	CALL SCALE(C,NC,C,NC,GAM)	BIL02070
207	N2 = N + M + 1	BIL02080
208	CALL SUM(DUMMY,NA,C,NC,DUMMY(N1),NB,IOPTT,SYM,DUMMY(N2))	BIL02090
209	C	BIL02100
210	700 CONTINUE	BIL02110
211	IF( IOP(1) .EQ. 0 ) RETURN	BIL02120
212	CALL PRNT(C,NC,4H X ,1)	BIL02130
213	RETURN	BIL02140
214	END	BIL02150

1	SUBROUTINE BARSTW(A,NA,B,NB,C,NC,IOP,SYM,EPSA,EPSE,DUMMY)	BAR00010
2	IMPLICIT REAL*8 (A-H,O-Z)	BAR00020
3	DIMENSION A(1),B(1),C(1),DUMMY(1)	BAR00030
4	DIMENSION NA(2),NB(2),NC(2),NDUM1(2),NDUM2(2),NDUM3(2),NDUM4(2)	BAR00040
5	LOGICAL SYM	BAR00050
6	IF ( IOP .EQ. 0 ) GO TO 250	BAR00060
7	IF(SYM) GO TO 100	BAR00070
8	CALL LNCNT(3)	BAR00080
9	PRINT 50	BAR00090
10	50 FORMAT(/, ' LINEAR EQUATION SOLVER      AX + XB = C ')	BAR00100
11	CALL PRNT(A,NA,4H A ,1)	BAR00110
12	CALL PRNT(B,NB,4H B ,1)	BAR00120
13	GO TO 200	BAR00130
14	100 CONTINUE	BAR00140
15	CALL LNCNT(3)	BAR00150
16	PRINT 150	BAR00160
17	150 FORMAT(/, ' LINEAR EQUATION SOLVER ( B TRANSPOSE )X + XB = C')	BAR00170
18	CALL TRNP(A,NA,DUMMY,NDUM1)	BAR00180
19	CALL PRNT(DUMMY,NDUM1,4H B ,1)	BAR00190
20	200 CONTINUE	BAR00200
21	CALL PRNT(C,NC,4H C ,1)	BAR00210
22	C	BAR00220
23	250 CONTINUE	BAR00230
24	CALL EQUATE(A,NA,DUMMY,NDUM1)	BAR00240
25	N1=(NA(1)**2)+1	BAR00250
26	N2=N1+NA(1)-1	BAR00260
27	DO 300 I=N1,N2	BAR00270
28	DUMMY(I)=0.0	BAR00280
29	300 CONTINUE	BAR00290
30	C	BAR00300
31	NDUM1(2)=NDUM1(2)+1	BAR00310
32	NDUM2(1)=1	BAR00320
33	NDUM2(2)=NDUM1(2)	BAR00330
34	N1=NDUM1(1)*NDUM1(2)+1	BAR00340
35	CALL NULL(DUMMY(N1),NDUM2)	BAR00350
36	LU=(NA(1)+1)**2 + 1	BAR00360
37	CALL JUXTA(DUMMY,NDUM1,DUMMY(N1),NDUM2,DUMMY(LU),NDUM3)	BAR00370
38	CALL EQUATE(DUMMY(LU),NDUM3,DUMMY,NDUM1)	BAR00380
39	N=NA(1)+1	BAR00390
40	C	BAR00400
41	IF(SYM ) GO TO 500	BAR00410
42	C	BAR00420
43	CALL EQUATE(B,NB,DUMMY(LU),NDUM2)	BAR00430
44	M1=LU+NB(1)**2	BAR00440
45	M2=M1+NB(1)-1	BAR00450
46	DO 400 I=M1,M2	BAR00460
47	DUMMY(I)=0.0	BAR00470
48	400 CONTINUE	BAR00480
49	C	BAR00490
50	NDUM2(2)=NDUM2(2)+1	BAR00500
51	NDUM3(1)=1	BAR00510
52	NDUM3(2)=NDUM2(2)	BAR00520
53	M1=NDUM2(1)*NDUM2(2)+LU	BAR00530
54	CALL NULL(DUMMY(M1),NDUM3)	BAR00540
55	M2=LU+(NB(1)+1)**2	BAR00550
56	CALL JUXTA(DUMMY(LU),NDUM2,DUMMY(M1),NDUM3,DUMMY(M2),NDUM4)	BAR00560
57	CALL EQUATE(DUMMY(M2),NDUM4,DUMMY(LU),NDUM2)	BAR00570
58	M=NB(1)+ 1	BAR00580
59	LN3 = LU	BAR00590
60	LU = LU + (NB(1)+1)**2	BAR00600
61	LV = LU + NA(1)**2	BAR00610
62	CALL AXPXA(DUMMY,DUMMY(LU),NA(1),N,NA(1),DUMMY(LN3),DUMMY(LV),NB(1)	BAR00620
63	1),M,NB(1),C,NC(1),EPSA,EPSE,FAIL)	BAR00630

63	GO TO 600	BAR00640
64	C	BAR00650
65	500 CONTINUE	BAR00660
66	CALL TRANP(DUMMY,NDUM1,DUMMY(LU),NDUM2)	BAR00670
67	CALL EQUATE(DUMMY(LU),NDUM2,DUMMY,NDUM1)	BAR00680
68	CALL ATXPXA(DUMMY,DUMMY(LU),C,NA(1),N,NA(1),NC(1),EPSA,NFAIL)	BAR00690
69	C	BAR00700
70	600 CONTINUE	BAR00710
71	IF(NFAIL.EQ.0) GO TO 700	BAR00720
72	CALL LNCNT(3)	BAR00730
73	PRINT 650	BAR00740
74	650 FORMAT(//,' IN BARSTN, EITHER THE SUBROUTINE AXPXB OR ATXPXA	BAR00750
75	IS UNABLE TO REDUCE A OR 4 TO SCHUR FORM')	BAR00760
76	RETURN	BAR00770
77	C	BAR00780
78	700 CONTINUE	BAR00790
79	C	BAR00800
80	IF(IOP.NE.0) CALL PRNT(C,NC,4H X,1)	BAR00810
81	RETURN	BAR00820
82	END	BAR00830

1	SUBROUTINE TESTSA(A,NA,ALPHA,DISC,STABLE,IOP,DUMMY)	TES00010
2	IMPLICIT REAL*8 (A-H,O-Z)	TES00020
3	DIMENSION A(1),DUMMY(1)	TES00030
4	DIMENSION NA(2),NDUM1(2),NDUM2(2)	TES00040
5	LOGICAL DISC,STABLE	TES00050
6	STABLE = .FALSE.	TES00060
7	C	TES00070
8	CALL EQUATE(A,NA,DUMMY,NA)	TES00080
9	N1= NA(1)**2 + 1	TES00090
10	N2= N1+NA(1)	TES00100
11	N3= N2+NA(1)	TES00110
12	ISV = 0	TES00120
13	CALL EIGEN(NA(1),NA(1),DUMMY,DUMMY(N1),DUMMY(N2),ISV,ISV,V,DUMMY(NTES00130	
14	13),IERR)	TES00140
15	NEVL = NA(1)	TES00150
16	IF( IERR .EQ. 0 ) GO TO 200	TES00160
17	CALL LNCNT(4)	TES00170
18	PRINT 100,IERR	TES00180
19	100 FORMAT(//,' IN TESTSA, THE ',IS,' EIGENVALUE OF A HAS NOT BEEN FO	TES00190
20	UND AFTER 30 ITERATIONS',/)	TES00200
21	RETURN	TES00210
22	C	TES00220
23	200 CONTINUE	TES00230
24	NDUM1(1) = NEVL	TES00240
25	NDUM1(2) = 1	TES00250
26	CALL JUXTC(DUMMY(N1),NDUM1,DUMMY(N2),NDUM1,DUMMY,NDUM2)	TES00260
27	C	TES00270
28	IF( DISC ) GO TO 400	TES00280
29	DO 300 I=1,NEVL	TES00290
30	IF( DUMMY(I) .GE. ALPHA ) GO TO 600	TES00300
31	300 CONTINUE	TES00310
32	GO TO 550	TES00320
33	400 CONTINUE	TES00330
34	N = NDUM2(1)*NDUM2(2)+1	TES00340
35	DO 500 I =1,NEVL	TES00350
36	K = I + NEVL	TES00360
37	L=N + I -1	TES00370
38	DUMMY(L) = DSQRT((DUMMY(I)**2)+(DUMMY(K)**2))	TES00380
39	500 CONTINUE	TES00390
40	C	TES00400
41	IF( DUMMY(L) .GE. ALPHA ) GO TO 600	TES00410
42	C	TES00420
43	550 CONTINUE	TES00430
44	STABLE = .TRUE.	TES00440
45	600 CONTINUE	TES00450
46	IF( IOP .EQ. 0 ) RETURN	TES00460
47	CALL LNCNT(4)	TES00470
48	PRINT 700	TES00480
49	700 FORMAT(//,' PROGRAM TO TEST THE RELATIVE STABILITY OF THE MATRIX A	TES00490
50	1',/)	TES00500
51	CALL PRNT(A,NA,4H A ,1)	TES00510
52	CALL LNCNT(4)	TES00520
53	PRINT 750	TES00530
54	750 FORMAT(//,' EIGENVALUES OF A ',/)	TES00540
55	CALL PRNT(DUMMY,NDUM2,4HEVLA,1)	TES00550
56	IF( .NOT. DISC ) GO TO 850	TES00560
57	CALL LNCNT(4)	TES00570
58	PRINT 800	TES00580
59	800 FORMAT(//,' MODULI OF EIGENVALUES OF A ',/)	TES00590
60	CALL PRNT(DUMMY(N),NDUM1,4HMODA,1)	TES00600
61	C	TES00610
62	850 CONTINUE	TES00620
63	CALL LNCNT(4)	TES00630

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      IF(STABLE) PRINT 900,ALPHA
64      IF( .NOT. STABLE) PRINT 950,ALPHA
65      900 FORMAT(//,' MATRIX A  IS STABLE RELATIVE TO ',E16.8,/)
66      950 FORMAT(//,' MATRIX A  IS UNSTABLE RELATIVE TO ',E16.8,/)
67 C
68      RETURN
69      END

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TES00640
TES00650
TES00660
TES00670
TES00680
TES00690
TES00700

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1	SUBROUTINE EXPSER(A,NA,EXPA,NEXPA,T,IOP,DUMMY)	EXP00010
2	IMPLICIT REAL*8 (A-H,O-Z)	EXP00020
3	DIMENSION A(1),EXPA(1),DUMMY(1)	EXP00030
4	DIMENSION NA(2),NEXPA(2)	EXP00040
5	COMMON/CONV/SUMCV,RICTCV,SERCV,MAXSUM	EXP00050
6		EXP00060
7	N = NA(1)	EXP00070
8	L = (N**2) + 1	EXP00080
9	TT = T	EXP00090
10	NEXPA(1)=NA(1)	EXP00100
11	NEXPA(2)=NA(2)	EXP00110
12		EXP00120
13	CALL MAXEL(A,NA,ANAA)	EXP00130
14	ANAA = ANAA*TT	EXP00140
15	ANAA = DABS(ANAA)	EXP00150
16	IF( ANAA .GT. 1.E-15 ) GO TO 100	EXP00160
17	CALL UNITY(EXPA,NEXPA)	EXP00170
18	GO TO 800	EXP00180
19		EXP00190
20	100 CONTINUE	EXP00200
21	IOPT=2	EXP00210
22	CALL NORMS(N,N,N,A,IOPT,ZERO)	EXP00220
23	ZERO=ZERO/(2.**47)	EXP00230
24	CALL TRCE(A,NA,TR)	EXP00240
25	TR = TR/N	EXP00250
26	DO 200 I = 1,N	EXP00260
27	M = I+N*(I-1)	EXP00270
28	A(M) = A(M) - TR	EXP00280
29	200 CONTINUE	EXP00290
30		EXP00300
31	IOPT = 1	EXP00310
32	CALL NORMS(N,N,N,A,IOPT,COL)	EXP00320
33	IOPT = 3	EXP00330
34	CALL NORMS(N,N,N,A,IOPT,ROW)	EXP00340
35	ANORM = ROW	EXP00350
36	IF( ANORM .GT. COL ) ANORM = COL	EXP00360
37	TMAX = 1./ANORM	EXP00370
38	K = 0	EXP00380
39	300 CONTINUE	EXP00390
40	IF( TMAX = TT ) 325,350,350	EXP00400
41	325 CONTINUE	EXP00410
42	K=K+1	EXP00420
43	TT = T/(2**K)	EXP00430
44	IF( K = 1000 ) 300,700,700	EXP00440
45	350 CONTINUE	EXP00450
46	SC = TT	EXP00460
47	CALL SCALE(A,NA,A,NA,TT)	EXP00470
48	CALL UNITY(EXPA,NEXPA)	EXP00480
49	II = 2	EXP00490
50	CALL ADD(A,NA,EXPA,NEXPA,DUMMY,NA)	EXP00500
51	CALL EQUATE(A,NA,DUMMY(L),NA)	EXP00510
52	400 CONTINUE	EXP00520
53	CALL MULT(A,NA,DUMMY(L),NA,EXPA,NEXPA)	EXP00530
54	S = 1./II	EXP00540
55	CALL SCALE(EXPA,NEXPA,DUMMY(L),NA,S)	EXP00550
56	CALL ADD(DUMMY(L),NA,DUMMY,NA,EXPA,NEXPA)	EXP00560
57	CALL MAXEL(DUMMY,NA,TOT)	EXP00570
58	CALL MAXEL(DUMMY(L),NA,DELT)	EXP00580
59	IF( TOT .GT. 1.0 ) GO TO 500	EXP00590
60	IF( DELT/TOT .LT. SERCV ) GO TO 600	EXP00600
61	GO TO 550	EXP00610
62	500 CONTINUE	EXP00620
63	IF( DELT .LT. SERCV ) GO TO 600	EXP00630

550	CONTINUE	EXP00640
	CALL EQUATE(EXPA,NEXPA,DUMMY,NA)	EXP00650
65	II = II + 1	EXP00660
	GO TO 400	EXP00670
7 C		EXP00680
600	CONTINUE	EXP00690
	IF( K ) 625,675,650	EXP00700
625	CONTINUE	EXP00710
	CALL LNCNT(1)	EXP00720
72	PRINT 635	EXP00730
635	FORMAT( ' ERROR IN EXPSER, K IS NEGATIVE ' )	EXP00740
	RETURN	EXP00750
5 C		EXP00760
650	CONTINUE	EXP00770
	DO 660 I = 1,K	EXP00780
	TT = 2*TT	EXP00790
	CALL EQUATE(EXPA,NEXPA,DUMMY,NA)	EXP00800
	CALL EQUATE(DUMMY,NA,DUMMY(L),NA)	EXP00810
	CALL MULT(DUMMY(L),NA,DUMMY,NA,EXPA,NEXPA)	EXP00820
660	CONTINUE	EXP00830
	T = TT	EXP00840
675	CONTINUE	EXP00850
	S = 1./SC	EXP00860
	CALL SCALE(A,NA,A,NA,S)	EXP00870
	DO 685 I = 1,N	EXP00880
	M = I + N*(I-1)	EXP00890
	A(M) = A(M) + TR	EXP00900
	IF( DABS(A(M)) .LE. ZERO ) A(M) = 0.0	EXP00910
685	CONTINUE	EXP00920
2 C		EXP00930
	TR=TR*T	EXP00940
	S = DEXP(T)	EXP00950
	CALL SCALE(EXPA,NEXPA,EXPA,NEXPA,S)	EXP00960
	GO TO 800	EXP00970
7 C		EXP00980
700	CONTINUE	EXP00990
	CALL LNCNT(1)	EXP01000
	PRINT 750	EXP01010
750	FORMAT( ' ERROR IN EXPSER, K = 1000 ' )	EXP01020
	RETURN	EXP01030
103 C		EXP01040
800	CONTINUE	EXP01050
	IF( IOP .EQ. 0 ) RETURN	EXP01060
	CALL LNCNT(4)	EXP01070
	PRINT 825	EXP01080
825	FORMAT(// ' COMPUTATION OF THE MATRIX EXPONENTIAL EXP(A T) BY THE SERIES METHOD '//)	EXP01090
	CALL PRNT(A,NA,4H A ,1)	EXP01100
	CALL LNCNT(3)	EXP01110
	PRINT A50,T	EXP01120
850	FORMAT(// ' T = ',D16.8//)	EXP01130
	CALL PRNT(EXPA,NEXPA,4H EXPA,1)	EXP01140
	RETURN	EXP01150
	END	EXP01160



0	SUBROUTINE EXPADE (MAX, N, A, EA, IDIG, WK, IERR)	EXP00010
	IMPLICIT REAL*8 (A-H,O-Z)	EXP00020
	DIMENSION A(MAX,N),EA(MAX,N),WK(N,1),C(9)	EXP00030
3	REAL*4 SDIGC,ALOG10	EXP00040
	IERR = 0	EXP00050
C	CALCULATE NORM OF A	EXP00060
6	ANORM = 0.	EXP00070
7	DO 10 I=1,N	EXP00080
8	S = 0.	EXP00090
9	DO 5 J=1,N	EXP00100
10	S = S + DABS(A(I,J))	EXP00110
5	CONTINUE	EXP00120
2	IF (S .GT. ANORM) ANORM = S	EXP00130
13 10	CONTINUE	EXP00140
4 C ****		EXP00150
5 C	CALCULATE ACCURACY ESTIMATE	EXP00160
16 C ****		EXP00170
17	DIGC = 24.*DFLOAT(N)	EXP00180
8	IF (ANORM .GT. 1.) DIGC = DIGC*ANORM	EXP00190
9	SDIGC=DIGC	EXP00200
20	IDIG = 15 - IFIX(ALOG10(SDIGC) + .5)	EXP00210
1 C	DETERMINE POWER OF TWO AND NORMALIZATION FACTOR	EXP00220
2 C ****		EXP00230
23	M = 0	EXP00240
24	IF (ANORM .LE. 1.) GO TO 27	EXP00250
5	FACTOR = 2.	EXP00260
26	DO 15 M=1,46	EXP00270
27	IF (ANORM .LE. FACTOR) GO TO 20	EXP00280
8	FACTOR = FACTOR*2.	EXP00290
9 15	CONTINUE	EXP00300
30	GO TO 125	EXP00310
1 20	CONTINUE	EXP00320
2 C ****		EXP00330
33 C	NORMALIZE MATRIX	EXP00340
34 C ****		EXP00350
5	DO 25 I=1,N	EXP00360
36	DO 25 J=1,N	EXP00370
37	A(I,J) = A(I,J)/FACTOR	EXP00380
8 25	CONTINUE	EXP00390
9 27	CONTINUE	EXP00400
40 C ****		EXP00410
1 C	SET COEFFICIENTS FOR (9,9) PADE TABLE ENTRY	EXP00420
2 C ****		EXP00430
43	C(1) = .5	EXP00440
44	C(2) = 1.17647058823520-01	EXP00450
45	C(3) = 1.71568627450980-02	EXP00460
46	C(4) = 1.71568627450980-03	EXP00470
47	C(5) = 1.22549019607840-04	EXP00480
48	C(6) = 6.28456510809450-06	EXP00490
49	C(7) = 2.24448753860510-07	EXP00500
50	C(8) = 5.10110804228450-09	EXP00510
51	C(9) = 5.66789782476050-11	EXP00520
52 C ****		EXP00530
53 C	CALCULATE PADE NUMERATOR AND DENOMINATOR BY COLUMNS	EXP00540
54 C ****		EXP00550
55	NP1 = N+1	EXP00560
56	NP7 = N+7	EXP00570
57	DO 95 J=1,N	EXP00580
58 C ****		EXP00590
59 C	COMPUTE JTH COLUMN OF FIRST NINE POWERS OF A	EXP00600
60 C ****		EXP00610
61	DO 35 I=1,N	EXP00620
62	S = 0.	EXP00630

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3	DO 30 L=1,N	EXP00640
4	S = S + A(I,L)*A(L,J)	EXP00650
5 30	CONTINUE	EXP00660
66	WK(I,NP1) = S	EXP00670
7 35	CONTINUE	EXP00680
8	DO 45 K=NP1,NP7	EXP00690
69	KP1 = K+1	EXP00700
0	DO 45 I=1,N	EXP00710
1	S = 0.	EXP00720
72	DO 40 L=1,N	EXP00730
73	S = S + A(I,L)*WK(L,K)	EXP00740
4 40	CONTINUE	EXP00750
5	WK(I,KP1) = S	EXP00760
76 45	CONTINUE	EXP00770
7 C ****		EXP00780
8 C	COLLECT TERMS FOR JTH COLUMN OF NUMERATOR AND DENOMINATOR	EXP00790
79 C ****		EXP00800
0	DO 85 I=1,N	EXP00810
1	S = 0.	EXP00820
62	U = 0.	EXP00830
83	DO 65 L=1,8	EXP00840
4	K = N+9-L	EXP00850
5	KN1 = K-N+1	EXP00860
86	P = C(KN1)*WK(I,K)	EXP00870
7	S = S + P	EXP00880
8	IEO = MOD(KN1,2)	EXP00890
89	IF (IEO.EQ.0) GO TO 55	EXP00900
90	U = U - P	EXP00910
1	GO TO 65	EXP00920
42 55	CONTINUE	EXP00930
93	U = U + P	EXP00940
4 65	CONTINUE	EXP00950
5	P = C(1)*A(I,J)	EXP00960
96	S = S + P	EXP00970
7	U = U - P	EXP00980
8	IF (I.NE. J) GO TO 80	EXP00990
99	S = S + 1.	EXP01000
00	U = U + 1.	EXP01010
11 80	CONTINUE	EXP01020
12	EA(I,J) = S	EXP01030
03	WK(I,J) = U	EXP01040
4 85	CONTINUE	EXP01050
5 95	CONTINUE	EXP01060
06 C ****		EXP01070
7 C	CALCULATE NORMALIZED EXP(A) BY WK * EXP(A) = EA	EXP01080
08 C ****		EXP01090
09	CALL GAUSEL (MAX,N,WK,N,EA,IERR)	EXP01100
10	IF (IERR.NE. 0) GO TO 130	EXP01110
11	IF (M.EQ. 0) GO TO 130	EXP01120
12 C ****		EXP01130
13 C	TAKE OUT EFFECT OF NORMALIZATION ON EXP(A)	EXP01140
14 C ****		EXP01150
15	DO 120 K=1,M	EXP01160
16	DO 110 I=1,N	EXP01170
17	DO 110 J=1,N	EXP01180
18	S = 0.	EXP01190
19	DO 105 L=1,N	EXP01200
20	S = S + EA(I,L)*EA(L,J)	EXP01210
21 105	CONTINUE	EXP01220
22	WK(I,J) = S	EXP01230
23 110	CONTINUE	EXP01240
24	DO 115 I=1,N	EXP01250
25	DO 115 J=1,N	EXP01260

26		EA(I,J) = WK(I,J)	EXP01270
7	115	CONTINUE	EXP01280
28	120	CONTINUE	EXP01290
29	C	****	EXP01300
0	C	UN-NORMALIZE A	EXP01310
1	C	****	EXP01320
32		DO 122 I=1,N	EXP01330
3		DO 122 J=1,N	EXP01340
4		A(I,J) = A(I,J)*FACTOR	EXP01350
35	122	CONTINUE	EXP01360
36		GO TO 130	EXP01370
7	C	****	EXP01380
38	C	NORM OF A IS EXCESSIVE	EXP01390
39	C	****	EXP01400
0	125	CONTINUE	EXP01410
1		IERR = 1	EXP01420
42	C	****	EXP01430
43	C	EXIT ROUTINE	EXP01440
44	C	****	EXP01450
45	130	CONTINUE	EXP01460
46		RETURN	EXP01470
47		END	EXP01480

0		SUBROUTINE EXPINT(A,NA,B,NB,C,NC,T,IOP,DUMMY)	EXP00
1		IMPLICIT REAL*8 (A-H,O-Z)	EXP00
2		DIMENSION A(1),B(1),C(1),DUMMY(1)	EXP00
3		DIMENSION NA(2),NB(2),NC(2)	EXP00
4		COMMON/CONV/SUMCV,RICTCV,SERCV,MAXSUM	EXP00
5		N = NA(1)	EXP00
6		L = (N**2)+1	EXP00
7		NC(1) = NA(1)	EXP00
8		NC(2) = NA(2)	EXP00
9		NB(1) = NA(1)	EXP00
10		NB(2) = NA(2)	EXP00
11		TT = T	EXP00
12	C		EXP00
13		IOP1 = 1	EXP00
14		CALL NORMS(N,N,N,A,IOP1,COL)	EXP00
15		IOP1 = 3	EXP00
16		CALL NORMS(N,N,N,A,IOP1,ROW)	EXP00
17		ANAA = COL	EXP00
18		IF( ANAA .GT. ROW ) ANAA = ROW	EXP00
19		TMAX = 1./ANAA	EXP00
20		K = 0	EXP00
21	100	CONTINUE	EXP00
22		IF( TMAX - TT ) 125,150,150	EXP00
23	125	CONTINUE	EXP00
24		K = K + 1	EXP00
25		TT = T/(2**K)	EXP00
26		IF( K = 1000 )100,600,600	EXP00
27	C		EXP00
28	150	CONTINUE	EXP00
29		SC = TT	EXP00
30		CALL SCALE(A,NA,A,NA,TT)	EXP00
31		CALL UNITY(B,NB)	EXP00
32		CALL SCALE(B,NB,DUMMY,NB,TT)	EXP00
33		S = TT/2.	EXP00
34		CALL SCALE(A,NA,DUMMY(L),NA,S)	EXP00
35		II = 2	EXP00
36		CALL ADD(DUMMY,NA,DUMMY(L),NA,DUMMY(L),NA)	EXP00
37		CALL ADD(A,NA,B,NB,DUMMY,NA)	EXP00
38		CALL EQUATE(A,NA,C,NC)	EXP00
39	200	CONTINUE	EXP00
40		CALL MULT(A,NA,C,NC,B,NB)	EXP00
41		S = 1./II	EXP00
42		CALL SCALE(B,NB,C,NC,S)	EXP00
43		CALL MAXEL(DUMMY,NA,TOT)	EXP00
44		CALL MAXEL(C,NC,DELT)	EXP00
45		IF( TOT .GT. 1.0 ) GO TO 300	EXP00
46		IF( DELT/TOT .LT. SERCV ) GO TO 400	EXP00
47		GO TO 350	EXP00
48	300	CONTINUE	EXP00
49		IF( DELT .LT. SERCV ) GO TO 400	EXP00
50	350	CONTINUE	EXP00
51		S = TT/(II + 1)	EXP00
52		CALL SCALE(C,NC,B,NB,S)	EXP00
53		CALL ADD(B,NB,DUMMY(L),NB,DUMMY(L),NB)	EXP00
54		CALL ADD(C,NC,DUMMY,NC,DUMMY,NC)	EXP00
55		II = II + 1	EXP00
56		GO TO 200	EXP00
57	C		EXP00
58	400	CONTINUE	EXP00
59		CALL EQUATE(DUMMY,NB,B,NB)	EXP00
60		IF( K ) 425,500,450	EXP00
61	425	CONTINUE	EXP00
62		CALL LNCNT(1)	EXP00

3	PRINT 435	EXP00640
4	435 FORMAT(' ERROR IN EXPINT, K IS NEGATIVE')	EXP00650
65	RETURN	EXP00660
46 C		EXP00670
7	450 CONTINUE	EXP00680
68	DO 475 J = 1,K	EXP00690
69	TT = 2*TT	EXP00700
0	CALL EQUATE(B,NB,DUMMY,NB)	EXP00710
1	CALL MULT(DUMMY,NA,DUMMY(L),NA,C,NC)	EXP00720
72	CALL ADD(DUMMY(L),NC,C,NC,DUMMY(L),NC)	EXP00730
73	CALL MULT(DUMMY,NB,DUMMY,NB,B,NB)	EXP00740
4	475 CONTINUE	EXP00750
75	T = TT	EXP00760
76 C		EXP00770
7	500 CONTINUE	EXP00780
78	CALL EQUATE(DUMMY(L),NC,C,NC)	EXP00790
79	S = 1./SC	EXP00800
80	CALL SCALE(A,NA,A,NA,S)	EXP00810
81 C		EXP00820
82	IF( IOP .EQ. 0 ) RETURN	EXP00830
93	CALL LNCNT(5)	EXP00840
94	PRINT 550	EXP00850
85	550 FORMAT('/', ' COMPUTATION OF THE MATRIX EXPONENTIAL EXP(A T)', '/', ' AND ITS INTEGRAL OVER (0,T) BY THE SERIES METHOD ', '/')	EXP00860
86		EXP00870
87	CALL PRNT(A,NA,4H A ,1)	EXP00880
88	CALL LNCNT(3)	EXP00890
89	PRINT 575, T	EXP00900
90	575 FORMAT('/', ' T = ',D16.8, '/')	EXP00910
91	CALL PRNT(B,NB,4HEXPA,1)	EXP00920
92	CALL PRNT(C,NC,4HINT ,1)	EXP00930
93	RETURN	EXP00940
94 C		EXP00950
95	600 CONTINUE	EXP00960
96	CALL LNCNT(1)	EXP00970
97	PRINT 650	EXP00980
98	650 FORMAT(' ERROR IN EXPINT, K = 1000')	EXP00990
99	RETURN	EXP01000
100 C		EXP01010
101	END	EXP01020

0	SUBROUTINE VARANC(A,NA,G,NG,Q,NQ,W,NW,IDENT,DISC,IOP,DUMMY)	VAR0001
1	IMPLICIT REAL*8 (A-H,O-Z)	VAR0002
2	DIMENSION A(1),G(1),Q(1),W(1),DUMMY(1)	VAR0003
3	DIMENSION NA(2),NG(2),NQ(2),NW(2),NDUM1(2),IOP(3),IOPT(2)	VAR0004
4	LOGICAL IDENT,DISC,SYM	VAR0005
5	COMMON/TOL/EPSAM,EPSSM,IACM	VAR0006
6	IF( IOP(1) .EQ. 0 ) GO TO 100	VAR0007
7	CALL LNCNT(5)	VAR0008
8	IF( DISC ) PRINT 25	VAR0009
9	IF( .NOT. DISC ) PRINT 35	VAR0010
10	25 FORMAT('/', ' PROGRAM TO SOLVE FOR THE STEADY-STATE VARIANCE MATRIX '	VAR0011
11	1,/, ' FOR A LINEAR DISCRETE SYSTEM',/)	VAR0012
12	35 FORMAT('/', ' PROGRAM TO SOLVE FOR THE STEADY-STATE VARIANCE MATRIX '	VAR0013
13	1,/, ' FOR A LINEAR CONTINUOUS SYSTEM',/)	VAR0014
14	CALL PRNT(A,NA,4H A ,1)	VAR0015
15	IF( .NOT. IDENT ) GO TO 55	VAR0016
16	CALL LNCNT(3)	VAR0017
17	PRINT 45	VAR0018
18	45 FORMAT('/', ' G IS AN IDENTITY MATRIX ',/)	VAR0019
19	GO TO 65	VAR0020
20	55 CONTINUE	VAR0021
21	CALL PRNT(G,NG,4H G ,1)	VAR0022
22	65 CONTINUE	VAR0023
23	IF ( .NOT. IDENT ) GO TO 85	VAR0024
24	CALL LNCNT(3)	VAR0025
25	PRINT 75	VAR0026
26	75 FORMAT('/', ' INTENSITY MATRIX FOR COVARIANCE OF PROCESS NOISE ',/)	VAR0027
27	C	VAR0028
28	85 CONTINUE	VAR0029
29	CALL PRNT(Q,NQ,4H Q ,1)	VAR0030
30	C	VAR0031
31	100 CONTINUE	VAR0032
32	IF( IDENT ) GO TO 200	VAR0033
33	CALL MULT(G,NG,Q,NQ,DUMMY,NG)	VAR0034
34	N1 = NG(1)*NG(2) + 1	VAR0035
35	CALL TRANSP(G,NG,DUMMY(N1),NDUM1)	VAR0036
36	CALL MULT(DUMMY,NG,DUMMY(N1),NDUM1,Q,NQ)	VAR0037
37	C	VAR0038
38	IF( IOP(1) .EQ. 0 ) GO TO 200	VAR0039
39	CALL LNCNT(3)	VAR0040
40	PRINT 75	VAR0041
41	CALL PRNT(Q,NQ,4H QGT,1)	VAR0042
42	C	VAR0043
43	200 CONTINUE	VAR0044
44	IF(.NOT. DISC) CALL SCALE(W,NW,W,NW,-1.0)	VAR0045
45	IOPT(1) = IOP(2)	VAR0046
46	IOPT(2) = 1	VAR0047
47	SYM = .TRUE.	VAR0048
48	IF( DISC ) GO TO 300	VAR0049
49	IF( IOP(3) .EQ. 0 ) GO TO 250	VAR0050
50	CALL BILIN(A,NA,A,NA,W,NW,IOPT,BETA,SYM,DUMMY)	VAR0051
51	GO TO 400	VAR0052
52	C	VAR0053
53	250 CONTINUE	VAR0054
54	CALL BARSTW(A,NA,A,NA,W,NW,IOPT,SYM,EPSA,EPSSA,DUMMY)	VAR0055
55	GO TO 400	VAR0056
56	C	VAR0057
57	300 CONTINUE	VAR0058
58	CALL EQUATE(A,NA,DUMMY,NA)	VAR0059
59	N = NA(1)*2	VAR0060
60	N1 = N + 1	VAR0061
61	CALL TRANSP(A,NA,DUMMY(N1),NA)	VAR0062
62	N2 = N1 + N	VAR0063

63	CALL SUM(DUMMY,NA,W,NW,DUMMY(N1),NA,IOP,SYM,DUMMY(N2))	VAR0061
64 C		VAR0061
65	400 CONTINUE	VAR0061
66	IF( IOP(1) .EQ. 0 ) RETURN	VAR0061
67	CALL LNCNT(3)	VAR0061
68	PPINT 450	VAR0071
69	450 FORMAT(/, ' VARIANCE MATRIX ',/)	VAR0071
70	CALL PRNT(W,NW,4H W ,1)	VAR0071
71 C		VAR0071
72	RETURN	VAR0071
73	END	VAR0071

0	SUBROUTINE CTROL(A,NA,B,NB,C,NC,IOP,IAC,IRANK,DUMMY)	CTR000
1	IMPLICIT REAL*8 (A-H,O-Z)	CTR000
2	DIMENSION A(1),B(1),C(1),DUMMY(1)	CTR000
3	DIMENSION NA(2),NB(2),NC(2),NV(2),IOP(5)	CTR000
4	N = NA(1)*NB(2)	CTR000
5	N1 = N+1	CTR000
6	N2 = N1+N	CTR000
7	K = NA(1)-1	CTR000
8	J = 1	CTR000
9	C	CTR001
10	CALL EQUATE(B,NB,DUMMY(N2),NV)	CTR001
11	CALL EQUATE(B,NB,DUMMY,NB)	CTR001
12	100 CONTINUE	CTR001
13	CALL MULT(A,NA,DUMMY,NB,DUMMY(N1),NB)	CTR001
14	CALL JUXTC(DUMMY(N2),NV,DUMMY(N1),NB,C,NC)	CTR001
15	C	CTR001
16	IF( J .EQ. K ) GO TO 200	CTR001
17	C	CTR001
18	CALL EQUATE(DUMMY(N1),NB,DUMMY,NB)	CTR001
19	CALL EQUATE(C,NC,DUMMY(N2),NV)	CTR002
20	J = J + 1	CTR002
21	GO TO 100	CTR002
22	C	CTR002
23	200 CONTINUE	CTR002
24	C	CTR002
25	IF(IOP(1) .EQ. 0 ) GO TO 300	CTR002
26	CALL PRNT(A,NA,4H A ,1)	CTR002
27	CALL PRNT(B,NB,4H B ,1)	CTR002
28	CALL LNCNT(4)	CTR002
29	PRINT 250	CTR002
30	250 FORMAT(//,' THE MATRIX C IS THE CONTROLLABILITY MATRIX FOR THE A/	CTR003
31	1B PAIR',/)	CTR003
32	CALL PRNT(C,NC,4H C ,1)	CTR003
33	C	CTR003
34	300 IF( IOP(2) .EQ. 0 ) RETURN	CTR003
35	NOS = 0	CTR003
36	IOPT = 2	CTR003
37	K = NC(2)	CTR003
38	NC(2) = NB(2)*(NA(2)-NB(2)+1)	CTR003
39	N = NC(1)*NC(2)	CTR004
40	CALL TRANSP(C,NC,DUMMY,NV)	CTR004
41	NC(2) = K	CTR004
42	N1 = N + 1	CTR004
43	N2 = N1 + NV(2)	CTR004
44	CALL SNVDEC(IOPT,NV(1),NV(2),NV(1),NV(2),DUMMY,NOS,B,IAC,ZTEST,DUM	CTR004
45	1MY(N1),DUMMY(N2),IRANK,A,IERR)	CTR004
46	IF( IERR .EQ. 0 ) GO TO 340	CTR004
47	CALL LNCNT(5)	CTR004
48	IF( IERR .GT. 0 ) PRINT 310,IERR	CTR004
49	IF( IERR .EQ. -1 ) PRINT 320, ZTEST,IRANK	CTR005
50	310 FORMAT(//,' IN CTROL, SNVDEC HAS FAILED TO CONVERGE TO THE ',I4, 'CTR005	CTR005
51	1 SINGULAR VALUE AFTER 30 ITERATIONS ')	CTR005
52	320 FORMAT(//,' IN CTROL, THE MATRIX SUBMITTED TO SNVDEC USING ZTEST =CTR005	CTR005
53	1',D16.8,' IS CLOSE TO A MATRIX WHICH IS OF LOWER RANK',/, ' IF THE CTR005	CTR005
54	2ACCURACACY IS REDUCED THE RANK MAY ALSO BE REDUCED',/, ' CURRENT RACTR005	CTR005
55	3NK =',I4)	CTR005
56	IF( IERR .GT. 0 ) RETURN	CTR005
57	C	CTR005
58	340 CONTINUE	CTR005
59	IF( IOP(3) .EQ. 0 ) GO TO 400	CTR006
60	CALL LNCNT(6)	CTR006
61	PRINT 350,ZTEST,IRANK	CTR006
62	350 FORMAT(//,' BASED ON THE ZERO-TEST ',D16.8,' THE RANK OF THE CONTRCTR006	CTR006



63	CONTROLLABILITY MATRIX IS 'I4,/, ' THE SINGULAR VALUES ARE '.,/)	CTR0
64	IOPT = 0	CTR0
65	NV(1) = NV(2)	CTR0
66	NV(2) = 1	CTR0
67	CALL PRNT(DUMMY(N1),NV,IOPT,3)	CTR0
68 C		CTR0
69	400 IF( IOP(4) .EQ. 0 ) RETURN	CTR0
70	N = NA(1)**2	CTR0
71	CALL EQUATE(DUMMY(N2),NA,DUMMY,NA)	CTR0
72	N1 = N + 1	CTR0
73	N2 = N1 + N	CTR0
74	CALL MULT(A,NA,DUMMY,NA,DUMMY(N1),NA)	CTR0
75	CALL TRANP(DUMMY,NA,DUMMY(N2),NA)	CTR0
76	CALL EQUATE(DUMMY(N2),NA,DUMMY,NA)	CTR0
77	CALL MULT(DUMMY,NA,DUMMY(N1),NA,DUMMY(N2),NA)	CTR0
78	CALL MULT(DUMMY,NA,B,NB,DUMMY(N1),NB)	CTR0
79 C		CTR0
80	IF( IOP(5) .EQ. 0 ) RETURN	CTR0
81	CALL LNCNT(5)	CTR0
82	PRINT 500	CTR0
83	500 FORMAT(/, ' CONTROLLABILITY CANONICAL FORM '.,/,' (V TRANSPOSE) A	CTR0
84	1 V.')	CTR0
85	CALL PRNT(DUMMY(N2),NA,IOPT,3)	CTR0
86	CALL LNCNT(2)	CTR0
87	PRINT 510	CTR0
88	510 FORMAT(/, ' (V TRANSPOSE ) B ')	CTR0
89	CALL PRNT(DUMMY(N1),NB,IOPT,3)	CTR0
90	CALL LNCNT(2)	CTR0
91	PRINT 520	CTR0
92	520 FORMAT(/, ' V TRANSPOSE')	CTR0
93	CALL PRNT(DUMMY,NA,IOPT,3)	CTR0
94 C		CTR0
95	RETURN	CTR0
96	END	CTR0

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0	SUBROUTINE TRNSIT(A,NA,B,NB,H,NH,G,NG,F,NF,V,NV,T,X,NX,DISC,STABL	TRN000
1	1E,IOP,DUMMY)	TRN000
2	IMPLICIT REAL*8 (A-H,O-Z)	TRN000
3	DIMENSION A(1),B(1),H(1),G(1),F(1),V(1),X(1),DUMMY(1)	TRN000
4	DIMENSION NA(2),NB(2),NH(2),NG(2),NF(2),NV(2),NX(2),T(2),IOP(4)	TRN000
5	DIMENSION NDUM1(2),NDUM2(2)	TRN000
6	LOGICAL DISC,STABLE	TRN000
7	N = NA(1)*NA(2)	TRN000
8	N1 = N + 1	TRN000
9	N2 = N + N1	TRN001
10	N3 = N + N2	TRN001
11	N4 = N + N3	TRN001
12	N5 = N + N4	TRN001
13	N6 = N + N5	TRN001
14	C	TRN001
15	CALL LNCNT(4)	TRN001
16	IF(DISC) PRINT 100	TRN001
17	IF( .NOT. DISC ) PRINT 120	TRN001
18	100 FORMAT(//, ' COMPUTATION OF TRANSIENT RESPONSE FOR THE DIGITAL SYSTEM	TRN001
19	1EM ',/)	TRN002
20	120 FORMAT(//, ' COMPUTATION OF TRANSIENT RESPONSE FOR THE CONTINUOUS	TRN002
21	1 SYSTEM',/)	TRN002
22	CALL PRNT(A,NA,4H A ,1)	TRN002
23	CALL PRNT(B,NB,4H B ,1)	TRN002
24	IF( (IOP(1) .NE. 1) .AND. (IOP(1) .NE. 0) ) GO TO 180	TRN002
25	CALL LNCNT(3)	TRN002
26	IF( IOP(1) .EQ. 0 ) PRINT 140	TRN002
27	IF( IOP(1) .EQ. 1 ) PRINT 160	TRN002
28	140 FORMAT(//, ' H IS A NULL MATRIX ')	TRN002
29	160 FORMAT(//, ' H IS AN IDENTITY MATRIX ')	TRN003
30	GO TO 200	TRN003
31	180 CONTINUE	TRN003
32	CALL PRNT(H,NH,4H H ,1)	TRN003
33	200 CONTINUE	TRN003
34	IF( (IOP(2) .NE. 1) .AND. (IOP(2) .NE. 0) ) GO TO 260	TRN003
35	CALL LNCNT(3)	TRN003
36	IF( IOP(2) .EQ. 0 ) PRINT 220	TRN003
37	IF( IOP(2) .EQ. 1 ) PRINT 240	TRN003
38	220 FORMAT(//, ' G IS A NULL MATRIX ')	TRN003
39	240 FORMAT(//, ' G IS AN IDENTITY MATRIX ')	TRN004
40	GO TO 280	TRN004
41	260 CONTINUE	TRN004
42	CALL PRNT(G,NG,4H G ,1)	TRN004
43	280 CONTINUE	TRN004
44	CALL PRNT(F,NF,4H F ,1)	TRN004
45	IF( (IOP(3) .NE. 0) .AND. (IOP(3) .NE. 1) ) GO TO 295	TRN004
46	CALL LNCNT(3)	TRN004
47	IF(IOP(3).EQ.0) PRINT 285	TRN004
48	IF(IOP(3).EQ.1) PRINT 290	TRN004
49	285 FORMAT(//, ' V IS A NULL MATRIX ')	TRN005
50	290 FORMAT(//, ' V IS AN IDENTITY MATRIX ')	TRN005
51	GO TO 300	TRN005
52	295 CONTINUE	TRN005
53	CALL PRNT(V,NV,4H V ,1)	TRN005
54	C	TRN005
55	300 CONTINUE	TRN005
56	CALL EQUATE(A,NA,DUMMY(N6),NA)	TRN005
57	CALL MULT(B,NB,F,NF,DUMMY,NA)	TRN005
58	CALL SUBT(A,NA,DUMMY,NA,A,NA)	TRN005
59	C	TRN006
60	IF(DISC) GO TO 350	TRN006
61	NMAX = T(1)/T(2)	TRN006
62	IOPT = 1	TRN006

63	TT = T(2)	TRN00
64	IF( IOP(3) .NE. 0 ) GO TO 315	TRN00
65	CALL EXPSER(A,NA,DUMMY,NA,TT,IOP,DUMMY(N1))	TRN00
66	GO TO 400	TRN00
67	315 CONTINUE	TRN00
68	CALL EXPINT(A,NA,DUMMY,NA,DUMMY(N1),NA,TT,IOP,DUMMY(N2))	TRN00
69	CALL MULT(DUMMY(N1),NA,B,NB,DUMMY(N2),NB)	TRN00
70	IF( IOP(3) .NE. 1 ) GO TO 325	TRN00
71	CALL EQUATE(DUMMY(N2),NB,DUMMY(N1),NX)	TRN00
72	GO TO 400	TRN00
73	325 CONTINUE	TRN00
74	CALL MULT(DUMMY(N2),NB,V,NV,DUMMY(N1),NX)	TRN00
75	GO TO 400	TRN00
76	350 CONTINUE	TRN00
77	NMAX = IOP(4)	TRN00
78	CALL EQUATE(A,NA,DUMMY,NA)	TRN00
79	IF( IOP(3) .EQ. 0 ) GO TO 400	TRN00
80	CALL MULT(B,NB,V,NV,DUMMY(N1),NX)	TRN00
81	C	TRN00
82	400 CONTINUE	TRN00
83	CALL LNCNT(4)	TRN00
84	PRINT 420	TRN00
85	420 FORMAT('/', ' STRUCTURE OF PRINTING TO FOLLOW',/)	TRN00
86	CALL LNCNT(6)	TRN00
87	PRINT 440	TRN00
88	440 FORMAT(' TIME OR STAGE ',/, ' STATE = X TRANSPOSE = FROM DX = AX	TRN00
89	1 + BU',/, ' OUTPUT = Y TRANSPOSE = FROM Y = HX + GU IF DIFFERENT	TRN00
90	2 FROM X',/, ' CONTROL = U TRANSPOSE = FROM U = -FX + V',/)	TRN00
91	C	TRN00
92	K = 0	TRN00
93	L = 0	TRN00
94	CALL SCALE(F,NF,F,NF,-1,0)	TRN00
95	C	TRN00
96	450 CONTINUE	TRN00
97	IF( K .GT. NMAX ) GO TO 800	TRN00
98	CALL MULT(F,NF,X,NX,DUMMY(N2),NV)	TRN00
99	IF( IOP(3) .NE. 0 ) CALL ADD(DUMMY(N2),NV,V,NV,DUMMY(N2),NV)	TRN01
100	CALL MULT(DUMMY,NA,X,NX,DUMMY(N3),NX)	TRN01
101	IF( IOP(3) .EQ. 0 ) GO TO 475	TRN01
102	CALL ADD(DUMMY(N1),NX,DUMMY(N3),NX,DUMMY(N3),NX)	TRN01
103	475 CONTINUE	TRN01
104	IF( IOP(2) .EQ. 0 ) GO TO 525	TRN01
105	IF( IOP(2) .EQ. 1 ) GO TO 500	TRN01
106	CALL MULT(G,NG,DUMMY(N2),NV,DUMMY(N4),NDUM1)	TRN01
107	GO TO 525	TRN01
108	500 CONTINUE	TRN01
109	CALL EQUATE(DUMMY(N2),NV,DUMMY(N4),NDUM1)	TRN01
110	525 CONTINUE	TRN01
111	IF( IOP(1) .EQ. 0 ) GO TO 575	TRN01
112	IF( IOP(1) .EQ. 1 ) GO TO 550	TRN01
113	CALL MULT(H,NH,X,NX,DUMMY(N5),NDUM1)	TRN01
114	GO TO 575	TRN01
115	550 CONTINUE	TRN01
116	CALL EQUATE(X,NX,DUMMY(N5),NDUM1)	TRN01
117	575 CONTINUE	TRN01
118	IF( IOP(2) .EQ. 0 ) GO TO 600	TRN01
119	IF( IOP(1) .EQ. 0 ) GO TO 700	TRN01
120	CALL ADD(DUMMY(N4),NDUM1,DUMMY(N5),NDUM1,DUMMY(N4),NDUM1)	TRN01
121	GO TO 700	TRN01
122	600 CONTINUE	TRN01
123	IF( IOP(1) .NE. 0 ) CALL EQUATE(DUMMY(N5),NDUM1,DUMMY(N4),NDUM1)	TRN01
124	C	TRN01
125	700 CONTINUE	TRN01

126	CALL LNCNT(5)	TRN0
127	IF( .NOT. DISC ) GO TO 720	TRN0
128	PRINT 710,K	TRN0
129	710 FORMAT(////,15)	TRN0
130	GO TO 740	TRN0
131	720 CONTINUE	TRN0
132	TIME=K*T(2)	TRN0
133	PRINT 730,TIME	TRN0
134	730 FORMAT(////,D16.7)	TRN0
135	740 CONTINUE	TRN0
136	CALL TRANP(X,NX,DUMMY(N5),NDUM2)	TRN0
137	CALL PRNT(DUMMY(N5),NDUM2,L,3)	TRN0
138	IF( (IOP(2) .EQ. 0) .AND. ( (IOP(1) .EQ. 0) .OR. (IOP(1) .EQ. 1) )	TRN0
139	1) GO TO 750	TRN0
140	CALL TRANP(DUMMY(N4),NDUM1,DUMMY(N5),NDUM2)	TRN0
141	CALL PRNT(DUMMY(N5),NDUM2,L,3)	TRN0
142	750 CONTINUE	TRN0
143	CALL TRANP(DUMMY(N2),NV,DUMMY(N5),NDUM2)	TRN0
144	CALL PRNT(DUMMY(N5),NDUM2,L,3)	TRN0
145	C	TRN0
146	CALL EQUATE(DUMMY(N3),NX,X,NX)	TRN0
147	K = K + 1	TRN0
148	GO TO 450	TRN0
149	C	TRN0
150	C	TRN0
151	800 CONTINUE	TRN0
152	CALL SCALE(F,NF,F,NF,-1.0)	TRN0
153	IF( .NOT. STABLE .OR. IOP(3) .EQ. 0 ) GO TO 900	TRN0
154	IF( IOP(3) .EQ. 1 ) GO TO 820	TRN0
155	CALL MULT(B,NB,V,NV,DUMMY,NX)	TRN0
156	GO TO 840	TRN0
157	820 CONTINUE	TRN0
158	CALL EQUATE(B,NB,DUMMY,NX)	TRN0
159	840 CONTINUE	TRN0
160	IF( .NOT. DISC ) GO TO 860	TRN0
161	CALL UNITY(DUMMY(N1),NA)	TRN0
162	CALL SUBT(DUMMY(N1),NA,A,NA,A,NA)	TRN0
163	860 CONTINUE	TRN0
164	IFAC = 0	TRN0
165	CALL GELIM(NA(1),NA(1),A,NX(2),DUMMY,DUMMY(N1),IFAC,DUMMY(N2),IERR	TRN0
166	1)	TRN0
167	IF( IERR .EQ. 0 ) GO TO 880	TRN0
168	CALL LNCNT(3)	TRN0
169	IF( .NOT. DISC ) PRINT 865	TRN0
170	IF( DISC ) PRINT 870	TRN0
171	865 FORMAT(//,' IN TRNSIT, THE MATRIX A-BF SUBMITTED TO GELIM IS SINGU	TRN0
172	1LAR')	TRN0
173	870 FORMAT(//,' IN TRNSIT, THE MATRIX I - (A-BF) SUBMITTED TO GELIM I	TRN0
174	S SINGULAR')	TRN0
175	GO TO 900	TRN0
176	880 CONTINUE	TRN0
177	IF( .NOT. DISC ) CALL SCALE(DUMMY,NX,DUMMY,NX,-1.0)	TRN0
178	CALL LNCNT(5)	TRN0
179	PRINT 890	TRN0
180	890 FORMAT(////,' STEADY-STATE VALUE OF X TRANSPOSE')	TRN0
181	CALL TRANP(DUMMY,NX,DUMMY(N5),NDUM2)	TRN0
182	CALL PRNT(DUMMY(N5),NDUM2,L,3)	TRN0
183	C	TRN0
184	900 CONTINUE	TRN0
185	CALL EQUATE(DUMMY(N6),NA,A,NA)	TRN0
186	C	TRN0
187	RETURN	TRN0
188	END	TRN0

0	SUBROUTINE SAMPL(A,NA,B,NB,Q,NQ,R,NR,W,NW,T,IOP,DUMMY)	SAM000
1	IMPLICIT REAL*8 (A-H,O-Z)	SAM000
2	DIMENSION A(1),R(1),Q(1),R(1),W(1),DUMMY(1)	SAM000
3	DIMENSION NA(2),NB(2),NQ(2),NR(2),NW(2),IOP(2),NDUM(2)	SAM000
4	COMMON/CONV/SUMCV,RICTCV,SERCV,MAXSUM	SAM000
5	IF( IOP(1) .EQ. 0 ) GO TO 100	SAM000
6 C		SAM000
7	IF( IOP(2) .EQ. 0 ) GO TO 50	SAM000
8 C		SAM000
9	CALL LNCNT(5)	SAM000
10	PRINT 25	SAM000
11	25 FORMAT(/,,' COMPUTATION OF WEIGHTING MATRICES FOR THE OPTIMAL SAMP	SAM000
12	1LED-DATA REGULATOR PROBLEM',//)	SAM000
13	CALL PRNT(A,NA,4H A ,1)	SAM000
14	CALL PRNT(B,NB,4H B ,1)	SAM000
15	CALL LNCNT(3)	SAM000
16	PRINT 35	SAM000
17	35 FORMAT(/,,' CONTINUOUS PERFORMANCE INDEX WEIGHTING MATRICES',//)	SAM000
18	CALL PRNT(Q,NQ,4H Q ,1)	SAM000
19	CALL PRNT(R,NR,4H R ,1)	SAM002
20	CALL LNCNT(3)	SAM002
21	PRINT 45,T	SAM002
22	45 FORMAT(/,,' SAMPLE TIME = ',D16.8,//)	SAM002
23 C		SAM002
24	GO TO 100	SAM002
25 C		SAM002
26	50 CONTINUE	SAM002
27	CALL LNCNT(8)	SAM002
28	PRINT 75	SAM002
29	75 FORMAT(/,,' COMPUTATION OF THE RECONSTRUCTIBILITY GRAMIAN',//,,' FOR	SAM003
30	1 THE (A,H) SYSTEM OVER THE INTERVAL (0,T) ',//,,' THE MATRIX Q IS (	SAM003
31	2 H TRANSPOSE ) X H',//)	SAM003
32	CALL PRNT(A,NA,4H A ,1)	SAM003
33	CALL PRNT(Q,NQ,4H Q ,1)	SAM003
34	CALL LNCNT(3)	SAM003
35	PRINT 85,T	SAM003
36	85 FORMAT(/,,' T = ',D16.8,//)	SAM003
37 C		SAM003
38	100 CONTINUE	SAM003
39 C		SAM004
40	N = NA(1)	SAM004
41	L = ( N**2)	SAM004
42	N1 = L + 1	SAM004
43	N2 = N1 + L	SAM004
44	TT = T	SAM004
45 C		SAM004
46	IOPT = 1	SAM004
47	CALL NORMS(N,N,N,A,IOPT,ANORM)	SAM004
48	IOPT = 3	SAM004
49	CALL NORMS(N,N,N,A,IOPT,ROWA)	SAM005
50	IF( ANORM .GT. ROWA ) ANORM = ROWA	SAM005
51 C		SAM005
52	IF( ANORM .LE. 1.E-15 ) GO TO 900	SAM005
53 C		SAM005
54	TMAX = 1.0/ANORM	SAM005
55	K = 0	SAM005
56 C		SAM005
57	125 CONTINUE	SAM005
58	IF( TMAX - TT ) 150,150,200	SAM005
59	150 CONTINUE	SAM006
60	K = K + 1	SAM006
61	TT = T/( 2**K)	SAM006
62	IF( K - 1000 ) 125,800,800	SAM006

63	C		SAM00
64		200 CONTINUE	SAM00
65	C		SAM00
66		I = 0	SAM00
67		SC = TT	SAM00
68		CALL SCALE(A,NA,A,NA,TT)	SAM00
69		CALL SCALE(Q,NQ,Q,NQ,TT)	SAM00
70		CALL EQUATE(Q,NQ,DUMMY,NQ)	SAM00
71	C		SAM00
72		IF( IOP(2) .NE. 0 ) GO TO 500	SAM00
73	C		SAM00
74		225 CONTINUE	SAM00
75		II = I + 2	SAM00
76		I = I + 1	SAM00
77		F = 1.0/II	SAM00
78		CALL SCALE(A,NA,DUMMY(N1),NA,F)	SAM00
79		CALL MULT(DUMMY,NA,DUMMY(N1),NA,DUMMY(N2),NA)	SAM00
80		CALL TRANP(DUMMY(N2),NA,DUMMY(N1),NA)	SAM00
81		CALL ADD(DUMMY(N1),NA,DUMMY(N2),NA,DUMMY,NA)	SAM00
82	C		SAM00
83		CALL MAXEL(Q,NQ,TOT)	SAM00
84		CALL MAXEL(DUMMY,NA,DELT)	SAM00
85		IF( TOT .GT. 1.0 ) GO TO 250	SAM00
86		IF( DELT/TOT .LT. SERCV ) GO TO 300	SAM00
87		GO TO 275	SAM00
88		250 CONTINUE	SAM00
89		IF( DELT .LT. SERCV ) GO TO 300	SAM00
90		275 CONTINUE	SAM00
91		CALL ADD(Q,NQ,DUMMY,NA,Q,NQ)	SAM00
92		GO TO 225	SAM00
93	C		SAM00
94		300 CONTINUE	SAM00
95	C		SAM00
96		IF( K .EQ. 0 ) GO TO 400	SAM00
97		N3 = N2 + L	SAM00
98		G = 1.0	SAM00
99		IOPT = 0	SAM01
100		CALL EXPSER(A,NA,DUMMY,NA,G,IOPT,DUMMY(N1))	SAM01
101	C		SAM01
102		350 CONTINUE	SAM01
103		IF( K .EQ. 0 ) GO TO 400	SAM01
104		K = K - 1	SAM01
105	C		SAM01
106		CALL TRANP(DUMMY,NA,DUMMY(N1),NA)	SAM01
107		CALL MULT(Q,NQ,DUMMY,NA,DUMMY(N2),NA)	SAM01
108		CALL MULT(DUMMY(N1),NA,DUMMY(N2),NA,DUMMY(N3),NA)	SAM01
109		CALL ADD(Q,NQ,DUMMY(N3),NA,Q,NQ)	SAM01
110		CALL MULT(DUMMY,NA,DUMMY,NA,DUMMY(N1),NA)	SAM01
111		CALL EQUATE(DUMMY(N1),NA,DUMMY,NA)	SAM01
112	C		SAM01
113		GO TO 350	SAM01
114	C		SAM01
115		400 CONTINUE	SAM01
116		S = 1.0/SC	SAM01
117		CALL SCALE(A,NA,A,NA,S)	SAM01
118	C		SAM01
119		IF( IOP(1) .EQ. 0 ) RETURN	SAM01
120		CALL PRNT(Q,NQ,4HGRAM,1)	SAM01
121		RETURN	SAM01
122	C		SAM01
123		500 CONTINUE	SAM01
124		CALL SCALE(B,NB,B,NB,TT)	SAM01
125		N3 = N2 + L	SAM01

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126	N4 = N3 + L	SAM012
127	N5 = N4 + L	SAM012
128	N6 = N5 + L	SAM012
129 C		SAM013
130	525 CONTINUE	SAM013
131	II = I + 2	SAM013
132	I = I + 1	SAM013
133	F = 1.0/II	SAM013
134	CALL SCALE(A,NA,DUMMY(N1),NA,F)	SAM013
135	CALL TRANP(DUMMY(N1),NA,DUMMY(N2),NA)	SAM013
136	CALL MULT(DUMMY,NA,DUMMY(N1),NA,DUMMY(N3),NA)	SJM013
137	CALL TRANP(DUMMY(N3),NA,DUMMY(N1),NA)	SJM013
138	CALL MULT(DUMMY,NA,B,NB,DUMMY(N5),NW)	SAM013
139	CALL ADD(DUMMY(N1),NA,DUMMY(N3),NA,DUMMY,NA)	SAM014
140	CALL SCALE(DUMMY(N5),NW,DUMMY(N1),NW,F)	SAM014
141	IF( I .NE. 1 ) GO TO 550	SAM014
142	CALL EQUATE(DUMMY(N1),NW,W,NW)	SJM014
143	CALL EQUATE(DUMMY(N1),NW,DUMMY(N6),NW)	SAM014
144	CALL ADD(Q,NQ,DUMMY,NQ,Q,NQ)	SAM014
145	GO TO 525	SAM014
146 C		SAM014
147	550 CONTINUE	SAM014
148	CALL MULT(DUMMY(N2),NA,DUMMY(N6),NW,DUMMY(N5),NW)	SAM014
149	CALL ADD(DUMMY(N5),NW,DUMMY(N1),NW,DUMMY(N1),NW)	SAM015
150	CALL TRANP(B,NB,DUMMY(N2),NDUM)	SAM015
151	CALL SCALE(DUMMY(N2),NDUM,DUMMY(N2),NDUM,F)	SAM015
152	CALL MULT(DUMMY(N2),NDUM,DUMMY(N6),NW,DUMMY(N3),NR)	SAM015
153	CALL TRANP(DUMMY(N3),NR,DUMMY(N5),NR)	SAM015
154	CALL ADD(DUMMY(N3),NR,DUMMY(N5),NR,DUMMY(N3),NR)	SAM015
155	CALL EQUATE(DUMMY(N1),NW,DUMMY(N6),NW)	SAM015
156	IF( I .NE. 2 ) GO TO 575	SAM015
157	CALL ADD(Q,NQ,DUMMY,NQ,Q,NQ)	SAM015
158	CALL ADD(W,NW,DUMMY(N1),NW,W,NW)	SAM015
159	CALL EQUATE(DUMMY(N3),NR,DUMMY(N4),NR)	SAM016
160	GO TO 525	SJM016
161 C		SAM016
162	575 CONTINUE	SAM016
163	CALL MAXEL(Q,NQ,TOT)	SAM016
164	CALL MAXEL(DUMMY,NQ,DELT)	SAM016
165	IF( TOT .GT. 1.0 ) GO TO 580	SAM016
166	IF( DELT/TOT .LT. SERCV ) GO TO 585	SAM016
167	GO TO 595	SAM016
168 C		SAM016
169	580 CONTINUE	SAM017
170	IF( DELT .LT. SERCV ) GO TO 585	SAM017
171	GO TO 595	SAM017
172 C		SAM017
173	585 CONTINUE	SAM017
174	CALL MAXEL(DUMMY(N4),NR,TOT)	SAM017
175	CALL MAXEL(DUMMY(N3),NR,DELT)	SAM017
176	IF( TOT .GT. 1.0 ) GO TO 590	SAM017
177	IF( DELT/TOT .LT. SERCV ) GO TO 600	SAM017
178	GO TO 595	SAM017
179 C		SAM018
180	590 CONTINUE	SAM018
181	IF( DELT .LT. SERCV ) GO TO 600	SAM018
182 C		SAM018
183	595 CONTINUE	SAM018
184	CALL ADD(Q,NQ,DUMMY,NQ,Q,NQ)	SAM018
185	CALL ADD(W,NW,DUMMY(N1),NW,W,NW)	SAM018
186	CALL ADD(DUMMY(N4),NR,DUMMY(N3),NR,DUMMY(N4),NR)	SAM018
187	GO TO 525	SAM018
188 C		SAM018

189	600	CONTINUE	SAM01
190		IF( K .EQ. 0 ) GO TO 700	SAM01
191		G = 1.0	SAM01
192		IOPT = 0	SAM01
193		CALL EXPINT(A,NA,DUMMY,NA,DUMMY(N1),NA,G,IOPT,DUMMY(N2))	SAM01
194		CALL MULT(DUMMY(N1),NA,B,NB,DUMMY(N2),NB)	SAM01
195		CALL EQUATE(DUMMY(N2),NB,DUMMY(N1),NB)	SAM01
196	C		SAM01
197	650	CONTINUE	SAM01
198		IF( K .EQ. 0 ) GO TO 700	SAM01
199		K = K - 1	SAM02
200		CALL MULT(Q,NQ,DUMMY,NA,DUMMY(N2),NA)	SAM02
201		CALL TRANP(DUMMY,NA,DUMMY(N3),NA)	SAM02
202		CALL MULT(DUMMY(N3),NA,DUMMY(N2),NA,DUMMY(N5),NA)	SAM02
203		CALL MULT(Q,NQ,DUMMY(N1),NB,DUMMY(N2),NB)	SAM02
204		CALL ADD(Q,NQ,DUMMY(N5),NA,Q,NQ)	SAM02
205		CALL MULT(DUMMY(N3),NA,DUMMY(N2),NB,DUMMY(N5),NB)	SAM02
206		CALL MULT(DUMMY(N3),NA,W,NW,DUMMY(N6),NW)	SAM02
207		CALL ADD(DUMMY(N5),NW,DUMMY(N6),NW,DUMMY(N5),NW)	SAM02
208		CALL TRANP(DUMMY(N1),NB,DUMMY(N6),NDUM)	SAM02
209		CALL MULT(DUMMY(N6),NDUM,W,NW,DUMMY(N3),NR)	SAM02
210		CALL ADD(W,NW,DUMMY(N5),NW,W,NW)	SAM02
211		CALL MULT(DUMMY(N6),NDUM,DUMMY(N2),NB,DUMMY(N5),NR)	SAM02
212		CALL ADD(DUMMY(N5),NR,DUMMY(N3),NR,DUMMY(N5),NR)	SAM02
213		CALL TRANP(DUMMY(N3),NR,DUMMY(N6),NR)	SAM02
214		CALL ADD(DUMMY(N5),NR,DUMMY(N6),NR,DUMMY(N6),NR)	SAM02
215		CALL SCALE(DUMMY(N4),NR,DUMMY(N4),NR,2.0)	SAM02
216		CALL ADD(DUMMY(N6),NR,DUMMY(N4),NR,DUMMY(N4),NR)	SAM02
217		CALL MULT(DUMMY,NA,DUMMY(N1),NB,DUMMY(N3),NB)	SAM02
218		CALL ADD(DUMMY(N3),NB,DUMMY(N1),NB,DUMMY(N1),NB)	SAM02
219		CALL MULT(DUMMY,NA,DUMMY,NA,DUMMY(N3),NA)	SAM02
220		CALL EQUATE(DUMMY(N3),NA,DUMMY,NA)	SAM02
221		GO TO 650	SAM02
222	C		SAM02
223	700	CONTINUE	SAM02
224		CALL SCALE(R,NR,R,NR,T)	SAM02
225		CALL ADD(R,NR,DUMMY(N4),NR,R,NR)	SAM02
226		CALL SCALE(W,NW,W,NW,2.0)	SAM02
227		S = 1.0/SC	SAM02
228		CALL SCALE(A,NA,A,NA,S)	SAM02
229		CALL SCALE(B,NB,B,NB,S)	SAM02
230		IF( IOP(1) .EQ. 0 ) RETURN	SAM02
231	C		SAM02
232		CALL LNCNT(3)	SAM02
233		PRINT 750	SAM02
234	750	FORMAT(/,' DISCRETE PERFORMANCE INDEX WEIGHTING MATRICES',/)	SAM02
235		CALL PRNT(Q,NQ,4H Q ,1)	SAM02
236		CALL PRNT(W,NW,4H W ,1)	SAM02
237		CALL PRNT(R,NR,4H R ,1)	SAM02
238		RETURN	SAM02
239	C		SAM02
240	800	CONTINUE	SAM02
241		CALL LNCNT(1)	SAM02
242		PRINT 850	SAM02
243	850	FORMAT(' ERROR IN SAMPL , K = 1000')	SAM02
244		RETURN	SAM02
245	C		SAM02
246	900	CONTINUE	SAM02
247		CALL SCALE(Q,NQ,Q,NQ,T)	SAM02
248		IF( IOP(2) .NE. 0 ) GO TO 925	SAM02
249		IF( IOP(1) .NE. 0 ) CALL PRNT(Q,NQ,4HGRAM,1)	SAM02
250		RETURN	SAM02
51	C		SAM02



252	925 CONTINUE	SAM02
253	CALL MULT(Q,NQ,B,NB,W,NW)	SAM02
254	CALL SCALE(W,NW,W,NW,T)	SAM02
255	CALL TRANP(B,NB,DUMMY,NDUM)	SAM02
256	CALL MULT(DUMMY,NDUM,W,NW,DUMMY(N1),NP)	SAM02
257	TT = T/3.	SJM02
258	CALL SCALE(DUMMY(N1),NR,DUMMY,NR,TT)	SAM02
259	CALL SCALE(R,NR,R,NR,T)	SAM02
260	CALL ADD(R,NR,DUMMY,NR,R,NR)	SAM02
261	IF( IOP(1) .EQ. 0 ) RETURN	SAM02
262	CALL LNCNT(3)	SAM02
263	PRINT 750	SAM02
264	CALL PRNT(Q,NQ,4H Q ,1)	SAM02
265	CALL PRNT(W,NW,4H W ,1)	SAM02
266	CALL PRNT(R,NR,4H R ,1)	SAM02
267	RETURN	SAM02
268 C		SAM02
269	END	SAM02

0	SUBROUTINE PREFIL(A,NA,B,NB,Q,NQ,W,NW,R,NR,F,NF,IOP,DUMMY)	PRE00
1	IMPLICIT REAL*8 (A-H,O-Z)	PRE00
2	DIMENSION A(1),B(1),Q(1),W(1),R(1),F(1),DUMMY(1)	PRE00
3	DIMENSION NA(2),NB(2),NQ(2),NW(2),NR(2),NF(2),IOP(3)	PRE00
4	IF( IOP(1) .EQ. 0 ) GO TO 100	PRE00
5	CALL LNCNT(5)	PRE00
6	PRINT 25	PRE00
7	25 FORMAT(/, ' PROGRAM TO COMPUTE PREFILTER GAIN F TO ELEMIMATE CROSS	PRE00
8	IS-PRODUCT TERM ',/, ' IN QUADRATIC PERFORMANCE INDEX ',/)	PRE00
9	IF( IOP(3) .EQ. 0 ) GO TO 50	PRE00
10	CALL PRNT(A,NA,4H A ,1)	PRE00
11	CALL PRNT(B,NB,4H B ,1)	PRE00
12	50 CONTINUE	PRE00
13	CALL PRNT(Q,NQ,4H Q ,1)	PRE00
14	CALL PRNT(W,NW,4H W ,1)	PRE00
15	CALL PRNT(R,NR,4H R ,1)	PRE00
16	C	PRE00
17	100 CONTINUE	PRE00
18	CALL TRANP(W,NW,F,NF)	PRE00
19	CALL SCALE(F,NF,F,NF,0.5)	PRE00
20	CALL EQUATE(R,NR,DUMMY,NR)	PRE00
21	IOPT=0	PRE00
22	IFAC=0	PRE00
23	N1=NR(1)**2+1	PRE00
24	M = NR(1)	PRE00
25	CALL SYMPDS(M,M,DUMMY,NF(2),F,IOPT,IFAC,DETERM,ISCALE,DUMMY(N1),IE	PRE00
26	1RR)	PRE00
27	IF( IERR .EQ. 0 ) GO TO 200	PRE00
28	CALL LNCNT(4)	PRE00
29	PRINT 150	PRE00
30	150 FORMAT(/, ' IN PREFIL, THE MATRIX R IS NOT SYMMETRIC POSITIVE DEF	PRE00
31	INITE',/)	PRE00
32	RETURN	PRE00
33	C	PRE00
34	200 CONTINUE	PRE00
35	IF( IOP(2) .EQ. 0 ) GO TO 300	PRE00
36	CALL MULT(W,NW,F,NF,DUMMY,NQ)	PRE00
37	CALL SCALE(DUMMY,NQ,DUMMY,NQ,0.5)	PRE00
38	CALL SUBT(Q,NQ,DUMMY,NQ,Q,NQ)	PRE00
39	C	PRE00
40	300 CONTINUE	PRE00
41	IF( IOP(3) .EQ. 0 ) GO TO 400	PRE00
42	CALL MULT(B,NB,F,NF,DUMMY,NA)	PRE00
43	CALL SUBT(A,NA,DUMMY,NA,A,NA)	PRE00
44	C	PRE00
45	400 CONTINUE	PRE00
46	IF( IOP(1) .EQ. 0 ) RETURN	PRE00
47	CALL PRNT(F,NF,4H F ,1)	PRE00
48	IF( IOP(2) .EQ. 0 ) GO TO 500	PRE00
49	CALL LNCNT(3)	PRE005
50	PRINT 450	PRE005
51	450 FORMAT(/, ' MATRIX Q = (W/2)F ',/)	PRE005
52	CALL PRNT(Q,NQ,4HNEWQ,1)	PRE005
53	C	PRE005
54	500 CONTINUE	PRE005
55	IF( IOP(3) .EQ. 0 ) RETURN	PRE005
56	CALL PRNT(A,NA,4HNEWA,1)	PRE005
57	RETURN	PRE005
58	END	PRE005

0	SUBROUTINE CSTAB(A,NA,B,NB,F,NF,IOP,SCLE,DUMMY)	CST001
1	IMPLICIT REAL*8 (A-H,O-Z)	CST001
2	DIMENSION A(1),B(1),F(1),DUMMY(1)	CST001
3	DIMENSION NA(2),NB(2),NF(2),IOP(3),NDUM(2)	CST001
4	DIMENSION IOPT(2)	CST001
5	LOGICAL SYM	CST001
6	COMMON/TOL/EPSSM,EPSSM,IACM	CST001
7	N = NA(1)**2	CST001
8	N1=N+1	CST001
9	C	CST001
10	IF(IOP(2) .EQ. 0 ) GO TO 100	CST001
11	CALL EQUATE(A,NA,DUMMY,NA)	CST001
12	N2=N1+NA(1)	CST001
13	N3=N2+NA(1)	CST001
14	ISV = 0	CST001
15	ILV = 0	CST001
16	CALL EIGEN(NA(1),NA(1),DUMMY,DUMMY(N1),DUMMY(N2),ISV,ILV,V,DUMMY(NCST00	CST001
17	13),IERR)	CST001
18	C	CST001
19	M=NA(1)	CST001
20	IF(IERR .EQ. 0) GO TO 50	CST001
21	CALL LNCNT(3)	CST001
22	PRINT 25,IERR	CST001
23	25 FORMAT(/,' IN CSTAB, THE SUBROUTINE EIGEN FAILED TO DETERMINE THE	CST001
24	1 ',I4,' EIGENVALUE FOR THE MATRIX A AFTER 30 ITERATIONS')	CST001
25	IERR=1	CST001
26	CALL NORMS(M,M,M,A,IERR,BETA)	CST001
27	BETA=2.*BETA	CST001
28	GO TO 200	CST001
29	50 CONTINUE	CST001
30	C	CST001
31	BETA = 0.0	CST001
32	DO 75 I = 1,M	CST001
33	J = N1 + I - 1	CST001
34	BETA1 = DABS(DUMMY(J))	CST001
35	IF(BETA1 .GT. BETA) BETA = BETA1	CST001
36	75 CONTINUE	CST001
37	BETA = SCLE*(BETA + .001)	CST001
38	GO TO 200	CST001
39	C	CST001
40	100 CONTINUE	CST001
41	BETA = SCLE	CST001
42	200 CONTINUE	CST001
43	C	CST001
44	CALL TRANP(B,NB,DUMMY,NDUM)	CST001
45	CALL MULT(B,NB,DUMMY,NDUM,DUMMY(N1),NA)	CST001
46	CALL SCALE(DUMMY(N1),NA,DUMMY,NA,-2.0)	CST001
47	CALL SCALE(A,NA,DUMMY(N1),NA,-1.0)	CST001
48	J = -NA(1)	CST001
49	NAX = NA(1)	CST001
50	DO 225 I=1,NAX	CST001
51	J = J+NAX+1	CST001
52	K = N1+J-1	CST001
53	DUMMY(K)=DUMMY(K)-BETA	CST001
54	225 CONTINUE	CST001
55	N2 = N1 + N	CST001
56	SYM = .TRUE.	CST001
57	IOPT(1)=0	CST001
58	C	CST001
59	IF( IOP(3) .NE. 0 ) GO TO 300	CST001
60	EPSA=EPSSM	CST001
61	CALL BARSTW(DUMMY(N1),NA,A,NA,DUMMY,NA,IOPT,SYM,EPSA,EPSSM,DUMMY(N2CST006:	CST006:
62	1))	CST006:

63	GO TO 350	CST01
64	300 CONTINUE	CST01
65	IOPT(2) = 1	CST01
66	CALL BILIN(DUMMY(N1),NA,A,NA,DUMMY,NA,IOPT,ASCLE,SYM,DUMMY(N2))	CST01
67	350 CONTINUE	CST01
68	C	CST01
69	CALL EQUATE(B,NB,DUMMY(N1),NB)	CST01
70	IOPT(1) = 3	CST01
71	IAC = IACM	CST01
72	N3 = N2 + NA(1)	CST01
73	CALL SNVDEC(IOPT,NA(1),NA(1),NA(1),NA(1),DUMMY,NB(2),DUMMY(N1),IAC	CST01
74	1,ZTEST,DUMMY(N2),DUMMY(N3),IRANK,APLUS,IERR)	CST01
75	IF(IERR.EQ. 0) GO TO 400	CST01
76	CALL LNCNT(5)	CST01
77	IF(IERR.GT. 0) PRINT 360,IERR	CST01
78	IF(IERR.EQ. -1) PRINT 370,ZTEST,IRANK	CST01
79	360 FORMAT(//,' IN CSTAB, SNVDEC HAS FAILED TO CONVERGE TO THE ',I4,'	CST01
80	1SINGULARVALUE AFTER 30 ITERATIONS',//)	CST01
81	370 FORMAT(//,' IN CSTAB, THE MATRIX SUBMITTED TO SNVDEC USING ZTEST =	CST01
82	1 ',D16.8,' IS CLOSE TO A MATRIX OF LOWER RANK ',//,' IF THE ACCUR	CST01
83	2ACY IAC IS REDUCED THE RANK MAY ALSO BE REDUCED',//,' CURRENT RANK	CST01
84	3 = ',I4)	CST01
85	IF( IERR.GT. 0 ) RETURN	CST01
86	NDUM(1) = NA(1)	CST01
87	NDUM(2) = 1	CST01
88	CALL PRNT(DUMMY(N2),NDUM,4HSGVL,1)	CST01
89	400 CONTINUE	CST01
90	C	CST01
91	CALL TRANP(DUMMY(N1),NB,F,NF)	CST01
92	IF ( IOPT(1).EQ. 0 ) RETURN	CST01
93	CALL LNCNT(4)	CST01
94	PRINT 500	CST01
95	500 FORMAT(//,' COMPUTATION OF F MATRIX SUCH THAT A-BF IS ASYMPTOTICAL	CST01
96	1LY STABLE IN THE CONTINUOUS SENSE ',//)	CST01
97	CALL PRNT(A,NA,4H A ,1)	CST01
98	CALL LNCNT(4)	CST01
99	PRINT 550,BETA	CST01
100	550 FORMAT(//,' BETA = ',D16.8,//)	CST01
101	CALL PRNT(B,NB,4H B ,1)	CST01
102	CALL PRNT(F,NF,4H F ,1)	CST01
103	CALL MULT(B,NB,F,NF,DUMMY,NA)	CST01
104	CALL SUBT(A,NA,DUMMY,NA,DUMMY,NA)	CST01
105	CALL PRNT(DUMMY,NA,4HA-BF,1)	CST01
106	N2 = N1+NA(1)	CST01
107	N3 = N2+NA(1)	CST01
108	ISV = 0	CST01
109	ILV = 0	CST01
110	CALL EIGEN(NA(1),NA(1),DUMMY,DUMMY(N1),DUMMY(N2),ISV,ILV,V,DUMMY(N	CST01
111	13),IERR)	CST01
112	I = NA(1)	CST01
113	IF( IERR.EQ. 0 ) GO TO 600	CST01
114	M = NA(1)-IERR	CST01
115	CALL LNCNT(3)	CST01
116	PRINT 25,IERR	CST01
117	600 CONTINUE	CST01
118	CALL LNCNT(4)	CST01
119	PRINT 650	CST01
120	650 FORMAT(//,' EIGENVALUES OF A-BF',//)	CST01
121	675 FORMAT(10X,2D16.8)	CST01
122	CALL LNCNT(M)	CST01
123	DO 700 I=1,M	CST01
124	J = N1+I-1	CST01
125	K = N2+I-1	CST01

126 PRINT 675,DUMMY(J),DUMMY(K)

127 700 CONTINUE

128 C

129 RETURN

130 END

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0	SUBROUTINE DSTAB(A,NA,B,NB,F,NF,SING,IOP,SCLE,DUMMY)	DST
1	IMPLICIT REAL*8 (A-H,O-Z)	DST
2	DIMENSION A(1),B(1),F(1),DUMMY(1)	DST
3	DIMENSION NA(2),NB(2),NF(2),NDUM(2),IOP(2),IOPT(3),NDUM1(2)	DST
4	LOGICAL SING,SYM	DST
5	COMMON/TOL/EPSSAM,EPSSBM,IACM	DST
6	N = NA(1)**2	DST
7	N1 = N + 1	DST
8	N2 = N1 + N	DST
9	IF( .NOT. SING ) GO TO 100	DST
10	IOPT(1)=IOP(1)	DST
11	IOPT(2) = 1	DST
12	IOPT(3) = 0	DST
13	CSCLE=1.05	DST
14	CALL CSTAB(A,NA,B,NB,F,NF,IOPT,CSCLE,DUMMY)	DST
15	CALL MULT(B,NB,F,NF,DUMMY,NA)	DST
16	CALL SUBT(A,NA,DUMMY,NA,DUMMY,NA)	DST
17	CALL EQUATE(DUMMY,NA,DUMMY(N1),NA)	DST
18	GO TO 200	DST
19 C		DST
20	100 CONTINUE	DST
21	CALL EQUATE(A,NA,DUMMY,NA)	DST
22	CALL EQUATE(A,NA,DUMMY(N1),NA)	DST
23 C		DST
24	200 CONTINUE	DST
25	IF( IOP(2) .EQ. 0 ) GO TO 300	DST
26	N3 = N2 + NA(1)	DST
27	N4 = N3 + NA(1)	DST
28	ISV = 0	DST
29	CALL EIGEN(NA(1),NA(1),DUMMY(N1),DUMMY(N2),DUMMY(N3),ISV,ISV,V,DUM	DST
30	MY(N4),IERR)	DST
31	CALL EQUATE(DUMMY,NA,DUMMY(N1),NA)	DST
32	M = NA(1)	DST
33	IF( IERR .EQ. 0 ) GO TO 250	DST
34	CALL LNCNT(3)	DST
35	PRINT 225, IERR	DST
36 225	FORMAT(// 'IN DSTAB , THE PROGRAM EIGEN FAILED TO DETERMINE',	DST
37	1 IS, 'EIGENVALUE FOR THE MATRIX A-BG AFTER 30 ITERATIONS ')	DST
38	CALL PRNT(DUMMY,NA,4HA-BG,1)	DST
39	IF( SING ) CALL PRNT(F,NF,4H G ,1)	DST
40	RETURN	DST
41 C		DST
42	250 CONTINUE	DST
43	ALPHA = 1.0	DST
44	DO 275 I =1,M	DST
45	I1 = N2 + I -1	DST
46	I2 = N3 + I -1	DST
47	ALPHA1 = DSQRT(DUMMY(I1)**2 + DUMMY(I2)**2)	DST
48	IF( ALPHA1 .LT. ALPHA .AND. ALPHA1 .NE. 0 ) ALPHA = ALPHA1	DST
49	275 CONTINUE	DST
50	ALPHA = SCLE*ALPHA	DST
51	GO TO 400	DST
52 C		DST
53	300 CONTINUE	DST
54	ALPHA = SCLE	DST
55 C		DST
56	400 CONTINUE	DST
57	J = -NA(1)	DST
58	NAX = NA(1)	DST
59	DO 425 I = 1,NAX	DST
60	J = J + NAX + 1	DST
61	K = N1 + J -1	DST
62	DUMMY(K) = DUMMY(J) - ALPHA	DST

63	DUMMY(J) = DUMMY(J) + ALPHA	DST
64	425 CONTINUE	DST
65	CALL EQUATE(B,NB,DUMMY(N2),NB)	DST
66	N3 = N2 + NA(1)*NB(2)	DST
67	NRHS = NA(1)+NB(2)	DST
68	N4 = N3 + NA(1)	DST
69	IFAC = 0	DST
70	CALL GELIM(NA(1),NA(1),DUMMY,NRHS,DUMMY(N1),DUMMY(N3),IFAC,DUMMY(NOST	DST
71	14),IERR)	DST
72	IF( IERR .EQ. 0 ) GO TO 500	DST
73	CALL LNCNT(3)	DST
74	IF( .NOT. SING ) GO TO 445	DST
75	PRINT 435	DST
76	435 FORMAT(//,' IN DSTAB, GELIM HAS FOUND THE MATRIX ( A-BG) + (ALPHA)	DST
77	1 I SINGULAR ')	DST
78	CALL PRNT(A,NA,4H A ,1)	DST
79	CALL PRNT(B,NB,4H B ,1)	DST
80	GO TO 465	DST
81	445 CONTINUE	DST
82	CALL LNCNT(3)	DST
83	PRINT 455	DST
84	455 FORMAT(//,' IN DSTAB, GELIM HAS FOUND THE MATRIX A + (ALPHA)I SING	DST
85	ULAR ')	DST
86	CALL PRNT(A,NA,4H A ,1)	DST
87	465 CONTINUE	DST
88	CALL LNCNT(3)	DST
89	PRINT 475,ALPHA	DST
90	475 FORMAT(//,' ALPHA = ',D16.8)	DST
91	RETURN	DST
92	C	DST
93	500 CONTINUE	DST
94	CALL EQUATE(DUMMY(N1),NA,DUMMY,NA)	DST
95	CALL TRANSP(DUMMY(N2),NB,DUMMY(N1),NDUM)	DST
96	N3 = N2 + N	DST
97	CALL MULT(DUMMY(N2),NB,DUMMY(N1),NDUM,DUMMY(N3),NA)	DST
98	CALL SCALE(DUMMY(N3),NA,DUMMY(N1),NA,4.0)	DST
99	SYM = .TRUE.	DST
100	IOPT(1) = 0	DST
101	EPSA=EPSAM	DST
102	CALL BARSTW(DUMMY,NA,B,NB,DUMMY(N1),NA,IOPT,SYM,EPSA,EPSA,DUMMY(N2)	DST
103	1))	DST
104	CALL EQUATE(DUMMY(N1),NA,DUMMY,NA)	DST
105	CALL TRANSP(B,NB,DUMMY(N1),NDUM)	DST
106	CALL MULT(B,NB,DUMMY(N1),NDUM,DUMMY(N2),NA)	DST
107	CALL ADD(DUMMY,NA,DUMMY(N2),NA,DUMMY,NA)	DST
108	CALL EQUATE(A,NA,DUMMY(N1),NA)	DST
109	IF( .NOT. SING ) GO TO 600	DST
110	CALL MULT(B,NB,F,NF,DUMMY(N1),NA)	DST
111	CALL SUBT(A,NA,DUMMY(N1),NA,DUMMY(N1),NA)	DST
112	C	DST
113	600 CONTINUE	DST
114	IOPT(1) = 3	DST
115	M = NA(1)	DST
116	IAC=IACM	DST
117	CALL SNVDEC(IOPT,M,M,M,M,DUMMY,M,DUMMY(N1),IAC,ZTEST,DUMMY(N2),DUM	DST
118	MY(N3),IRANK,APLUS,IERR)	DST
119	IF( IERR .EQ. 0 ) GO TO 700	DST
120	CALL LNCNT(5)	DST
121	IF( IERR .GT. 0 ) PRINT 625,IERR	DST
122	IF( IERR .EQ. -1 ) PRINT 650,ZTEST,IRANK	DST
123	625 FORMAT(//,' IN DSTAB, SNVDEC HAS FAILED TO CONVERGE TO THE ',I5,'	DST
124	1 SINGULAR VALUE AFTER 30 ITERATIONS')	DST
125	650 FORMAT(//,' IN DSTAB, THE MATRIX SUBMITTED TO SNVDEC, USING ZTEST	DST

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126 1= 'D16.8,' , IS CLOSE TO A MATRIX OF LOWER RANK',/, ' IF THE ACCURST
127 2ACY IAC IS REDUCED THE RANK MAY ALSO BE REDUCED',/, ' CURRENT RANK DST
128 3 =',I4) DST
129 IF( IERR .GT. 0 ) RETURN DST
130 NDUM(1)= NA(1) DST
131 NDUM(2)= 1 DST
132 CALL PRNT(DUMMY(N2),NDUM,4HSGVL,1) DST
133 C DST
134 700 CONTINUE DST
135 CALL TRNP(8,N8,DUMMY(N2),NDUM) DST
136 CALL MULT(DUMMY(N2),NDUM,DUMMY(N1),NA,DUMMY,NF) DST
137 IF( .NOT. SING ) GO TO 800 DST
138 CALL ADD(F,NF,DUMMY,NF,F,NF) DST
139 GO TO 900 DST
140 C DST
141 800 CONTINUE DST
142 CALL EQUATE(DUMMY,NF,F,NF) DST
143 C DST
144 900 CONTINUE DST
145 IF( IOP(1) .EQ. 0 ) RETURN DST
146 CALL LNCNT(4) DST
147 PRINT 1000 DST
148 1000 FORMAT(/, ' COMPUTATION OF F SUCH THAT A-BF IS ASYMPTOTICALLY STABDST
149 1LE IN THE DISCRETE SENSE',/) DST
150 CALL PRNT(A,NA,4H A ,1) DST
151 CALL PRNT(B,NB,4H B ,1) DST
152 CALL LNCNT(4) DST
153 PRINT 1100,ALPHA DST
154 1100 FORMAT(/, ' ALPHA = ',D16.8,/) DST
155 CALL PRNT(F,NF,4H F ,1) DST
156 CALL MULT(B,NB,F,NF,DUMMY,NA) DST
157 CALL SUBT(A,NA,DUMMY,NA,DUMMY,NA) DST
158 CALL PRNT(DUMMY,NA,4HA-BF,1) DST
159 CALL LNCNT(3) DST
160 PRINT 1200 DST
161 1200 FORMAT(/, ' EIGENVALUES OF A-BF' ) DST
162 NDUM(1) = NA(1) DST
163 NDUM(2) = 1 DST
164 N2 = N1 + NA(1) DST
165 N3 = N2 + NA(1) DST
166 ISV = 0 DST
167 CALL EIGEN(NA(1),NA(1),DUMMY,DUMMY(N1),DUMMY(N2),ISV,ISV,V,DUMMY(NDST
168 13),IERR) DST
169 IF( IERR .EQ. 0 ) GO TO 1300 DST
170 CALL LNCNT(3) DST
171 PRINT 1250 DST
172 1250 FORMAT(/, ' IN DSTAB, THE PROGRAM EIGEN FAILED TO DETERMINE THE ',DST
173 1IS, ' EIGENVALUE FOR THE A-BF MATRIX AFTER 30 ITERATIONS' ) DST
174 NDUM(1)=NA(1)-IERR DST
175 C DST
176 1300 CONTINUE DST
177 CALL JUXTC(DUMMY(N1),NDUM,DUMMY(N2),NDUM,DUMMY,NDUM1) DST
178 CALL PRNT(DUMMY,NDUM1,4HEIGN,1) DST
179 CALL LNCNT(4) DST
180 PRINT 1400 DST
181 1400 FORMAT(/, ' MODULI OF EIGENVALUES OF A-BF',/) DST
182 M =NDUM(1) DST
183 DO 1500 I = 1,M DST
184 J = N1 + I - 1 DST
185 K = N2 + I - 1 DST
186 DUMMY(I)=DSQRT(DUMMY(J)**2 + DUMMY(K)**2) DST
187 1500 CONTINUE DST
188 CALL PRNT(DUMMY,NDUM,4HMOD ,1) DST

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189 C

190

191

RETURN

END

DST

DST

DST

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0  SUBROUTINE DISREG(A,NA,B,NB,H,NH,Q,NQ,R,NR,F,NF,P,NP,IOP,IDENT,OU DIS
1  DUMMY) DIS
2  IMPLICIT REAL*8 (A-H,O-Z) DIS
3  DIMENSION A(1),B(1),Q(1),R(1),F(1),P(1),DUMMY(1) DIS
4  DIMENSION NA(2),NB(2),NQ(2),NR(2),NF(2),NP(2) DIS
5  DIMENSION IOP(3) DIS
6  DIMENSION H(1),NH(2),NDUM(2) DIS
7  LOGICAL IDENT DIS
8  COMMON/TOL/EP3AM,EP3BM,IACM DIS
9  COMMON/CONV/SUMCV,RICTCV,SERCV,MAXSUM DIS
10 N = NA(1)**2 DIS
11 N1 = N + 1 DIS
12 N2 = N1 + N DIS
13 N3 = N2 + N DIS
14 C DIS
15 KSS = 0 DIS
16 I = IOP(3) DIS
17 C DIS
18 IF(IOP(1) .EQ. 0) GO TO 85 DIS
19 CALL LNCNT(5) DIS
20 PRINT 25 DIS
21 25 FORMAT(/,,' PROGRAM TO SOLVE THE TIME-INVARIANT FINITE-DURATION OPDIS
22 1TIMAL',/,,' DIGITAL REGULATOR PROBLEM WITH NOISE-FREE MEASUREMENTS'DIS
23 2,/) DIS
24 CALL PRNT(A,NA,4H A ,1) DIS
25 CALL PRNT(B,NB,4H B ,1) DIS
26 CALL PRNT(Q,NQ,4H Q ,1) DIS
27 IF(.NOT. IDENT) GO TO 45 DIS
28 CALL LNCNT(3) DIS
29 PRINT 35 DIS
30 35 FORMAT(/,,' H IS AN IDENTITY MATRIX',/) DIS
31 GO TO 65 DIS
32 45 CONTINUE DIS
33 CALL PRNT(H,NH,4H H ,1) DIS
34 CALL MULT(Q,NQ,H,NH,DUMMY,NH) DIS
35 CALL TRANSP(H,NH,DUMMY(N1),NF) DIS
36 CALL MULT(DUMMY(N1),NF,DUMMY,NH,Q,NQ) DIS
37 CALL LNCNT(3) DIS
38 PRINT 55 DIS
39 55 FORMAT(/,,' MATRIX ( H TRANSPOSE )QH',/) DIS
40 CALL PRNT(Q,NQ,4HHTQH,1) DIS
41 65 CONTINUE DIS
42 CALL PRNT(R,NR,4H R ,1) DIS
43 CALL LNCNT(4) DIS
44 PRINT 75 DIS
45 75 FORMAT(/,,' WEIGHTING ON TERMINAL VALUE OF STATE VECTOR',/) DIS
46 CALL PRNT(P,NP,4H P ,1) DIS
47 C DIS
48 85 CONTINUE DIS
49 IF((IOP(1) .NE. 0) .OR. IDENT) GO TO 100 DIS
50 CALL MULT(Q,NQ,H,NH,DUMMY,NH) DIS
51 CALL TRANSP(H,NH,DUMMY(N1),NF) DIS
52 CALL MULT(DUMMY(N1),NF,DUMMY,NH,Q,NQ) DIS
53 C DIS
54 100 CONTINUE DIS
55 I = I - 1 DIS
56 CALL EQUATE(P,NP,DUMMY,NP) DIS
57 CALL MULT(P,NP,A,NA,DUMMY(N1),NA) DIS
58 CALL TRANSP(B,NB,DUMMY(N2),NF) DIS
59 CALL MULT(DUMMY(N2),NF,DUMMY(N1),NA,F,NF) DIS
60 CALL MULT(P,NP,B,NR,DUMMY(N1),NB) DIS
61 CALL MULT(DUMMY(N2),NF,DUMMY(N1),NB,DUMMY(N3),NR) DIS
62 CALL ADD(R,NR,DUMMY(N3),NR,DUMMY(N1),NR) DIS

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63	IOPT = 3	DIS
64	IAC=IACM	DIS
65	MF = NP(1)	DIS
66	CALL SNVDEC(IOPT, MF, MF, MF, MF, DUMMY(N1), NF(2), F, IAC, ZTEST, DUMMY(N2))	DIS
67	1, DUMMY(N3), IRANK, APLUS, IERR)	DIS
68	IF( IERR .EQ. 0) GO TO 300	DIS
69	CALL LNCNT(5)	DIS
70	IF(IERR .GT. 0) PRINT 200, IERR	DIS
71	IF(IERR .EQ. -1) PRINT 250, ZTEST, IRANK	DIS
72	200 FORMAT(///, ' IN DISREG, SNVDEC HAS FAILED TO CONVERGE TO THE ', I4,	DIS
73	1 'SINGULARVALUE AFTER 30 ITERATIONS', //)	DIS
74	250 FORMAT(///, ' IN DISREG, THE MATRIX SUBMITTED TO SNVDEC USING ZTEST	DIS
75	1=' ,D16.8, ' IS CLOSE TO A MATRIX OF LOWER RANK', //, 'IF THE ACCURACY	DIS
76	2 IAC IS REDUCED THE RANK MAY ALSO BE REDUCED', //, ' CURRENT RANK = '	DIS
77	3 , I4)	DIS
78	IF( IERR .GT. 0 ) RETURN	DIS
79	NDUM(1) = NA(1)	DIS
80	NDUM(2) = 1	DIS
81	CALL PRNT(DUMMY(N2), NDUM, 4HSGVL, 1)	DIS
82	C	DIS
83	300 CONTINUE	DIS
84	CALL MULT(R, NR, F, NF, DUMMY(N1), NF)	DIS
85	CALL TRANP(F, NF, DUMMY(N2), NB)	DIS
86	CALL MULT(DUMMY(N2), NB, DUMMY(N1), NF, P, NP)	DIS
87	CALL ADD(Q, NQ, P, NP, P, NP)	DIS
88	CALL MULT(B, NB, F, NF, DUMMY(N1), NA)	DIS
89	CALL SUBT(A, NA, DUMMY(N1), NA, DUMMY(N1), NA)	DIS
90	CALL MULT(DUMMY, NA, DUMMY(N1), NA, DUMMY(N2), NA)	DIS
91	CALL TRANP(DUMMY(N1), NA, DUMMY(N3), NA)	DIS
92	CALL MULT(DUMMY(N3), NA, DUMMY(N2), NA, DUMMY(N1), NA)	DIS
93	CALL ADD(P, NP, DUMMY(N1), NA, P, NP)	DIS
94	C	DIS
95	IF( IOP(2) .EQ. 0 ) GO TO 400	DIS
96	CALL LNCNT(5)	DIS
97	PRINT 350, I	DIS
98	350 FORMAT(///, ' STAGE ', I5, //)	DIS
99	CALL PRNT(F, NF, 4H F , 1)	DIS
100	CALL PRNT(P, NP, 4H P , 1)	DIS
101	C	DIS
102	400 CONTINUE	DIS
103	IF( I .EQ. 0 ) GO TO 600	DIS
104	CALL MAXEL(DUMMY, NP, ANORM1)	DIS
105	CALL SUBT(DUMMY, NP, P, NP, DUMMY(N2), NP)	DIS
106	CALL MAXEL(DUMMY(N2), NP, ANORM2)	DIS
107	IF( ANORM1 .NE. 0.0 ) GO TO 500	DIS
108	GO TO 100	DIS
109	C	DIS
110	500 CONTINUE	DIS
111	IF(ANORM1 .GT. 1.0 ) GO TO 550	DIS
112	IF( ANORM2/ANORM1 .LT. RICTCV ) KSS = 1	DIS
113	GO TO 575	DIS
114	550 CONTINUE	DIS
115	IF( ANORM2 .LT. RICTCV ) KSS=1	DIS
116	575 CONTINUE	DIS
117	IF( KSS .EQ. 1) GO TO 600	DIS
118	GO TO 100	DIS
119	C	DIS
120	600 CONTINUE	DIS
121	K = IOP(1) + IOP(2)	DIS
122	IF( K .EQ. 0 ) RETURN	DIS
123	IF( KSS .EQ. 0) GO TO 700	DIS
124	CALL LNCNT(4)	DIS
125	PRINT 650	DIS

126	650	FORMAT(/, ' STEADY-STATE SOLUTION HAS BEEN REACHED IN DISREG', /)	DIS01
127	C		DIS01
128	700	CONTINUE	DIS01
129		IF( IOP(2) .NE. 0 ) RETURN	DIS01
130		IF( IOP(1) .EQ. 0 ) RETURN	DIS01
131		CALL LNCNT(3)	DIS01
132		I = IOP(3)-1	DIS01
133		PRINT 800, I	DIS01
134	800	FORMAT(/, ' F AND P AFTER ', I5, ' STEPS', /)	DIS01
135		CALL PRNT(F, NF, 4H F , 1)	DIS01
136		CALL PRNT(P, NP, 4H P , 1)	DIS01
137		RETURN	DIS01
138		END	DIS01

0	SUBROUTINE CNTREG(A,NA,B,NB,H,NH,Q,NQ,R,NR,Z,W,LAMBOA,S,F,NF,P,NP	CNT
1	1,T,IOP,IDENT,DUMMY)	CNT
2	IMPLICIT REAL*8 (A-H,O-Z)	CNT
3	C	CNT
4	DIMENSION A(1),B(1),H(1),Q(1),R(1),Z(1),W(1),LAMBOA(1),S(1),F(1),P	CNT
5	1(1),T(1),DUMMY(1)	CNT
6	DIMENSION NA(2),NB(2),NH(2),NQ(2),NR(2),NF(2),NP(2),IOP(3),NDUM1(2	CNT
7	1),NDUM2(2)	CNT
8	LOGICAL IDENT	CNT
9	REAL*8 LAMBOA	CNT
10	COMMON/CONV/SUMCV,RICTCV,SERCV,MAXSUM	CNT
11	C	CNT
12	IF( IOP(1) .EQ. 0 ) GO TO 65	CNT
13	CALL LNCNT(5)	CNT
14	IF( IOP(3) .EQ. 0 ) PRINT 25	CNT
15	25 EFORMAT(// ' PROGRAM TO SOLVE THE TIME-INVARIANT FINITE-DURATION CONC	CNT
16	1 TINUOUS OPTIMAL'// ' REGULATOR PROBLEM WITH NOISE-FREE MEASUREMENTS'	CNT
17	2)	CNT
18	IF( IOP(3) .NE. 0 ) PRINT 30	CNT
19	30 FORMAT(// ' PROGRAM TO SOLVE THE TIME-INVARIANT INFINITE-DURATION C	CNT
20	1 ONTINUOUS OPTIMAL'// ' REGULATOR PROBLEM WITH NOISE-FREE MEASUREMEN	CNT
21	2 TS')	CNT
22	CALL PRNT(A,NA,4H A ,1)	CNT
23	CALL PRNT(B,NB,4H B ,1)	CNT
24	CALL PRNT(Q,NQ,4H Q ,1)	CNT
25	IF( .NOT. IDENT ) GO TO 45	CNT
26	CALL LNCNT(3)	CNT
27	PRINT 35	CNT
28	35 FORMAT(// ' H IS AN IDENTITY MATRIX'//)	CNT
29	GO TO 55	CNT
30	C	CNT
31	45 CONTINUE	CNT
32	CALL PRNT(H,NH,4H H ,1)	CNT
33	CALL MULT(Q,NQ,H,NH,DUMMY,NH)	CNT
34	N1 = NH(1)*NH(2)+1	CNT
35	CALL TRANP(H,NH,DUMMY(N1),NDUM1)	CNT
36	CALL MULT(DUMMY(N1),NDUM1,DUMMY,NH,Q,NQ)	CNT
37	CALL LNCNT(3)	CNT
38	PRINT 50	CNT
39	50 FORMAT(// ' MATRIX (H TRANSPOSE)QH'//)	CNT
40	CALL PRNT(Q,NQ,0,3)	CNT
41	55 CONTINUE	CNT
42	CALL PRNT(R,NR,4H R ,1)	CNT
43	C	CNT
44	IF( IOP(3) .NE. 0 ) GO TO 65	CNT
45	CALL LNCNT(4)	CNT
46	PRINT 60	CNT
47	60 FORMAT(// ' WEIGHTING ON TERMINAL VALUE OF STATE VECTOR'//)	CNT
48	CALL PRNT(P,NP,4H P ,1)	CNT
49	C	CNT
50	65 CONTINUE	CNT
51	CALL EQUATE(R,NR,DUMMY,NR)	CNT
52	N = NA(1)*2	CNT
53	N1 = NR(1)+NB(2)+1	CNT
54	CALL TRANP(B,NB,DUMMY(N1),NDUM1)	CNT
55	N2 = N1 + N	CNT
56	L = NR(1)	CNT
57	IOPT = 0	CNT
58	IFAC = 0	CNT
59	CALL SYMPDS(L,L,DUMMY,NB(1),DUMMY(N1),IOPT,IFAC,DET,ISCALE,DUMMY(N	CNT
60	12),IERR)	CNT
61	C	CNT
62	IF( IERR .EQ. 0 ) GO TO 100	CNT

63	CALL LNCNT(4)	CNT0
64	PRINT 75	CNT0
65	75 FORMAT(/// ' IN CNTREG, THE SUBROUTINE SYMPOS HAS FOUND THE MATRIX	CNT0
66	1 R NOT SYMMETRIC POSITIVE DEFINITE'//)	CNT0
67	RETURN	CNT0
68	C	CNT0
69	100 CONTINUE	CNT0
70	CALL EQUATE(DUMMY(N1),NDUM1,DUMMY,NDUM1)	CNT0
71	CALL MULT(B,NB,DUMMY(N1),NDUM1,DUMMY(N2),NA)	CNT0
72	CALL SCALE(DUMMY(N2),NA,DUMMY(N1),NA,-1.0)	CNT0
73	N3 = N2 + N	CNT0
74	IF( IDENT .OR. (IOP(1) .NE. 0) ) GO TO 200	CNT0
75	CALL MULT(Q,NQ,H,NH,DUMMY(N2),NH)	CNT0
76	CALL TRANSP(H,NH,DUMMY(N3),NDUM1)	CNT0
77	CALL MULT(DUMMY(N3),NDUM1,DUMMY(N2),NH,Q,NQ)	CNT0
78	C	CNT0
79	200 CONTINUE	CNT0
80	CALL SCALE(Q,NQ,Q,NQ,-1.0)	CNT0
81	CALL JUXTR(A,NA,Q,NQ,Z,NDUM1)	CNT0
82	CALL TRANSP(A,NA,DUMMY(N2),NA)	CNT0
83	CALL SCALE(DUMMY(N2),NA,DUMMY(N2),NA,-1.0)	CNT0
84	L = 2*N + 1	CNT0
85	CALL JUXTR(DUMMY(N1),NA,DUMMY(N2),NA,Z(L),NDUM1)	CNT0
86	CALL SCALE(Q,NQ,Q,NQ,-1.0)	CNT0
87	NDUM2(1) = 2*NA(1)	CNT0
88	NDUM2(2) = NDUM2(1)	CNT0
89	IF( IOP(1) .NE. 0 ) CALL PRNT(Z,NDUM2,4H Z ,1)	CNT0
90	CALL EQUATE(Z,NDUM2,DUMMY(N1),NDUM2)	CNT0
91	M = 4*N	CNT0
92	N2 = M + N1	CNT0
93	L = 2*NA(1)	CNT0
94	N3 = N2 + L	CNT0
95	N4 = N3 + L	CNT0
96	ISV = L	CNT0
97	ILV = 0	CNT0
98	CALL EIGEN(L,L,DUMMY(N1),DUMMY(N2),DUMMY(N3),ISV,ILV,W,DUMMY(N4),I	CNT0
99	1ERR)	CNT0
100	IF( IERR .EQ. 0 ) GO TO 300	CNT0
101	CALL LNCNT(4)	CNT0
102	IF( IERR .GT. 0 ) GO TO 250	CNT0
103	PRINT 225,IERR	CNT0
104	225 FORMAT(/// ' IN CNTREG, EIGEN FAILED TO COMPUTE THE ',I6,' EIGENVEC	CNT0
105	1TOR OF Z'//)	CNT0
106	RETURN	CNT0
107	250 CONTINUE	CNT0
108	PRINT 275,IERR	CNT0
109	275 FORMAT(/// ' IN CNTREG, THE ',I6,' EIGENVALUE OF Z HAS NOT BEEN FO	CNT0
110	UND AFTER 30 ITERATIONS IN EIGEN'//)	CNT0
111	RETURN	CNT0
112	C	CNT0
113	300 CONTINUE	CNT0
114	IF( IOP(1) .EQ. 0 ) GO TO 400	CNT0
115	CALL LNCNT(3)	CNT0
116	PRINT 325	CNT0
117	325 FORMAT(/// ' EIGENVALUES OF Z'//)	CNT0
118	NDUM1(1) = L	CNT0
119	NDUM1(2) = 2	CNT0
120	CALL PRNT(DUMMY(N2),NDUM1,0,3)	CNT0
121	CALL LNCNT(3)	CNT0
122	PRINT 350	CNT0
123	350 FORMAT(/// ' CORRESPONDING EIGENVECTORS'//)	CNT0
124	CALL PRNT(W,NDUM2,0,3)	CNT0
125	C	CNT0

126	400	CONTINUE	CNT
127		CALL EQUATE(W,NDUM2,DUMMY(N1),NDUM2)	CNT
128		J1 = 1	CNT
129		J2 = 1	CNT
130		M = 2*N	CNT
131		NDUM1(1) = L	CNT
132		NDUM1(2) = 1	CNT
133		K4 = N4	CNT
134	C		CNT
135		I=1	CNT
136	415	CONTINUE	CNT
137		IF( I .GT. L ) GO TO 515	CNT
138		K1 = N2+I-1	CNT
139		K2 = N1+(I-1)*L	CNT
140		K3 = N3+I-1	CNT
141		IF(DUMMY(K1) .GT. 0.0 ) GO TO 425	CNT
142		J = (J1-1)*L+M+1	CNT
143		J1 = J1+1	CNT
144		IF(DUMMY(K3) .NE. 0.0 ) J1=J1+1	CNT
145		GO TO 450	CNT
146	425	CONTINUE	CNT
147		DUMMY(K4)=I	CNT
148		K4 = K4+1	CNT
149		J = (J2-1)*L+1	CNT
150		J2 = J2+1	CNT
151		IF( DUMMY(K3) .NE. 0.0 ) J2 = J2 + 1	CNT
152	450	CONTINUE	CNT
153		CALL EQUATE(DUMMY(K2),NDUM1,W(J),NDUM1)	CNT
154		IF(DUMMY(K3) .EQ. 0.0) GO TO 500	CNT
155		I = I+1	CNT
156		K2 = K2+L	CNT
157		J = J+L	CNT
158		CALL EQUATE(DUMMY(K2),NDUM1,W(J),NDUM1)	CNT
159	500	CONTINUE	CNT
160		I=I+1	CNT
161		GO TO 415	CNT
162	515	CONTINUE	CNT
163	C		CNT
164		CALL NULL(LAMBDA,NA)	CNT
165		K0 = -1	CNT
166		J = -NA(1)	CNT
167		NAX = NA(1)	CNT
168		I=1	CNT
169	520	CONTINUE	CNT
170		IF( I .GT. NAX ) GO TO 530	CNT
171		J = NAX + J + 1	CNT
172		K0 = K0 + 1	CNT
173		K1 = N4 + K0	CNT
174		K2 = DUMMY(K1)	CNT
175		K = N2+K2-1	CNT
176		LAMBDA(J) = DUMMY(K)	CNT
177		K3 = N3+K2-1	CNT
178		IF( DUMMY(K3) .EQ. 0.0 ) GO TO 525	CNT
179		K4 = J+1	CNT
180		LAMBDA(K4) = -DUMMY(K3)	CNT
181		K4 = K4+NAX	CNT
182		LAMBDA(K4) = DUMMY(K)	CNT
183		K4 = K4-1	CNT
184		LAMBDA(K4) = DUMMY(K3)	CNT
185		K5 = M + (I-1)*L + 1	CNT
186		K6 = K5 + L	CNT
187		CALL EQUATE(W(K5),NDUM1,DUMMY(N1),NDUM1)	CNT
188		CALL EQUATE(W(K6),NDUM1,W(K5),NDUM1)	CNT

189	CALL EQUATE(DUMMY(N1),NDUM1,W(K6),NDUM1)	CNT0
190	I = I+1	CNT0
191	J = NAX + J + 1	CNT0
192	525 CONTINUE	CNT0
193	I=I+1	CNT0
194	GO TO 520	CNT0
195	530 CONTINUE	CNT0
196	C	CNT0
197	IF( IOP(1) .EQ. 0 ) GO TO 700	CNT0
198	CALL LNCNT(3)	CNT0
199	PRINT 535	CNT0
200	535 FORMAT(// ' REORDERED EIGENVECTORS ')	CNT0
201	CALL PRNT(W,NDUM2,0,3)	CNT0
202	CALL LNCNT(4)	CNT0
203	PRINT 545	CNT0
204	545 FORMAT(// ' LAMBDA MATRIX OF EIGENVALUES OF Z WITH POSITIVE REAL PARTS ')	CNT0
205	1RTS ')	CNT0
206	CALL PRNT(LAMBDA,NA,0,3)	CNT0
207	C	CNT0
208	CALL MULT(Z,NDUM2,W,NDUM2,DUMMY(N1),NDUM2)	CNT0
209	L = NDUM2(1)	CNT0
210	M = L**2	CNT0
211	N2 = N1+M	CNT0
212	CALL EQUATE(W,NDUM2,DUMMY(N2),NDUM2)	CNT0
213	N3 = N2+M	CNT0
214	N4 = N3+L	CNT0
215	IFAC = 0	CNT0
216	CALL GELIM(L,L,DUMMY(N2),L,DUMMY(N1),DUMMY(N3),IFAC,DUMMY(N4),IERR)	CNT0
217	1)	CNT0
218	IF( IERR .EQ. 0 ) GO TO 600	CNT0
219	CALL LNCNT(4)	CNT0
220	PRINT 550	CNT0
221	550 FORMAT(// ' IN CNTREG, GELIM HAS FOUND THE REORDERED MATRIX W TO BE SINGULAR ')	CNT0
222	1E SINGULAR ')	CNT0
223	600 CONTINUE	CNT0
224	CALL PRNT(DUMMY(N1),NDUM2,4HWIZW,1)	CNT0
225	C	CNT0
226	700 CONTINUE	CNT0
227	NDUM1(1) = 2*NA(1)	CNT0
228	NDUM1(2) = NA(1)	CNT0
229	N2 = 2*N + N1	CNT0
230	CALL TRANP(W,NDUM1,DUMMY(N2),NDUM2)	CNT0
231	NW11 = N1	CNT0
232	NDUM1(1) = NA(1)	CNT0
233	CALL TRANP(DUMMY(N2),NDUM1,DUMMY(NW11),NDUM1)	CNT0
234	L = N2+N	CNT0
235	NW21 = NW11+N	CNT0
236	CALL TRANP(DUMMY(L),NDUM1,DUMMY(NW21),NDUM1)	CNT0
237	L = 2*N+1	CNT0
238	NDUM1(1)=2*NA(1)	CNT0
239	N3 = N2 + 2*N	CNT0
240	CALL TRANP(W(L),NDUM1,DUMMY(N3),NDUM2)	CNT0
241	NDUM1(1) = NA(1)	CNT0
242	NW12 = NW21+N	CNT0
243	CALL TRANP(DUMMY(N3),NDUM1,DUMMY(NW12),NDUM1)	CNT0
244	L = N3 + N	CNT0
245	NW22 = NW12 + N	CNT0
246	CALL TRANP(DUMMY(L),NDUM1,DUMMY(NW22),NDUM1)	CNT0
247	C	CNT0
248	IF( IOP(1) .EQ. 0 ) GO TO 800	CNT0
249	CALL PRNT(DUMMY(NW11),NA,4HW11,1)	CNT0
250	CALL PRNT(DUMMY(NW21),NA,4HW21,1)	CNT0
251	CALL PRNT(DUMMY(NW12),NA,4HW12,1)	CNT0



252	CALL PRNT(DUMMY(NW22),NA,4HW22 ,1)	CNT0
253	C	CNT0
254	900 CONTINUE	CNT0
255	IF( IOP(3) .NE. 0 ) GO TO 900	CNT0
256	N2 = N1+4*N	CNT0
257	CALL MULT(P,NP,DUMMY(NW12),NA,S,NA)	CNT0
258	CALL MULT(P,NP,DUMMY(NW11),NA,DUMMY(N2),NA)	CNT0
259	CALL SUBT(S,NA,DUMMY(NW22),NA,S,NA)	CNT0
260	CALL SUBT(DUMMY(NW21),NA,DUMMY(N2),NA,DUMMY(N2),NA)	CNT0
261	N3 = N2+N	CNT0
262	L = NA(1)	CNT0
263	IFAC = 0	CNT0
264	N4 = N3+NA(1)	CNT0
265	CALL GELIM(L,L,DUMMY(N2),L,S,DUMMY(N3),IFAC,DUMMY(N4),IERR)	CNT0
266	IF( IERR .EQ. 0 ) GO TO 850	CNT0
267	CALL LNCNT(4)	CNT0
268	PRINT 825	CNT0
269	825 FORMAT(// ' IN CNTREG, GELIM HAS FOUND THE MATRIX W21 = P1XW11 TO	CNT0
270	BE SINGULAR'//)	CNT0
271	RETURN	CNT0
272	C	CNT0
273	850 CONTINUE	CNT0
274	IF( IOP(1) .EQ. 0 ) GO TO 1000	CNT0
275	CALL PRNT(S,NA,4H S ,1)	CNT0
276	NDUM1(1) = NR(1)	CNT0
277	NDUM1(2) = NA(1)	CNT0
278	CALL LNCNT(3)	CNT0
279	PRINT 875	CNT0
280	875 FORMAT(// ' MATRIX (R INVERSE)X(B TRANSPOSE)'	CNT0
281	CALL PRNT(DUMMY,NDUM1,0,3)	CNT0
282	GO TO 1000	CNT0
283	C	CNT0
284	900 CONTINUE	CNT0
285	N2 = N1+4*N	CNT0
286	CALL TRANSP(DUMMY(NW12),NA,DUMMY(N2),NA)	CNT0
287	CALL TRANSP(DUMMY(NW22),NA,P,NP)	CNT0
288	N3 = N2+N	CNT0
289	IFAC = 0	CNT0
290	L = NA(1)	CNT0
291	N4 = N3 + NA(1)	CNT0
292	CALL GELIM(L,L,DUMMY(N2),L,P,DUMMY(N3),IFAC,DUMMY(N4),IERR)	CNT0
293	IF( IERR .EQ. 0 ) GO TO 950	CNT0
294	CALL LNCNT(4)	CNT0
295	PRINT 925	CNT0
296	925 FORMAT(// ' IN CNTREG, GELIM HAS FOUND THE MATRIX W12 TO BE SINGUL	CNT0
297	AR'//)	CNT0
298	RETURN	CNT0
299	950 CONTINUE	CNT0
300	NDUM1(1) = NR(1)	CNT0
301	NDUM1(2) = NA(1)	CNT0
302	CALL MULT(DUMMY,NDUM1,P,NP,F,NF)	CNT0
303	IF( IOP(1) .EQ. 0 ) RETURN	CNT0
304	CALL PRNT(P,NP,4H P ,1)	CNT0
305	CALL PRNT(F,NF,4H F ,1)	CNT0
306	RETURN	CNT0
307	C	CNT0
308	1000 CONTINUE	CNT0
309	NMAX = T(1)/T(2)	CNT0
310	I = NMAX	CNT0
311	CALL EQUATE(LAMBDA,NA,DUMMY(N2),NA)	CNT0
312	TT = -T(2)	CNT0
313	N4 = N3+N	CNT0
314	N5 = N4+N	CNT0

315	N6 = N5+N	CNT
316	N7 = N6+NA(1)	CNT
317	KSS = 0	CNT
318	NDUM1(1) = NR(1)	CNT
319	NDUM1(2) = NA(1)	CNT
320	CALL EXPSER(DUMMY(N2),NA,DUMMY(N3),NA,TT,KSS,DUMMY(N4))	CNT
321	CALL EQUATE(DUMMY(N3),NA,DUMMY(N2),NA)	CNT
322	IF( IOP(1) .EQ. 0 ) GO TO 1075	CNT
323	CALL LNCNT(3)	CNT
324	PRINT 1050,T(2)	CNT
325	1050 FORMAT(// ' EXP(-LAMBDA X ',D16.8,')')	CNT
326	CALL PRNT(DUMMY(N2),NA,0,3)	CNT
327	1075 CONTINUE	CNT
328	IF( NMAX .LE. 0 ) RETURN	CNT
329	CALL EQUATE(S,NA,DUMMY(N3),NA)	CNT
330	1100 CONTINUE	CNT
331	TIME = I*T(2)	CNT
332	IF( I .NE. NMAX ) CALL EQUATE(DUMMY(N5),NA,P,NP)	CNT
333	CALL MULT(DUMMY(N3),NA,DUMMY(N2),NA,DUMMY(N4),NA)	CNT
334	CALL MULT(DUMMY(N2),NA,DUMMY(N4),NA,DUMMY(N3),NA)	CNT
335	CALL MULT(DUMMY(NW11),NA,DUMMY(N3),NA,DUMMY(N4),NA)	CNT
336	CALL ADD(DUMMY(NW12),NA,DUMMY(N4),NA,DUMMY(N4),NA)	CNT
337	CALL TRANSP(DUMMY(N4),NA,DUMMY(N5),NA)	CNT
338	CALL EQUATE(DUMMY(N5),NA,DUMMY(N4),NA)	CNT
339	CALL MULT(DUMMY(NW21),NA,DUMMY(N3),NA,DUMMY(N5),NA)	CNT
340	CALL ADD(DUMMY(NW22),NA,DUMMY(N5),NA,DUMMY(N5),NA)	CNT
341	CALL TRANSP(DUMMY(N5),NA,DUMMY(N6),NA)	CNT
342	CALL EQUATE(DUMMY(N6),NA,DUMMY(N5),NA)	CNT
343	L = NA(1)	CNT
344	IFAC = 0	CNT
345	CALL GELIM(L,L,DUMMY(N4),L,DUMMY(N5),DUMMY(N6),IFAC,DUMMY(N7),IERR	CNT
346	1)	CNT
347	IF( IERR .EQ. 0 ) GO TO 1200	CNT
348	CALL LNCNT(3)	CNT
349	PRINT 1150,TIME	CNT
350	1150 FORMAT(// ' IN CNTREG AT TIME ',D16.8, ' P CANNOT BE COMPUTED DUE T	CNT
351	10 MATRIX SINGULARITY IN GELIM')	CNT
352	RETURN	CNT
353	C	CNT
354	1200 CONTINUE	CNT
355	CALL MAXEL(P,NP,ANORM1)	CNT
356	CALL SUBT(DUMMY(N5),NA,P,NP,DUMMY(N4),NA)	CNT
357	CALL MAXEL(DUMMY(N4),NA,ANORM2)	CNT
358	IF( ANORM1 .NE. 0.0 ) GO TO 1225	CNT
359	GO TO 1300	CNT
360	C	CNT
361	1225 CONTINUE	CNT
362	IF(ANORM1 .GT. 1.0 ) GO TO 1250	CNT
363	IF( ANORM2/ANORM1 .LT. RICTCV ) KSS=1	CNT
364	GO TO 1300	CNT
365	1250 CONTINUE	CNT
366	IF( ANORM2 .LT. RICTCV ) KSS=1	CNT
367	C	CNT
368	1300 CONTINUE	CNT
369	CALL MULT(DUMMY,NDUM1,P,NP,F,NF)	CNT
370	IF( IOP(2) .EQ. 0 ) GO TO 1400	CNT
371	CALL LNCNT(5)	CNT
372	PRINT 1350,TIME	CNT
373	1350 FORMAT(/// ' TIME = ',D16.8/)	CNT
374	CALL PRNT(P,NP,4H P ,1)	CNT
375	IF( I .NE. NMAX ) CALL PRNT(F,NF,4H F ,1)	CNT
376	C	CNT
377	1400 CONTINUE	CNT

378	IF( KSS .EQ. 1 ) GO TO 1500	CNT
379	I = I-1	CNT
380	IF( I .GE. 0 ) GO TO 1100	CNT
381	GO TO 1600	CNT
382	1500 CONTINUE	CNT
383	CALL LNCNT(4)	CNT
384	PRINT 1550	CNT
385	1550 FORMAT(// ' STEADY-STATE SOLUTION HAS BEEN REACHED IN CNTREG'//)	CNT
386	C	CNT
387	1600 CONTINUE	CNT
388	IF( IOP(2) .NE. 0 ) RETURN	CNT
389	IF( IOP(1) .EQ. 0 ) RETURN	CNT
390	CALL LNCNT(5)	CNT
391	PRINT 1350, TIME	CNT
392	CALL PRNT(P, NP, 4H P , 1)	CNT
393	CALL PRNT(F, NF, 4H F , 1)	CNT
394	C	CNT
395	RETURN	LNT
396	END	CNT

0	SUBROUTINE RICNWT(A,NA,B,NB,H,NH,Q,NQ,R,NR,F,NF,P,NP,IOP,IDENT,DI	RIC00
1	ISC,FNULL,DUMMY)	RIC00
2	IMPLICIT REAL*8 (A-H,O-Z)	RIC00
3	DIMENSION A(1),B(1),Q(1),R(1),F(1),P(1),DUMMY(1)	RIC00
4	DIMENSION NA(2),NB(2),NQ(2),NR(2),NF(2),NP(2),IOP(3)	RIC00
5	DIMENSION H(1),NH(2),IOPT(2)	RIC00
6	LOGICAL IDENT,DISC,FNULL,SYM	RIC00
7	COMMON/TOL/EP3AM,EP3BM,IACM	RIC00
8	COMMON/CONV/SUMCV,RICTCV,SERCV,MAXSUM	RIC00
9	I=1	RIC00
10	IOPT(1)=0	RIC00
11	SYM = .TRUE.	RIC00
12 C		RIC00
13	N = NA(1)**2	RIC00
14	N1 = N + 1	RIC00
15	IF( .NOT. DISC) N1 = NA(1)*NR(1) + 1	RIC00
16	N2= N1+N	RIC00
17	N3= N2+N	RIC00
18	N4 = N3+N	RIC00
19 C		RIC00
20	IF( IOP(1) .EQ. 0 ) GO TO 210	RIC00
21	CALL LNCNT(4)	RIC00
22	IF(.NOT. DISC)PRINT 100	RIC00
23	IF( DISC )PRINT 150	RIC00
24	100 FORMAT(/, ' PROGRAM TO SOLVE CONTINUOUS STEADY-STATE RICCATI EQUATRIC00	
25	ION BY THE NEWTON ALGORITHM',/)	RIC00
26	150 FORMAT(/, ' PROGRAM TO SOLVE DISCRETE STEADY-STATE RICCATI EQUATIORIC00	
27	IN BY THE NEWTON ALGORITHM',/)	RIC00
28	CALL PRNT(A,NA,4H A ,1)	RIC00
29	CALL PRNT(B,NB,4H B ,1)	RIC00
30	CALL PRNT(Q,NQ,4H Q ,1)	RIC00
31	IF( .NOT. IDENT )GO TO 185	RIC00
32	CALL LNCNT(3)	RIC00
33	PRINT 180	RIC00
34	180 FORMAT(/, ' H IS AN IDENTITY MATRIX',/)	RIC00
35	GO TO 200	RIC00
36	185 CONTINUE	RIC00
37	CALL PRNT(H,NH,4H H ,1)	RIC00
38	CALL MULT(Q,NQ,H,NH,DUMMY,NH)	RIC00
39	CALL TRANSP(H,NH,DUMMY(N2),NP)	RIC00
40	CALL MULT(DUMMY(N2),NP,DUMMY,NH,Q,NQ)	RIC00
41	CALL LNCNT(3)	RIC00
42	PRINT 195	RIC00
43	195 FORMAT(/, ' MATRIX (H TRANSPOSE)QH ',/)	RIC00
44	CALL PRNT(Q,NQ,4HHTQH,1)	RIC00
45	200 CONTINUE	RIC00
46	CALL PRNT(R,NR,4H R ,1)	RIC00
47	IF( FNULL ) GO TO 210	RIC00
48	CALL LNCNT(3)	RIC00
49	PRINT 205	RIC00
50	205 FORMAT(/, ' INITIAL F MATRIX',/)	RIC00
51	CALL PRNT(F,NF,4H F ,1)	RIC00
52 C		RIC00
53	210 CONTINUE	RIC00
54	IF((IOP(1) .NE. 0) .OR. IDENT) GO TO 220	RIC00
55	CALL MULT(Q,NQ,H,NH,DUMMY,NH)	RIC00
56	CALL TRANSP(H,NH,DUMMY(N2),NP)	RIC00
57	CALL MULT(DUMMY(N2),NP,DUMMY,NH,Q,NQ)	RIC00
58	220 CONTINUE	RIC00
59 C		RIC00
60	IF (DISC) GO TO 900	RIC00
61 C		RIC00
62	CALL TRANSP(B,NB,P,NP)	RIC00

63	CALL EQUATE(R,NR,DUMMY,NR)	RIC
64	CALL SYMPOS(NR(1),NR(1),DUMMY,NP(2),P,IOP,IOPT,DET,ISCALE,DUMMY(NR(1),IERR)	RIC
65	IF(IERR.EQ. 0) GO TO 250	RIC
66	CALL LNCNT(3)	RIC
67	PRINT 225	RIC
68	225 FORMAT(/, ' IN RICNWT, A MATRIX WHICH IS NOT SYMMETRIC POSITIVE DERIC	RIC
69	IFINITE HAS BEEN SUBMITTED TO SYMPOS',/)	RIC
70	RETURN	RIC
71		RIC
72	C	RIC
73	250 CONTINUE	RIC
74	CALL EQUATE(P,NP,DUMMY,NF)	RIC
75	CALL MULT(B,NB,DUMMY,NF,DUMMY(N1),NA)	RIC
76	CALL TRANP(DUMMY(N1),NA,DUMMY(N2),NA)	RIC
77	CALL ADD(DUMMY(N1),NA,DUMMY(N2),NA,DUMMY(N1),NA)	RIC
78	CALL SCALE(DUMMY(N1),NA,DUMMY(N1),NA,0.5)	RIC
79	C	RIC
80	IF(FNULL) GO TO 300	RIC
81	C	RIC
82	CALL MULT(B,NB,F,NF,DUMMY(N2),NA)	RIC
83	CALL SUBT(A,NA,DUMMY(N2),NA,DUMMY(N2),NA)	RIC
84	CALL TRANP(DUMMY(N2),NA,DUMMY(N3),NA)	RIC
85	CALL EQUATE(DUMMY(N3),NA,DUMMY(N2),NA)	RIC
86	CALL MULT(R,NR,F,NF,DUMMY(N3),NF)	RIC
87	CALL TRANP(F,NF,P,NP)	RIC
88	CALL MULT(P,NP,DUMMY(N3),NF,DUMMY(N4),NA)	RIC
89	CALL TRANP(DUMMY(N4),NA,DUMMY(N3),NA)	RIC
90	CALL ADD(DUMMY(N4),NA,DUMMY(N3),NA,DUMMY(N3),NA)	RIC
91	CALL SCALE(DUMMY(N3),NA,DUMMY(N3),NA,0.5)	RIC
92	CALL ADD(DUMMY(N3),NA,Q,NQ,P,NP)	RIC
93	CALL SCALE(P,NP,P,NP,-1.0)	RIC
94	GO TO 350	RIC
95	C	RIC
96	300 CONTINUE	RIC
97	CALL TRANP(A,NA,DUMMY(N2),NA)	RIC
98	CALL SCALE(Q,NQ,P,NP,-1.0)	RIC
99	C	RIC
100	350 CONTINUE	RIC
101	IF(IOP(3).NE. 0) GO TO 400	RIC
102	EPSA= EPSAM	RIC
103	CALL BARSTW(DUMMY(N2),NA,B,NB,P,NP,IOPT,SYM,EPSA,EPSA,DUMMY(N3))	RIC
104	GO TO 450	RIC
105	C	RIC
106	400 CONTINUE	RIC
107	IOPT(2)=1	RIC
108	CALL BILIN(DUMMY(N2),NA,B,NB,P,NP,IOPT,SCLE,SYM,DUMMY(N3))	RIC
109	C	RIC
110	450 CONTINUE	RIC
111	CALL EQUATE(P,NP,DUMMY(N2),NP)	RIC
112	IF(IOP(2).EQ. 0) GO TO 550	RIC
113	CALL LNCNT(3)	RIC
114	PRINT 500,I	RIC
115	500 FORMAT(/, ' ITERATION ',IS,/)	RIC
116	CALL PRNT(P,NP,4H P ,1)	RIC
117	C	RIC
118	550 CONTINUE	RIC
119	CALL MULT(DUMMY(N1),NA,P,NP,DUMMY(N3),NA)	RIC
120	CALL MULT(P,NP,DUMMY(N3),NA,DUMMY(N4),NA)	RIC
121	CALL TRANP(DUMMY(N4),NA,P,NA)	RIC
122	CALL ADD(P,NP,DUMMY(N4),NA,P,NP)	RIC
123	CALL SCALE(P,NP,P,NP,0.5)	RIC
124	CALL ADD(Q,NQ,P,NP,P,NP)	RIC
125	CALL SCALE(P,NP,P,NP,-1.0)	RIC

126	CALL SUBT(A,NA,DUMMY(N3),NA,DUMMY(N4),NA)	RIC01
127	CALL TRANSP(DUMMY(N4),NA,DUMMY(N3),NA)	RIC01
128 C		RIC01
129	IF(IOP(3) .NE. 0 ) GO TO 650	RIC01
130	CALL BARSTW(DUMMY(N3),NA,B,NB,P,NP,IOPT,SYM,EPSA,EPSA,DUMMY(N4))	RIC01
131	GO TO 675	RIC01
132 C		RIC01
133 650	CONTINUE	RIC01
134	CALL RILIN(DUMMY(N3),NA,B,NB,P,NP,IOPT,SCLE,SYM,DUMMY(N4))	RIC01
135 C		RIC01
136 675	CONTINUE	RIC01
137	I=I+1	RIC01
138	CALL MAXEL(DUMMY(N2),NA,ANORM1)	RIC01
139	CALL SUBT(P,NP,DUMMY(N2),NA,DUMMY(N3),NA)	RIC01
140	CALL MAXEL(DUMMY(N3),NA,ANORM2)	RIC01
141	IF(ANORM1 .GT. 1.0) GO TO 700	RIC01
142	IF( ANORM2/ANORM1 .LT. RICTCV ) GO TO 800	RIC01
143	GO TO 750	RIC01
144 C		RIC01
145 700	CONTINUE	RIC01
146	IF( ANORM2 .LT. RICTCV ) GO TO 800	RIC01
147 C		RIC01
148 750	CONTINUE	RIC01
149	IF( I .LE. 101) GO TO 450	RIC01
150	CALL LNCNT(3)	RIC01
151	PRINT 775	RIC01
152 775	FORMAT(/, ' THE SUBROUTINE RICNWT HAS EXCEEDED 100 ITERATIONS WITHORIC01	RIC01
153	UT CONVERGENCE',/)	RIC01
154	IOP(1) = 1	RIC01
155 C		RIC01
156 800	CONTINUE	RIC01
157	CALL MULT(DUMMY,NF,P,NP,F,NF)	RIC01
158	GO TO 1300	RIC01
159 C		RIC01
160 900	CONTINUE	
161	IF( .NOT. FNULL ) GO TO 950	RIC01
162 C		RIC01
163	CALL EQUATE(Q,NQ,P,NP)	RIC01
164	CALL EQUATE(A,NA,DUMMY(N1),NA)	RIC01
165	CALL TRANSP(A,NA,DUMMY(N2),NA)	RIC01
166	GO TO 1000	RIC01
167 925	CONTINUE	RIC01
168 C		RIC01
169	I=I+1	RIC01
170	CALL EQUATE(P,NP,DUMMY,NP)	RIC01
171 950	CONTINUE	RIC01
172 C		RIC01
173	CALL MULT(R,NR,F,NF,DUMMY(N1),NF)	RIC01
174	CALL TRANSP(F,NF,P,NP)	RIC01
175	CALL MULT(P,NP,DUMMY(N1),NF,DUMMY(N2),NA)	RIC01
176	CALL TRANSP(DUMMY(N2),NA,DUMMY(N1),NA)	RIC01
177	CALL ADD(DUMMY(N1),NA,DUMMY(N2),NA,DUMMY(N1),NA)	RIC01
178	CALL SCALE(DUMMY(N1),NA,DUMMY(N1),NA,0.5)	RIC01
179	CALL ADD(Q,NQ,DUMMY(N1),NA,P,NP)	RIC01
180	CALL MULT(B,NB,F,NF,DUMMY(N1),NA)	RIC01
181	CALL SUBT(A,NA,DUMMY(N1),NA,DUMMY(N1),NA)	RIC01
182	CALL TRANSP(DUMMY(N1),NA,DUMMY(N2),NA)	RIC01
183 C		RIC01
184 1000	CONTINUE	RIC01
185	CALL SUM(DUMMY(N2),NA,P,NP,DUMMY(N1),NA,IOPT,SYM,DUMMY(N3))	RIC01
186	IF(IOP(2) .EQ. 0) GO TO 1100	RIC01
187	CALL LNCNT(3)	RIC01
188	PRINT 500,I	RIC01

189	CALL PRNT(P,NP,4H P ,1)	RIC0
190 C		RIC0
191 1100	CONTINUE	RIC0
192	CALL MULT(P,NP,4,NA,DUMMY(N1),NA)	RIC0
193	CALL MULT(P,NP,8,NB,DUMMY(N2),NB)	RIC0
194	CALL TRANP(B,NB,DUMMY(N3),NF)	RIC0
195	CALL MULT(DUMMY(N3),NF,DUMMY(N1),NA,F,NF)	RIC0
196	CALL MULT(DUMMY(N3),NF,DUMMY(N2),NB,DUMMY(N1),NR)	RIC0
197	CALL TRANP(DUMMY(N1),NR,DUMMY(N2),NR)	RIC0
198	CALL ADD(DUMMY(N1),NR,DUMMY(N2),NR,DUMMY(N1),NR)	RIC0
199	CALL SCALE(DUMMY(N1),NR,DUMMY(N1),NR,0.5)	RIC0
200	CALL ADD(R,NR,DUMMY(N1),NR,DUMMY(N1),NR)	RIC0
201	CALL SYMPS(NR(1),NR(1),DUMMY(N1),NA(1),F,IOPT,IOPT,DET,ISCALE,DUM	RIC0
202	MY(N2),IERR)	RIC0
203	IF(IERR.EQ.0) GO TO 1150	RIC0
204	CALL LNCNT(3)	RIC0
205	PRINT 225	RIC0
206	RETURN	RIC0
207 C		RIC0
208 1150	CONTINUE	RIC0
209	IF( I.EQ. 1) GO TO 925	RIC0
210	CALL MAXEL(DUMMY,NA,ANORM1)	RIC0
211	CALL SUBT(P,NP,DUMMY,NA,DUMMY(N1),NA)	RIC0
212	CALL MAXEL(DUMMY(N1),NA,ANORM2)	RIC0
213	IF( ANORM1.GT. 1.) GO TO 1200	RIC0
214	IF( ANORM2/ANORM1.LT. RICTCV ) GO TO 1300	RIC0
215	GO TO 1250	RIC0
216 1200	CONTINUE	RIC0
217	IF( ANORM2.LT. RICTCV ) GO TO 1300	RIC0
218 C		RIC0
219 1250	CONTINUE	RIC0
220	IF( I.LE. 101) GO TO 925	RIC0
221	CALL LNCNT(3)	RIC0
222	PRINT 775	RIC0
223	IOP(1) = 1	RIC0
224 C		RIC0
225 1300	CONTINUE	RIC0
226	IF(IOP(1).EQ.0) RETURN	RIC0
227	CALL LNCNT(4)	RIC0
228	PRINT 1350,I	RIC0
229 1350	FORMAT(//,' FINAL VALUES OF P AND F AFTER',IS,' ITERATIONS TO CONVR	RIC0
230	ERGE',/)	RIC0
231	CALL PRNT(P,NP,4H P ,1)	RIC0
232	CALL PRNT(F,NF,4H F ,1)	RIC0
233 C		RIC0
234	RETURN	RIC0
235	END	RIC0

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0 SUBROUTINE ASMREG(A,NA,B,NB,H,NH,G,NQ,R,NP,F,NF,P,NP,IDENT,DISC,N ASM0
1 NEWT,STABLE,FNULL,ALPHA,IOP,DUMMY) ASM0
2 IMPLICIT REAL*8 (A-H,O-Z) ASM0
3 DIMENSION A(1),B(1),H(1),G(1),R(1),F(1),P(1),DUMMY(1) ASM0
4 DIMENSION NA(2),NB(2),NH(2),NQ(2),NR(2),NF(2),NP(2),IOP(5),IOPT(3) ASM0
5 1,NDUM1(2),NDUM2(2),NDUM3(2) ASM0
6 LOGICAL IDENT,DISC,NEWT,STABLE,FNULL,SING ASM0
7 N = NA(1)**2 ASM0
8 N1 = N+1 ASM0
9 IOPTT=0 ASM0
10 IF ( .NOT. NEWT ) GO TO 600 ASM0
11 IF( STABLE ) GO TO 500 ASM0
12 IF ( FNULL ) GO TO 100 ASM0
13 CALL MULT(B,NB,F,NF,DUMMY,NA) ASM0
14 CALL SUBT(A,NA,DUMMY,NA,DUMMY,NA) ASM0
15 CALL TESTSA(DUMMY,NA,ALPHA,DISC,STABLE,IOPTT,DUMMY(N1)) ASM0
16 GO TO 200 ASM0
17 100 CONTINUE ASM0
18 CALL TESTSA(A,NA,ALPHA,DISC,STABLE,IOPTT,DUMMY) ASM0
19 C ASM0
20 200 CONTINUE ASM0
21 IF( STABLE ) GO TO 500 ASM0
22 IF( DISC ) GO TO 230 ASM0
23 J = -NA(1) ASM0
24 NAX = NA(1) ASM0
25 DO 210 I =1,NAX ASM0
26 J = J + NAX +1 ASM0
27 A(J) = A(J)-ALPHA ASM0
28 210 CONTINUE ASM0
29 SCLE = 3. ASM0
30 IOPT(1)=IOP(1) ASM0
31 IOPT(2) = 1 ASM0
32 IOPT(3)=1 ASM0
33 CALL CSTAB(A,NA,B,NB,F,NF,IOPT,SCLE,DUMMY) ASM0
34 J = -NA(1) ASM0
35 DO 220 I=1,NAX ASM0
36 J = J + NAX + 1 ASM0
37 A(J) = A(J) + ALPHA ASM0
38 220 CONTINUE ASM0
39 225 CONTINUE ASM0
40 CALL MULT(B,NB,F,NF,DUMMY,NA) ASM0
41 CALL SUBT(A,NA,DUMMY,NA,DUMMY,NA) ASM0
42 CALL TESTSA(DUMMY,NA,ALPHA,DISC,STABLE,IOPTT,DUMMY(N1)) ASM0
43 GO TO 300 ASM0
44 C ASM0
45 230 CONTINUE ASM0
46 J = 2*NA(1) + 1 ASM0
47 IF( .NOT. FNULL ) J = J + N ASM0
48 SING = .FALSE. ASM0
49 IF( DUMMY(J) .EQ. 0.0 ) SING = .TRUE. ASM0
50 IOPT(1) = IOP(1) ASM0
51 IOPT(2) = 1 ASM0
52 DSCLE = 0.5 ASM0
53 ALPHAT = 1./ALPHA ASM0
54 CALL SCALE(A,NA,A,NA,ALPHAT) ASM0
55 CALL SCALE(B,NB,B,NR,ALPHAT) ASM0
56 CALL DSTAB(A,NA,B,NB,F,NF,SING,IOPT,DSCLE,DUMMY) ASM0
57 CALL SCALE(A,NA,A,NA,ALPHA) ASM0
58 CALL SCALE(B,NB,B,NB,ALPHA) ASM0
59 GO TO 225 ASM0
60 C ASM0
61 300 CONTINUE ASM0
62 IF( STABLE ) GO TO 400 ASM0

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63	CALL LNCNT(5)	ASM00
64	IF( DISC ) GO TO 330	ASM00
65	PRINT 310,ALPHA	ASM00
66	310 FORMAT(// ' IN ASMREG, CSTAB HAS FAILED TO FIND A STABILIZING GAIN	ASM00
67	1 MATRIX (F) RELATIVE TO ',/, ' ALPHA = ',016.8/)	ASM00
68	RETURN	ASM00
69	330 CONTINUE	ASM00
70	PRINT 340,ALPHA	ASM00
71	340 FORMAT(// ' IN ASMREG, DSTAB HAS FAILED TO FIND A STABILIZING GAIN	ASM00
72	1 MATRIX (F) RELATIVE TO ',/, ' ALPHA = ',016.8/)	ASM00
73	RETURN	ASM00
74	C	ASM00
75	400 CONTINUE	ASM00
76	FNULL = .FALSE.	ASM00
77	C	ASM00
78	500 CONTINUE	ASM00
79	CALL RICNWT(A,NA,B,NB,H,NH,Q,NQ,R,NR,F,NF,P,NP,IOP,IDENT,DISC,FNU	ASM00
80	ILL,DUMMY)	ASM00
81	GO TO 750	ASM00
82	C	ASM00
83	600 CONTINUE	ASM00
84	IF( DISC ) GO TO 700	ASM00
85	NW = 4*N + 1	ASM00
86	NLAM = NW + 4*N	ASM00
87	NDUM = NLAM + N	ASM00
88	IOP(3) = 1	ASM00
89	CALL CNTREG(A,NA,B,NB,H,NH,Q,NQ,R,NR,DUMMY,DUMMY(NW),DUMMY(NLAM),	ASM00
90	IS,F,NF,P,NP,I,IOP,IDENT,DUMMY(NDUM))	ASM00
91	GO TO 750	ASM00
92	700 CONTINUE	ASM00
93	CALL DISREG(A,NA,B,NB,H,NH,Q,NQ,R,NR,F,NF,P,NP,IOP,IDENT,DUMMY)	ASM00
94	C	ASM00
95	750 CONTINUE	ASM00
96	C	ASM00
97	IF( IOP(4) .EQ. 0 ) GO TO 1100	ASM00
98	C	ASM00
99	N2= N1 + N	ASM01
100	N3= N2 + N	ASM01
101	C	ASM01
102	IF( DISC ) GO TO 800	ASM01
103	CALL MULT(P,NP,B,NB,DUMMY,NB)	ASM01
104	CALL MULT(DUMMY,NB,F,NF,DUMMY(N1),NP)	ASM01
105	CALL TRANSP(DUMMY(N1),NP,DUMMY,NP)	ASM01
106	CALL ADD(DUMMY,NP,DUMMY(N1),NP,DUMMY,NP)	ASM01
107	CALL SCALE(DUMMY,NP,DUMMY,NP,0.5)	ASM01
108	CALL SUBT(Q,NQ,DUMMY,NP,DUMMY,NP)	ASM01
109	CALL MULT(P,NP,A,NA,DUMMY(N1),NP)	ASM01
110	CALL ADD(DUMMY,NP,DUMMY(N1),NP,DUMMY,NP)	ASM01
111	CALL TRANSP(DUMMY(N1),NP,DUMMY(N2),NP)	ASM01
112	CALL ADD(DUMMY,NP,DUMMY(N2),NP,DUMMY,NP)	ASM01
113	GO TO 900	ASM01
114	C	ASM01
115	800 CONTINUE	ASM01
116	CALL MULT(R,NR,F,NF,DUMMY,NF)	ASM01
117	CALL TRANSP(F,NF,DUMMY(N1),NB)	ASM01
118	CALL MULT(DUMMY(N1),NB,DUMMY,NF,DUMMY(N2),NA)	ASM01
119	CALL ADD(DUMMY(N2),NA,Q,NQ,DUMMY,NA)	ASM01
120	CALL MULT(B,NB,F,NF,DUMMY(N1),NA)	ASM01
121	CALL SUBT(A,NA,DUMMY(N1),NA,DUMMY(N1),NA)	ASM01
122	CALL MULT(P,NP,DUMMY(N1),NA,DUMMY(N2),NA)	ASM01
123	CALL TRANSP(DUMMY(N1),NA,DUMMY(N3),NA)	ASM01
124	CALL MULT(DUMMY(N3),NA,DUMMY(N2),NA,DUMMY(N1),NA)	ASM01
125	CALL ADD(DUMMY,NA,DUMMY(N1),NA,DUMMY,NA)	ASM01

26	CALL SUBT(P, NP, DUMMY, NA, DUMMY, NA)	ASM01
27 C		ASM01
128	900 CONTINUE	ASM01
29	CALL LNCNT(4)	ASM01
30	PRINT 1000	ASM01
131	1000 FORMAT(// ' RESIDUAL ERROR IN RICCATI EQUATION ' /)	ASM01
132	CALL PRNT(DUMMY, NP, 4HEROR, 1)	ASM01
133 C		ASM01
134	1100 CONTINUE	ASM01
135	N2 = N1 + NA(1)	ASM01
136	N3 = N2 + NA(1)	ASM01
137	ISV = 0	ASM01
138	CALL EQUATE(P, NP, DUMMY, NP)	ASM01
139	CALL EIGEN(NA(1), NA(1), DUMMY, DUMMY(N1), DUMMY(N2), ISV, ISV, V, DUMMY(N	ASM01
140	13), IERR)	ASM01
141	NEVL = NA(1)	ASM01
142	IF( IERR .EQ. 0 ) GO TO 1300	ASM01
143	NEVL = NA(1) - IERR	ASM01
144	CALL LNCNT(4)	ASM01
145	PRINT 1200, IERR	ASM01
146	1200 FORMAT(// ' IN ASMREG, THE ', IS, ' EIGENVALUE OF P HAS NOT BEEN CO	ASM01
147	1PUTED AFTER 30 ITERATIONS ' /)	ASM01
148 C		ASM01
149	1300 CONTINUE	ASM01
150	NDUM1(1) = NEVL	ASM01
151	NDUM1(2) = 1	ASM01
152	CALL EQUATE(DUMMY(N1), NDUM1, DUMMY, NDUM1)	ASM01
153	N1 = NDUM1(1) + 1	ASM01
154	CALL MULT(B, NB, F, NF, DUMMY(N1), NA)	ASM01
155	CALL SUBT(A, NA, DUMMY(N1), NA, DUMMY(N1), NA)	ASM01
156	N2 = N1 + N	ASM01
157	CALL EQUATE(DUMMY(N1), NA, DUMMY(N2), NA)	ASM01
158	N3 = N2 + N	ASM01
159	N4 = N3 + NA(1)	ASM01
160	N5 = N4 + NA(1)	ASM01
161	CALL EIGEN(NA(1), NA(1), DUMMY(N2), DUMMY(N3), DUMMY(N4), ISV, ISV, V, DUM	ASM01
162	1MY(N5), IERR)	ASM01
163	NEVL = NA(1)	ASM01
164	IF( IERR .EQ. 0 ) GO TO 1500	ASM01
165	NEVL = NA(1) - IERR	ASM01
166	CALL LNCNT(4)	ASM01
167	PRINT 1400, IERR	ASM01
168	1400 FORMAT(// ' IN ASMREG, THE ', IS, ' EIGENVALUE OF A-BF HAS NOT BEEN C	ASM01
169	1OMPUTED AFTER 30 ITERATIONS ' /)	ASM01
170 C		ASM01
171	1500 CONTINUE	ASM01
172	NDUM2(1) = NEVL	ASM01
173	NDUM2(2) = 1	ASM01
174	CALL JUXTC(DUMMY(N3), NDUM2, DUMMY(N4), NDUM2, DUMMY(N2), NDUM3)	ASM01
175 C		ASM01
176	IF ( IOP(5) .EQ. 0 ) RETURN	ASM01
177 C		ASM01
178	CALL LNCNT(4)	ASM01
179	PRINT 1600	ASM01
180	1600 FORMAT(// ' EIGENVALUES OF P ' /)	ASM01
181	CALL PRNT(DUMMY, NDUM1, 4HEVLP, 1)	ASM01
182	CALL LNCNT(4)	ASM01
183	PRINT 1700	ASM01
184	1700 FORMAT(// ' CLOSED-LOOP RESPONSE MATRIX A-BF ' /)	ASM01
185	CALL PRNT(DUMMY(N1), NA, 4HA-BF, 1)	ASM01
186	CALL LNCNT(3)	ASM01
187	PRINT 1800	ASM01
188	1800 FORMAT(// ' EIGENVALUES OF A-BF ' /)	ASM01

189 CALL PRNT('DUMMY(N2),NDUM3,0,3)

190 C

191 RETURN

192 END

ASMO

ASMO

ASMO

ASMO

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0 SUBROUTINE ASMFIL(A,NA,G,NG,H,NH,Q,NQ,R,NR,F,NF,P,NP,IDENT,DISC,N AS
1 NEWT,STABLE,FNULL,ALPHA,IOP,DUMMY) AS
2 IMPLICIT REAL*8 (A-H,O-Z) AS
3 DIMENSION A(1),G(1),H(1),Q(1),R(1),F(1),P(1),DUMMY(1) AS
4 DIMENSION NA(2),NG(2),NH(2),NQ(2),NR(2),NF(2),NP(2),IOPT(5),NDUM1(AS
5 12),IOP(1) AS
6 LOGICAL IDENT,DISC,NEWT,STABLE,FNULL AS
7 IF( IOP(1) .EQ. 0 ) GO TO 100 AS
8 CALL LNCNT(4) AS
9 IF(DISC) PRINT 15 AS
10 IF( .NOT. DISC ) PRINT 25 AS
11 15 FORMAT(/,,' PROGRAM TO SOLVE THE DISCRETE INFINITE-DURATION OPTIMAAS
12 IL FILTER PROBLEM',/) AS
13 25 FORMAT(/,,' PROGRAM TO SOLVE THE CONTINUOUS INFINITE-DURATION OPTIAAS
14 MAL FILTER PROBLEM',/) AS
15 CALL PRNT(A,NA,4H A ,1) AS
16 IF( .NOT. IDENT ) GO TO 35 AS
17 CALL LNCNT(3) AS
18 PRINT 30 AS
19 30 FORMAT(/,,' G IS AN IDENTITY MATRIX',/) AS
20 GO TO 40 AS
21 35 CONTINUE AS
22 CALL PRNT(G,NG,4H G ,1) AS
23 40 CONTINUE AS
24 CALL PRNT(H,NH,4H H ,1) AS
25 CALL LNCNT(3) AS
26 PRINT 45 AS
27 45 FORMAT(/,,' INTENSITY MATRIX FOR COVARIANCE OF MEASUREMENT NOISE',/) AS
28 CALL PRNT(R,NR,4H R ,1) AS
29 C AS
30 IF( .NOT. IDENT ) GO TO 65 AS
31 CALL LNCNT(3) AS
32 PRINT 55 AS
33 55 FORMAT(/,,' INTENSITY MATRIX FOR COVARIANCE OF PROCESS NOISE',/) AS
34 C AS
35 65 CONTINUE AS
36 CALL PRNT(Q,NQ,4H Q ,1) AS
37 C AS
38 100 CONTINUE AS
39 IOPT(1)=IOP(2) AS
40 IOPT(2)=IOP(3) AS
41 IOPT(3)=IOP(4) AS
42 IOPT(4)=IOP(5) AS
43 IOPT(5)=0 AS
44 K = 0 AS
45 C AS
46 200 CONTINUE AS
47 CALL TRANP(A,NA,DUMMY,NA) AS
48 CALL EQUATE(DUMMY,NA,A,NA) AS
49 CALL TRANP(H,NH,DUMMY,NDUM1) AS
50 CALL EQUATE(DUMMY,NDUM1,H,NH) AS
51 IF( IDENT ) GO TO 250 AS
52 CALL TRANP(G,NG,DUMMY,NDUM1) AS
53 CALL EQUATE(DUMMY,NDUM1,G,NG) AS
54 250 CONTINUE AS
55 IF ( K .EQ. 1 ) RETURN AS
56 C AS
57 K = K+1 AS
58 CALL ASMREG(A,NA,H,NH,G,NG,Q,NQ,R,NR,F,NF,P,NP,IDENT,DISC,NEWT,ST AS
59 ABLE,FNULL,ALPHA,IOPT,DUMMY) AS
60 C AS
61 N1=(NA(1)*2)+3*NA(1)+1 AS
62 CALL TRANP(F,NF,DUMMY(N1),NDUM1) AS

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63		CALL EQUATE(DUMMY(N1),NDUM1,F,NF)	ASMO
64	C		ASMO
65		IF( IOP(1) .EQ. 0 ) GO TO 200	ASMO
66	C		ASMO
67		IF(IDENT) GO TO 300	ASMO
68		CALL LNCNT(3)	ASMO
69		PRINT 55	ASMO
70		CALL PRNT(Q,NQ,4HGGT,1)	ASMO
71	C		ASMO
72	300	CONTINUE	ASMO
73		CALL LNCNT(3)	ASMO
74		PRINT 325	ASMO
75	325	FORMAT(/, ' FILTER GAIN',/)	ASMO
76		CALL PRNT(F,NF,4H F ,1)	ASMO
77		CALL LNCNT(3)	ASMO
78		PRINT 350	ASMO
79	350	FORMAT(/, 'STEADY-STATE VARIANCE MATRIX OF RECONSTRUCTION ERROR',/)	ASMO
80		CALL PRNT(P,NP,4H P ,1)	ASMO
81		NDUM1(1)=NP(1)	ASMO
82		NDUM1(2)=1	ASMO
83		CALL LNCNT(3)	ASMO
84		PRINT 375	ASMO
85	375	FORMAT(/, ' EIGENVALUES OF P ',/)	ASMO
86		CALL PRNT(DUMMY,NDUM1,4HEVLP,1)	ASMO
87		N1 = NP(1) + 1	ASMO
88		N = NA(1)**2	ASMO
89		N2 = N1 + N + 2*NA(1)	ASMO
90		CALL TRANSP(DUMMY(N1),NA,DUMMY(N2),NA)	ASMO
91		CALL PRNT(DUMMY(N2),NA,4HA-FH,1)	ASMO
92		N2 = N1 + N	ASMO
93		CALL LNCNT(3)	ASMO
94		PRINT 385	ASMO
95	385	FORMAT(/, ' EIGENVALUES OF A-FH MATRIX',/)	ASMO
96		NDUM1(1) = NA(1)	ASMO
97		NDUM1(2) = 2	ASMO
98		CALL PRNT(DUMMY(N2),NDUM1,0,3)	ASMO
99	C		ASMO
100		GO TO 200	ASMO
101	C		ASMO
102		END	ASMO

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0 SUBROUTINE EXPMOD (A,NA,B,NB,H,NH,AM,NAM,HM,NHM,Q,NQ,R,NR,F,NF,P, EXP0
1 INP,HIDENT,HMDENT,DISC,NEWT,STABLE,FNULL,ALPHA,IOP,DUMMY) EXP0
2 IMPLICIT REAL*8 (A-H,O-Z) EXP0
3 DIMENSION A(1),B(1),H(1),AM(1),HM(1),Q(1),R(1),F(1),P(1),DUMMY(1) EXP0
4 DIMENSION NA(2),NB(2),NH(2),NAM(2),NHM(2),NQ(2),NR(2),NF(2),NP(2),EXP0
5 IOP(1),IOPT(5),NDUM1(2),NDUM2(2),NDUM3(2) EXP0
6 LOGICAL HIDENT,HMDENT,DISC,NEWT,STABLE,FNULL,SYM EXP0
7 COMMON/TOL/EPSSAM,EPSSBM,IACM EXP0
8 IF( IOP(1) .EQ. 0 ) GO TO 300 EXP0
9 CALL LNCNT(6) EXP0
10 IF( DISC ) PRINT 25 EXP0
11 IF( .NOT. DISC ) PRINT 50 EXP0
12 25 FORMAT(/,' PROGRAM TO SOLVE ASYMPTOTIC DISCRETE EXPLICIT MODEL-FOLEXP0
13 FOLLOWING PROBLEM',//,' PLANT DYNAMICS',/) EXP0
14 50 FORMAT(/,' PROGRAM TO SOLVE ASYMPTOTIC CONTINUOUS EXPLICIT MODEL-FEXP0
15 FOLLOWING PROBLEM',//,' PLANT DYNAMICS',/) EXP0
16 CALL PRNT(A,NA,4H A ,1) EXP0
17 CALL PRNT(B,NB,4H B ,1) EXP0
18 IF( HIDENT ) GO TO 75 EXP0
19 CALL PRNT(H,NH,4H H ,1) EXP0
20 GO TO 100 EXP0
21 75 CONTINUE EXP0
22 CALL LNCNT(3) EXP0
23 PRINT 85 EXP0
24 85 FORMAT(/,' H IS AN IDENTITY MATRIX',/) EXP0
25 C EXP0
26 100 CONTINUE EXP0
27 CALL LNCNT(4) EXP0
28 PRINT 125 EXP0
29 125 FORMAT(/,' MODEL DYNAMICS',/) EXP0
30 CALL PRNT(AM,NAM,4H AM ,1) EXP0
31 IF( HMDENT ) GO TO 175 EXP0
32 CALL PRNT(HM,NHM,4H HM ,1) EXP0
33 GO TO 200 EXP0
34 175 CONTINUE EXP0
35 CALL LNCNT(3) EXP0
36 PRINT 185 EXP0
37 185 FORMAT(/,' HM IS AN IDENTITY MATRIX ',/) EXP0
38 C EXP0
39 200 CONTINUE EXP0
40 CALL LNCNT(4) EXP0
41 PRINT 225 EXP0
42 225 FORMAT(/,' WEIGHTING MATRICES ',/) EXP0
43 CALL PRNT(Q,NQ,4H Q ,1) EXP0
44 CALL PRNT(R,NR,4H R ,1) EXP0
45 C EXP0
46 300 CONTINUE EXP0
47 IF( IOP(2) .EQ. 0 ) GO TO 400 EXP0
48 NF(1) = NB(2) EXP0
49 NF(2) = NA(1) EXP0
50 NP(1) = NA(1) EXP0
51 NP(2) = NA(1) EXP0
52 IOPT(1) = IOP(3) EXP0
53 IOPT(2) = IOP(4) EXP0
54 IOPT(3) = IOP(5) EXP0
55 IOPT(4) = 0 EXP0
56 IOPT(5) = 0 EXP0
57 N1 = NA(1)*NA(2) + 1 EXP0
58 CALL EQUATE(Q,NQ,DUMMY,NQ) EXP0
59 CALL ASMREG(A,NA,B,NB,H,NH,DUMMY,NQ,R,NR,F,NF,P,NP,HIDENT,DISC,NE EXP0
60 WT,STABLE,FNULL,ALPHA,IOPT,DUMMY(N1)) EXP0
61 C EXP0
62 400 CONTINUE EXP0

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63	IF( IOP(1) .EQ. 0 ) GO TO 600	EXP00
64	CALL LNCNT(4)	EXP00
65	PRINT 425	EXP00
66	425 FORMAT(/, ' CONTROL LAW U = -F( COL.(X,XM) ), F = (F11,F12)',/)	EXP00
67	CALL LNCNT(3)	EXP00
68	PRINT 450	EXP00
69	450 FORMAT(/, ' PART OF F MULTIPLYING X ',/)	EXP00
70	CALL PRNT(F,NF,4H F11,1)	EXP00
71	IF( .NOT. DISC .AND. IOP(2) .EQ. 0 ) GO TO 600	EXP00
72	CALL PRNT(P,NP,4H P11,1)	EXP00
73	IF( IOP(2) .EQ. 0 ) GO TO 600	EXP00
74	CALL LNCNT(2)	EXP00
75	PRINT 475	EXP00
76	475 FORMAT(/, ' EIGENVALUES OF P11')	EXP00
77	NDUM1(1) = NA(1)	EXP00
78	NDUM1(2) = 1	EXP00
79	CALL PRNT(DUMMY(N1),NDUM1,0,3)	EXP00
80	N1 = N1 + NDUM1(1)	EXP00
81	NDUM1(2) = NA(1)	EXP00
82	CALL LNCNT(2)	EXP00
83	PRINT 500	EXP00
84	500 FORMAT(/, ' PLANT CLOSED-LOOP RESPONSE MATRIX A = BF11')	EXP00
85	CALL PRNT(DUMMY(N1),NDUM1,0,3)	EXP00
86	CALL LNCNT(2)	EXP00
87	PRINT 525	EXP00
88	525 FORMAT(/, ' EIGENVALUES OF CLOSED-LOOP RESPONSE MATRIX')	EXP00
89	N1 = N1 + NDUM1(1)*NDUM1(2)	EXP00
90	NDUM1(2) = 2	EXP00
91	CALL PRNT(DUMMY(N1),NDUM1,0,3)	EXP00
92	C	EXP00
93	600 CONTINUE	EXP00
94	NF(1) = NB(2)	EXP00
95	NF(2) = NA(1)	EXP00
96	CALL MULT(B,NB,F,NF,DUMMY,NA)	EXP00
97	CALL SUBT(A,NA,DUMMY,NA,DUMMY,NA)	EXP00
98	IF( IOP(1).EQ. 0 .OR. IOP(2) .NE. 0 ) GO TO 700	EXP00
99	CALL LNCNT(2)	EXP00
100	PRINT 500	EXP00
101	CALL PRNT(DUMMY,NA,0,3)	EXP00
102	C	EXP00
103	700 CONTINUE	EXP00
104	N1 = NA(1)**2 + 1	EXP00
105	CALL TRANP(DUMMY,NA,DUMMY(N1),NA)	EXP00
106	CALL EQUATE(DUMMY(N1),NA,DUMMY,NA)	EXP00
107	NF(2) = NA(1) + NAM(1)	EXP00
108	NP(2) = NF(2)	EXP00
109	IF( .NOT. DISC .AND. IOP(2).EQ. 0 ) NP(2) = NAM(2)	EXP00
110	IOPTT=0	EXP00
111	SYM = .FALSE.	EXP00
112	CALL EQUATE( Q,NQ,DUMMY(N1),NDUM2)	EXP00
113	IF( HMDENT ) GO TO 725	EXP00
114	CALL MULT(Q,NQ,HM,NHM,DUMMY(N1),NDUM2)	EXP00
115	725 CONTINUE	EXP00
116	IF( HIDENT ) GO TO 750	EXP00
117	N2 = N1 + NQ(1)*NHM(2)	EXP00
118	CALL TRANP(H,NH,DUMMY(N2),NDUM1)	EXP00
119	N3 = N2 + NH(1)*NH(2)	EXP00
120	CALL MULT(DUMMY(N2),NDUM1,DUMMY(N1),NHM,DUMMY(N3),NDUM2)	EXP00
121	CALL EQUATE(DUMMY(N3),NDUM2,DUMMY(N1),NDUM2)	EXP00
122	750 CONTINUE	EXP00
123	N2 = NA(1)**2 + NA(1)*NHM(2) + 1	EXP00
124	N3 = NA(1)**2 + 1	EXP00
125	IF( .NOT. DISC .AND. IOP(2) .EQ. 0 ) N3 = 1	EXP00

126	CALL EQUATE(DUMMY(N1),NDUM2,P(N3),NDUM2)	EXP0
127	IF( DISC ) GO TO 800	EXP0
128	EPSA = EPSAM	EXP0
129	CALL HARSTW(DUMMY,NA,AM,NAM,P(N3),NDUM2,IOPTT,SYM ,EPSA,EPSA,DUMMY	EXP0
130	1(N2))	EXP0
131	GO TO 900	EXP0
132	C	EXP0
133	800 CONTINUE	EXP0
134	CALL SCALE(P(N3),NDUM2,P(N3),NDUM2,-1.0)	EXP0
135	N4 = N2 + NAM(1)**2	EXP0
136	CALL EQUATE(AM,NAM,DUMMY(N2),NAM)	EXP0
137	CALL SUM(DUMMY,NA,P(N3),NDUM2,DUMMY(N2),NAM,IOPTT,SYM,DUMMY(N4))	EXP0
138	C	EXP0
139	900 CONTINUE	EXP0
140	N2 = NB(2)*NA(1) + 1	EXP0
141	CALL TRANSP(B,NB,DUMMY,NDUM1)	EXP0
142	CALL MULT(DUMMY,NDUM1,P(N3),NDUM2,F(N2),NDUM3)	EXP0
143	IF( .NOT. DISC ) GO TO 1000	EXP0
144	N1 = NB(1)*NB(2) + 1	EXP0
145	CALL MULT(DUMMY,NDUM1,P,NA,DUMMY(N1),NDUM2)	EXP0
146	CALL MULT(DUMMY(N1),NDUM2,B,NB,DUMMY,NR)	EXP0
147	CALL ADD(R,NR,DUMMY,NR,DUMMY,NR)	EXP0
148	GO TO 1100	EXP0
149	C	EXP0
150	1000 CONTINUE	EXP0
151	CALL EQUATE(R,NR,DUMMY,NR)	EXP0
152	C	EXP0
153	1100 CONTINUE	EXP0
154	N1 = NR(1)**2 + 1	EXP0
155	CALL SYMPOS(NR(1),NR(1),DUMMY,NHM(2),F(N2),IOPTT,IOPTT,DETERM,ISCA	EXP0
156	1LE,DUMMY(N1),IERR)	EXP0
157	IF( IERR .EQ. 0 ) GO TO 1200	EXP0
158	CALL LNCNT(3)	EXP0
159	PRINT 1150	EXP0
160	1150 FORMAT(/,' IN EXPMDF, THE COEFFICIENT MATRIX FOR SYMPOS IS NOT SY	EXP0
161	MMETRIC POSITIVE DEFINITE ',/)	EXP0
162	RETURN	EXP0
163	C	EXP0
164	1200 CONTINUE	EXP0
165	IF( .NOT. DISC ) GO TO 1300	EXP0
166	CALL MULT(F(N2),NDUM3,AM,NAM,DUMMY,NDUM1)	EXP0
167	CALL EQUATE(DUMMY,NDUM1,F(N2),NDUM1)	EXP0
168	1300 CONTINUE	EXP0
169	IF( IOP(1) .EQ. 0 ) RETURN	EXP0
170	CALL LNCNT(3)	EXP0
171	PRINT 1325	EXP0
172	1325 FORMAT(/,' PART OF F MULTIPLYING XM ',/)	EXP0
173	CALL PRNT(F(N2),NDUM3,4H F12,1)	EXP0
174	NDUM1(1) = NA(1)	EXP0
175	NDUM1(2) = NAM(1)	EXP0
176	CALL PRNT(P(N3),NDUM1,4H P12,1)	EXP0
177	RETURN	EXP0
178	END	EXP0

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0      SUBROUTINE IMPMOD(A,NA,B,NB,H,NH,AM,NAM,BM,NBM,Q,NQ,R,NR,F,NF,P,N IMP0
1      IP,IDENT,DISC,NEWT,STABLE,FNULL,ALPHA,IOP,DUMMY) IMP0
2      IMPLICIT REAL*8 (A-H,O-Z) IMP0
3      DIMENSION A(1),B(1),H(1),AM(1),BM(1),Q(1),R(1),F(1),P(1),DUMMY(1) IMP0
4      DIMENSION NA(2),NB(2),NH(2),NAM(2),NBM(2),NQ(2),NR(2),NF(2),NP(2), IMP0
5      IOP(1),IOP(5),NDUM1(2) IMP0
6      LOGICAL IDENT,DISC,NEWT,STABLE,FNULL,HIDENT IMP0
7      IF( IOP(1) .EQ. 0 ) GO TO 200 IMP0
8      CALL LNCNT(6) IMP0
9      IF( DISC ) PRINT 25 IMP0
10     IF( .NOT. DISC ) PRINT 50 IMP0
11     25 FORMAT(/,'PROGRAM TO SOLVE ASYMPTOTIC DISCRETE IMPLICIT MODEL-FOLLOWING IMP0
12     100 PROBLEM',//,' PLANT DYNAMICS ',//) IMP0
13     50 FORMAT(/,'PROGRAM TO SOLVE ASYMPTOTIC CONTINUOUS IMPLICIT MODEL-FOLLOWING IMP0
14     100 PROBLEM',//,' PLANT DYNAMICS ',//) IMP0
15     CALL PRNT(A,NA,4H A ,1) IMP0
16     CALL PRNT(B,NB,4H B ,1) IMP0
17     IF( IDENT ) GO TO 75 IMP0
18     CALL PRNT(H,NH,4H H ,1) IMP0
19     GO TO 100 IMP0
20     75 CONTINUE IMP0
21     CALL LNCNT(3) IMP0
22     PRINT 55 IMP0
23     85 FORMAT(/,' H IS AN IDENTITY MATRIX',//) IMP0
24 C IMP0
25     100 CONTINUE IMP0
26     CALL LNCNT(4) IMP0
27     PRINT 125 IMP0
28     125 FORMAT(/,' MODEL DYNAMICS ',//) IMP0
29     CALL PRNT(AM,NAM,4H AM ,1) IMP0
30     CALL PRNT(BM,NBM,4H BM ,1) IMP0
31     CALL LNCNT(4) IMP0
32     PRINT 150 IMP0
33     150 FORMAT(/,' WEIGHTING MATRICES ',//) IMP0
34     CALL PRNT(Q,NQ,4H Q ,1) IMP0
35     CALL PRNT(R,NR,4H R ,1) IMP0
36 C IMP0
37     200 CONTINUE IMP0
38     N = NA(1)**2 IMP0
39     N1 = N + 1 IMP0
40     IF( .NOT. IDENT ) GO TO 300 IMP0
41     CALL SUBT(A,NA,AM,NAM,DUMMY,NA) IMP0
42     CALL SUBT(B,NB,BM,NBM,DUMMY(N1),NB) IMP0
43     GO TO 400 IMP0
44 C IMP0
45     300 CONTINUE IMP0
46     CALL MULT(H,NH,A,NA,DUMMY,NH) IMP0
47     CALL MULT(AM,NAM,H,NH,DUMMY(N1),NH) IMP0
48     CALL SUBT(DUMMY,NH,DUMMY(N1),NH,DUMMY,NH) IMP0
49     CALL MULT(H,NH,B,NB,DUMMY(N1),NBM) IMP0
50     CALL SUBT(DUMMY(N1),NBM,BM,NBM,DUMMY(N1),NBM) IMP0
51 C IMP0
52     400 CONTINUE IMP0
53     IF( IOP(1) .EQ. 0 ) GO TO 500 IMP0
54     CALL LNCNT(3) IMP0
55     PRINT 450 IMP0
56     450 FORMAT(/,' MATRIX HA = AMH' ) IMP0
57     CALL PRNT(DUMMY,NH,0,3) IMP0
58     CALL LNCNT(3) IMP0
59     PRINT 475 IMP0
60     475 FORMAT(/,' MATRIX HB = BM' ) IMP0
61     CALL PRNT(DUMMY(N1),NBM,0,3) IMP0
62 C IMP0

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63	500	CONTINUE	IMP
64		N2 = N1 + N	IMP
65		N3 = N2 + N	IMP
66		N4 = N3 + N	IMP
67		CALL MULT(Q,NQ,DUMMY,NH,DUMMY(N2),NH)	IMP
68		CALL MULT(Q,NQ,DUMMY(N1),NBM,DUMMY(N3),NBM)	IMP
69		CALL TRANP(DUMMY,NH,DUMMY(N4),NDUM1)	IMP
70		CALL MULT(DUMMY(N4),NDUM1,DUMMY(N2),NH,DUMMY,NA)	IMP
71		CALL MULT(DUMMY(N4),NDUM1,DUMMY(N3),NBM,DUMMY(N2),NB)	IMP
72		CALL TRANP(DUMMY(N1),NBM,DUMMY(N4),NDUM1)	IMP
73		CALL SCALE(DUMMY(N2),NB,DUMMY(N1),NB,2.0)	IMP
74		CALL MULT(DUMMY(N4),NDUM1,DUMMY(N3),NBM,DUMMY(N2),NR)	IMP
75		CALL ADD(DUMMY(N2),NR,R,NR,DUMMY(N2),NR)	IMP
76		IF( IOP(1) .EQ. 0 ) GO TO 600	IMP
77		CALL LNCNT(3)	IMP
78		PRINT 525	IMP
79	525	FORMAT(//,' MATRIX (HA - AMH TRANSPOSE)Q( HA - AMH)')	IMP
80		CALL PRNT(DUMMY,NA,0,3)	IMP
81		CALL LNCNT(3)	IMP
82		PRINT 550	IMP
83	550	FORMAT(//,' MATRIX 2( HA - AMH TRANSPOSE)Q( HB - BM)')	IMP
84		CALL PRNT(DUMMY(N1),NB,0,3)	IMP
85		CALL LNCNT(3)	IMP
86		PRINT 575	IMP
87	575	FORMAT(//,' MATRIX ( HB - BM TRANSPOSE)Q( HB - BM ) + R')	IMP
88		CALL PRNT(DUMMY(N2),NR,0,3)	IMP
89	C		IMP
90	600	CONTINUE	IMP
91		IOPT(1)= 0	IMP
92		IOPT(2)= 1	IMP
93		IOPT(3)= 1	IMP
94		N5 = N4 + N	IMP
95		CALL EQUATE(A,NA,DUMMY(N3),NA)	IMP
96		CALL PREFIL(DUMMY(N3),NA,B,NB,DUMMY,NA,DUMMY(N1),NB,DUMMY(N2),NR,D	IMP
97		UMMY(N4),NF,IOPT,DUMMY(N5))	IMP
98		IF(IOP(1) .EQ. 0 ) GO TO 700	IMP
99		CALL LNCNT(3)	IMP
100		PRINT 625	IMP
101	625	FORMAT(//,' PREFILTER GAIN')	IMP
102		CALL PRNT(DUMMY(N4),NF,0,3)	IMP
103		CALL LNCNT(3)	IMP
104		PRINT 650	IMP
105	650	FORMAT(//,' MATRIX A = B(PREFILTER)')	IMP
106		CALL PRNT(DUMMY(N3),NA,0,3)	IMP
107		CALL LNCNT(3)	IMP
108		PRINT 675	IMP
109	675	FORMAT(//,' MODIFIED STATE VECTOR WEIGHTING MATRIX')	IMP
110		CALL PRNT(DUMMY,NA,0,3)	IMP
111	C		IMP
112	700	CONTINUE	IMP
113		CALL EQUATE(DUMMY(N4),NF,DUMMY(N1),NF)	IMP
114	C		IMP
115		IF( IOP(2) .EQ. -1000 ) RETURN	IMP
116	C		IMP
117		IOPT(1) = IOP(2)	IMP
118		IOPT(2) = IOP(3)	IMP
119		IOPT(3) = IOP(4)	IMP
120		IOPT(4) = 0	IMP
121		IOPT(5) = 0	IMP
122		HIDENT = .TRUE.	IMP
123		CALL ASMREG(DUMMY(N3),NA,B,NB,H,NH,DUMMY,NA,DUMMY(N2),NR,F,NF,P,N	IMP
124		IP,HIDENT,DISC,NEAT,STABLE,FNULL,ALPHA,IOPT,DUMMY(N4))	IMP
125		IF( IOP(1) .EQ. 0 ) GO TO 800	IMP

126	CALL LNCNT(3)	IMP0
127	PRINT 725	IMP0
129	725 FORMAT(//, ' GAIN FROM ASMREG')	IMP0
129	CALL PRNT(F,NF,0,3)	IMP0
130	CALL LNCNT(3)	IMP0
131	PRINT 750	IMP0
132	750 FORMAT(//, ' SOLUTION OF ASSOCIATED STEADY-STATE RICCATI EQUATION')	IMP0
133	CALL PRNT(P,NP,0,3)	IMP0
134	CALL LNCNT(3)	IMP0
135	PRINT 775	IMP0
136	775 FORMAT(//, ' EIGENVALUES OF P')	IMP0
137	NDUM1(1) = NA(1)	IMP0
138	NDUM1(2) = 1	IMP0
139	CALL PRNT(DUMMY(N4),NDUM1,0,3)	IMP0
140	C	IMP0
141	800 CONTINUE	IMP0
142	CALL ADD(F,NF,DUMMY(N1),NF,F,NF)	IMP0
143	IF( IOP(1) .EQ. 0 ) RETURN	IMP0
144	CALL LNCNT(4)	IMP0
145	PRINT 825	IMP0
146	825 FORMAT(//, ' GAIN FOR MODEL-FOLLOWING CONTROL LAW, $U = -F X$ , $F =$	IMP0
147	$L(\text{PREFILTER}) + (\text{ASMREG})'$ ,//)	IMP0
148	CALL PRNT(F,NF,4H F ,1)	IMP0
149	N6 = N4 + NA(1)	IMP0
150	CALL PRNT(DUMMY(N6),NA,4H A-BF,1)	IMP0
151	NDUM1(2) = 2	IMP0
152	N6 = N6 + N	IMP0
153	CALL LNCNT(3)	IMP0
154	PRINT 850	IMP0
155	850 FORMAT(//, ' EIGENVALUES OF A-BF')	IMP0
156	CALL PRNT(DUMMY(N6),NDUM1,0,3)	IMP0
157	C	IMP0
158	RETURN	IMP0
159	END	IMP0

0	SUBROUTINE READ1 (A,NA,NZ,NAM)	REA
1	IMPLICIT REAL*8 (A-H,O-Z)	REA
2	DIMENSION A(1),NA(2),NZ(2)	REA
3	IF (NZ(1).EQ.0) GO TO 410	REA
4	NR=NZ(1)	REA
5	NC=NZ(2)	REA
6	NLST=NR*NC	REA
7	IF( NLST .LT. 1 .OR. NR .LT. 1 ) GO TO 16	REA
8	DO 400 I = 1, NR	REA
9	400 READ (5,101) (A( J), J = I,NLST,NR)	REA
10	NA(1)=NR	REA
11	NA(2)=NC	REA
12	410 CALL PRNT (A,NA,NAM,1)	REA
13	101 FORMAT(8D10.2)	REA
14	RETURN	REA
15	16 CALL LNCNT(1)	REA
16	WRITE (6,916) NAM,NR,NC	REA
17	916 FORMAT (' ERROR IN READ1 MATRIX ',A4,' HAS NA=',2I6)	REA
18	RETURN	REA
19	END	REA

0	SUBROUTINE BALANC(NM,N,A,LOW,IGH,SCALE)	BAL000
1	IMPLICIT REAL*8 (A-H,O-Z)	BAL000
2	INTEGER I,J,K,L,M,N,JJ,NM,IGH,LOW,IEXC	BAL000
3	DIMENSION A(NM,N),SCALE(N)	BAL000
4 C	REAL C,F,G,R,S,B2,RADIX	BAL000
5 C	REAL DABS	BAL000
6	LOGICAL NOCONV	BAL000
7 C		BAL000
8 C		BAL000
9 C	***** RADIX IS A MACHINE DEPENDENT PARAMETER SPECIFYING	BAL000
10 C	THE BASE OF THE MACHINE FLOATING POINT REPRESENTATION.	BAL000
11 C		BAL000
12 C		BAL000
13	RADIX = 16.	BAL000
14 C		BAL000
15	B2 = RADIX * RADIX	BAL000
16	K = 1	BAL000
17	L = N	BAL000
18	GO TO 100	BAL000
19 C	***** IN-LINE PROCEDURE FOR ROW AND	BAL000
20 C	COLUMN EXCHANGE *****	BAL000
21	20 SCALE(M) = J	BAL000
22	IF (J .EQ. M) GO TO 50	BAL000
23 C		BAL000
24	DO 30 I = 1, L	BAL000
25	F = A(I,J)	BAL000
26	A(I,J) = A(I,M)	BAL000
27	A(I,M) = F	BAL000
28	30 CONTINUE	BAL000
29 C		BAL000
30	DO 40 I = K, N	BAL000
31	F = A(J,I)	BAL000
32	A(J,I) = A(M,I)	BAL000
33	A(M,I) = F	BAL000
34	40 CONTINUE	BAL000
35 C		BAL000
36	50 GO TO (80,130), IEXC	BAL000
37 C	***** SEARCH FOR ROWS ISOLATING AN EIGENVALUE	BAL000
38 C	AND PUSH THEM DOWN *****	BAL000
39	80 IF (L .EQ. 1) GO TO 280	BAL000
40	L = L - 1	BAL000
41 C	***** FOR J=L STEP -1 UNTIL 1 DO -- *****	BAL000
42	100 DO 120 JJ = 1, L	BAL000
43	J = L + 1 - JJ	BAL000
44 C		BAL000
45	DO 110 I = 1, L	BAL000
46	IF (I .EQ. J) GO TO 110	BAL000
47	IF (A(J,I) .NE. 0.000) GO TO 120	BAL000
48	110 CONTINUE	BAL000
49 C		BAL000
50	M = L	BAL000
51	IEXC = 1	BAL000
52	GO TO 20	BAL000
53	120 CONTINUE	BAL000
54 C		BAL000
55	GO TO 140	BAL000
56 C	***** SEARCH FOR COLUMNS ISOLATING AN EIGENVALUE	BAL000
57 C	AND PUSH THEM LEFT *****	BAL000
58	130 K = K + 1	BAL000
59 C		BAL000
60	140 DO 170 J = K, L	BAL000
61 C		BAL000
62	DO 150 I = K, L	BAL000

63		IF (I .EQ. J) GO TO 150	BAL00
64		IF (A(I,J) .NE. 0.000) GO TO 170	BAL00
65	150	CONTINUE	BAL00
66	C		BAL00
67		M = K	BAL00
68		IEYC = 2	BAL00
69		GO TO 20	BAL00
70	170	CONTINUE	BAL00
71	C	***** NOW BALANCE THE SUBMATRIX IN ROWS K TO L *****	BAL00
72		DQ 180 I = K, L	BAL00
73	180	SCALE(I) = 1.000	BAL00
74	C	***** ITERATIVE LOOP FOR NORM REDUCTION *****	BAL00
75	190	NOCONV = .FALSE.	BAL00
76	C		BAL00
77		DO 270 I = K, L	BAL00
78		C = 0.000	BAL00
79		R = 0.000	BAL00
80	C		BAL00
81		DO 200 J = K, L	BAL00
82		IF (J .EQ. I) GO TO 200	BAL00
83		C = C + DABS(A(J,I))	BAL00
84		R = R + DABS(A(I,J))	BAL00
85	200	CONTINUE	BAL00
86	C	***** GUARD AGAINST ZERO C OR R DUE TO UNDERFLOW *****	BAL00
87		IF (C .EQ. 0.000 .OR. R .EQ. 0.000) GO TO 270	BAL00
88		G = R / RADIX	BAL00
89		F = 1.000	BAL00
90		S = C + R	BAL00
91	210	IF (C .GE. G) GO TO 220	BAL00
92		F = F * RADIX	BAL00
93		C = C * B2	BAL00
94		GO TO 210	BAL00
95	220	G = R * RADIX	BAL00
96	230	IF (C .LT. G) GO TO 240	BAL00
97		F = F / RADIX	BAL00
98		C = C / B2	BAL00
99		GO TO 230	BAL01
100	C	***** NOW BALANCE *****	BAL01
101	240	IF ((C + R) / F .GE. 0.95 * S) GO TO 270	BAL01
102		G = 1.000 / F	BAL01
103		SCALE(I) = SCALE(I) * F	BAL01
104		NOCONV = .TRUE.	BAL01
105	C		BAL01
106		DO 250 J = K, N	BAL01
107	250	A(I,J) = A(I,J) * G	BAL01
108	C		BAL01
109		DO 260 J = 1, L	BAL01
110	260	A(J,I) = A(J,I) * F	BAL01
111	C		BAL01
112	270	CONTINUE	BAL01
113	C		BAL01
114		IF (NOCONV) GO TO 190	BAL01
115	C		BAL01
116	280	LOW = K	BAL01
117		IGH = L	BAL01
118		RETURN	BAL01
119	C	***** LAST CARD OF BALANC *****	BAL01
120		END	BAL01

0	SUBROUTINE ELMHES(NM,N,LOW,IGH,A,INT)	ELM000
1	IMPLICIT REAL*8 (A-H,O-Z)	ELM000
2	INTEGER I,J,M,N,LA,NM,IGH,KP1,LOW,MM1,MP1	ELM000
3	DIMENSION A(NM,N)	ELM000
4 C	REAL X,Y	ELM000
5 C	REAL DABS	ELM000
6	INTEGER INT(IGH)	ELM000
7 C		ELM000
8	LA = IGH - 1	ELM000
9	KP1 = LOW + 1	ELM001
10	IF (LA .LT. KP1) GO TO 200	ELM001
11 C		ELM001
12	DO 180 M = KP1, LA	ELM001
13	MM1 = M - 1	ELM001
14	X = 0.000	ELM001
15	I = M	ELM001
16 C		ELM001
17	DO 100 J = M, IGH	ELM001
18	IF (DABS(A(J,MM1)) .LE. DABS(X)) GO TO 100	ELM001
19	X = A(J,MM1)	ELM002
20	I = J	ELM002
21	100 CONTINUE	ELM002
22 C		ELM002
23	INT(M) = I	ELM002
24	IF (I .EQ. M) GO TO 130	ELM002
25 C	***** INTERCHANGE ROWS AND COLUMNS OF A *****	ELM002
26	DO 110 J = MM1, N	ELM002
27	Y = A(I,J)	ELM002
28	A(I,J) = A(M,J)	ELM002
29	A(M,J) = Y	ELM003
30	110 CONTINUE	ELM003
31 C		ELM003
32	DO 120 J = 1, IGH	ELM003
33	Y = A(J,I)	ELM003
34	A(J,I) = A(J,M)	ELM003
35	A(J,M) = Y	ELM003
36	120 CONTINUE	ELM003
37 C	***** END INTERCHANGE *****	ELM003
38	130 IF (X .EQ. 0.000) GO TO 180	ELM003
39	MP1 = M + 1	ELM004
40 C		ELM004
41	DO 160 I = MP1, IGH	ELM004
42	Y = A(I,MM1)	ELM004
43	IF (Y .EQ. 0.000) GO TO 160	ELM004
44	Y = Y / X	ELM004
45	A(I,MM1) = Y	ELM004
46 C		ELM004
47	DO 140 J = M, N	ELM004
48	140 A(I,J) = A(I,J) - Y * A(M,J)	ELM005
49 C		ELM005
50	DO 150 J = 1, IGH	ELM005
51	150 A(J,M) = A(J,M) + Y * A(J,I)	ELM005
52 C		ELM005
53	160 CONTINUE	ELM005
54 C		ELM005
55	180 CONTINUE	ELM005
56 C		ELM005
57	200 RETURN	ELM005
58 C	***** LAST CARD OF ELMHES *****	ELM005
59	END	ELM005

0	SUBROUTINE HQR(NM,N,LOW,IGH,H,WR,WI,IERR)	HQR0
1	IMPLICIT REAL*8 (A-H,O-Z)	HQR00
2	REAL*8 NORM,MACHEP	HQR0
3	INTEGER I,J,K,L,M,N,EN,LL,MM,NA,NM,IGH,ITS,LOW,MP2,ENM2,IERR	HQR0
4	DIMENSION H(NM,N),WR(N),WI(N)	HQR00
5 C	REAL P,Q,R,S,T,W,X,Y,ZZ,NORM,MACHEP	HQR00
6	REAL*8 DSQRT,DABS,DSIGN	HQR0
7 C	INTEGER MINO	HQR0
8	LOGICAL NOTLAS	HQR00
9 C		HQR0
10 C		HQR0
11 C	***** MACHEP IS A MACHINE DEPENDENT PARAMETER SPECIFYING	HQR00
12 C	THE RELATIVE PRECISION OF FLOATING POINT ARITHMETIC.	HQR00
13 C		HQR0
14 C		HQR00
15	MACHEP = 16.**(-13)	HQR00
16 C		HQR0
17	IERR = 0	HQR0
18	NORM = 0.000	HQR00
19	K = 1	HQR0
20 C	***** STORE ROOTS ISOLATED BY BALANC	HQR0
21 C	AND COMPUTE MATRIX NORM *****	HQR00
22	DO 50 I = 1, N	HQR00
23 C		HQR0
24	DO 40 J = K, N	HQR0
25 40	NORM = NORM + DABS(H(I,J))	HQR00
26 C		HQR0
27	K = I	HQR0
28	IF (I .GE. LOW .AND. I .LE. IGH) GO TO 50	HQR00
29	WR(I) = H(I,I)	HQR0
30	WI(I) = 0.000	HQR0
31 50	CONTINUE	HQR00
32 C		HQR00
33	EN = IGH	HQR0
34	T = 0.000	HQR0
35 C	***** SEARCH FOR NEXT EIGENVALUES *****	HQR00
36 60	IF (EN .LT. LOW) GO TO 1001	HQR0
37	ITS = 0	HQR0
38	NA = EN - 1	HQR00
39	ENM2 = NA - 1	HQR00
40 C	***** LOOK FOR SINGLE SMALL SUB-DIAGONAL ELEMENT	HQR0
41 C	FOR L=EN STEP -1 UNTIL LOW DO -- *****	HQR00
42 70	DO 80 LL = LOW, EN	HQR00
43	L = EN + LOW - LL	HQR0
44	IF (L .EQ. LOW) GO TO 100	HQR0
45	S = DABS(H(L-1,L-1)) + DABS(H(L,L))	HQR00
46	IF (S .EQ. 0.000) S = NORM	HQR00
47	IF (DABS(H(L,L-1)) .LE. MACHEP * S) GO TO 100	HQR0
48 80	CONTINUE	HQR00
49 C	***** FORM SHIFT *****	HQR00
50 100	X = H(EN,EN)	HQR0
51	IF (L .EQ. EN) GO TO 270	HQR0
52	Y = H(NA,NA)	HQR00
53	W = H(EN,NA) * H(NA,EN)	HQR0
54	IF (L .EQ. NA) GO TO 280	HQR0
55	IF (ITS .EQ. 30) GO TO 1000	HQR00
56	IF (ITS .NE. 10 .AND. ITS .NE. 20) GO TO 130	HQR00
57 C	***** FORM EXCEPTIONAL SHIFT *****	HQR0
58	T = T + X	HQR0
59 C		HQR00
60	DO 120 I = LOW, EN	HQR0
61 120	H(I,I) = H(I,I) - X	HQR0
62 C		HQR00



63	S = DABS(H(EN,NA)) + DABS(H(NA,ENM2))	HQR0
64	X = 0.75 * S	HQR0
65	Y = X	HQR0
66	W = -0.4375 * S * S	HQR0
67	130 ITS = ITS + 1	HQR0
68 C	***** LOOK FOR TWO CONSECUTIVE SMALL	HQR0
69 C	SUB-DIAGONAL ELEMENTS.	HQR0
70 C	FOR M=EN-2 STEP -1 UNTIL L DO -- *****	HQR0
71	DO 140 MM = L, ENM2	HQR0
72	M = ENM2 + L - MM	HQR0
73	ZZ = H(M,M)	HQR0
74	R = X - ZZ	HQR0
75	S = Y - ZZ	HQR0
76	P = (R * S - W) / H(M+1,M) + H(M,M+1)	HQR0
77	Q = H(M+1,M+1) - ZZ - R - S	HQR0
78	R = H(M+2,M+1)	HQR0
79	S = DABS(P) + DABS(Q) + DABS(R)	HQR0
80	P = P / S	HQR0
81	Q = Q / S	HQR0
82	R = R / S	HQR0
83	IF (M .EQ. L) GO TO 150	HQR0
84	IF (DABS(H(M,M-1)) * (DABS(Q) + DABS(R)) .LE. MACHEP * DABS(P)	HQR0
85	X * (DABS(H(M-1,M-1)) + DABS(ZZ) + DABS(H(M+1,M+1)))) GO TO 150	HQR0
86	140 CONTINUE	HQR0
87 C		HQR0
88	150 MP2 = M + 2	HQR0
89 C		HQR0
90	DO 160 I = MP2, EN	HQR0
91	H(I,I-2) = 0.000	HQR0
92	IF (I .EQ. MP2) GO TO 160	HQR0
93	H(I,I-3) = 0.000	HQR0
94	160 CONTINUE	HQR0
95 C	***** DOUBLE QR STEP INVOLVING ROWS L TO EN AND	HQR0
96 C	COLUMNS M TO EN *****	HQR0
97	DO 260 K = M, NA	HQR0
98	NOTLAS = K .NE. NA	HQR0
99	IF (K .EQ. M) GO TO 170	HQR0
100	P = H(K,K-1)	HQR0
101	Q = H(K+1,K-1)	HQR0
102	R = 0.000	HQR0
103	IF (NOTLAS) R = H(K+2,K-1)	HQR0
104	X = DABS(P) + DABS(Q) + DABS(R)	HQR0
105	IF (X .EQ. 0.000) GO TO 260	HQR0
106	P = P / X	HQR0
107	Q = Q / X	HQR0
108	R = R / X	HQR0
109	170 S = DSIGN(DSQRT(P*P+Q*Q+R*R),P)	HQR0
110	IF (K .EQ. M) GO TO 180	HQR0
111	H(K,K-1) = -S * X	HQR0
112	GO TO 190	HQR0
113	180 IF (L .NE. M) H(K,K-1) = -H(K,K-1)	HQR0
114	190 P = P * S	HQR0
115	X = P / S	HQR0
116	Y = Q / S	HQR0
117	ZZ = R / S	HQR0
118	Q = Q / P	HQR0
119	R = R / P	HQR0
120 C	***** ROW MODIFICATION *****	HQR0
121	DO 210 J = K, EN	HQR0
122	P = H(K,J) + Q * H(K+1,J)	HQR0
123	IF (.NOT. NOTLAS) GO TO 200	HQR0
124	P = P + R * H(K+2,J)	HQR0
125	H(K+2,J) = H(K+2,J) - P * ZZ	HQR0

126	200	H(K+1,J) = H(K+1,J) - P * Y	HQR
127		H(K,J) = H(K,J) - P * X	HQR
128	210	CONTINUE	HQR
129	C		HQR
130		J = MINO(EN,K+3)	HQR
131	C	***** COLUMN MODIFICATION *****	HQR
132		DO 230 I = L, J	HQR
133		P = X * H(I,K) + Y * H(I,K+1)	HQR
134		IF (.NOT. NOTLAS) GO TO 220	HQR
135		P = P + ZZ * H(I,K+2)	HQR
136		H(I,K+2) = H(I,K+2) - P * R	HQR
137	220	H(I,K+1) = H(I,K+1) - P * Q	HQR
138		H(I,K) = H(I,K) - P	HQR
139	230	CONTINUE	HQR
140	C		HQR
141	260	CONTINUE	HQR
142	C		HQR
143		GO TO 70	HQR
144	C	***** ONE ROOT FOUND *****	HQR
145	270	WR(EN) = X + T	HQR
146		WI(EN) = 0.000	HQR
147		EN = NA	HQR
148		GO TO 60	HQR
149	C	***** TWO ROOTS FOUND *****	HQR
150	280	P = (Y - X) / 2.000	HQR
151		Q = P * P + W	HQR
152		ZZ = DSQRT(DABS(Q))	HQR
153		X = X + T	HQR
154		IF (Q .LT. 0.000) GO TO 320	HQR
155	C	***** REAL PAIR *****	HQR
156		ZZ = P + DSIGN(ZZ,P)	HQR
157		WR(NA) = X + ZZ	HQR
158		WR(EN) = WR(NA)	HQR
159		IF (ZZ .NE. 0.000) WR(EN) = X - W / ZZ	HQR
160		WI(NA) = 0.000	HQR
161		WI(EN) = 0.000	HQR
162		GO TO 330	HQR
163	C	***** COMPLEX PAIR *****	HQR
164	320	WR(NA) = X + P	HQR
165		WR(EN) = X + P	HQR
166		WI(NA) = ZZ	HQR
167		WI(EN) = -ZZ	HQR
168	330	EN = ENM2	HQR
169		GO TO 60	HQR
170	C	***** SET ERROR -- NO CONVERGENCE TO AN	HQR
171	C	EIGENVALUE AFTER 30 ITERATIONS *****	HQR
172	1000	IERR = EN	HQR
173	1001	RETURN	HQR
174	C	***** LAST CARD OF HQR *****	HQR
175		END	HQR

0	SUBROUTINE INVIT(NM,N,A,WR,WI,SELECT,MM,M,Z,IERR,RM1,RV1,RV2)	INV0
1	IMPLICIT REAL*8 (A-H,O-Z)	INV0
2	REAL*8 NORM,NORMV,ILAMB0,MACHEP	INV0
3	INTEGER I,J,K,L,M,N,S,II,IP,MM,MP,NM,NS,N1,UK,IP1,ITS,KM1,IERR	RNV0
4	DIMENSION A(NM,N),WR(N),WI(N),Z(NM,MM),RM1(N,N),RV1(N),RV2(N)	INV0
5 C	REAL T,W,X,Y,EPS3,NORM,NORMV,GROWTO,ILAMB0,MACHEP,RLAMB0,UKROOT	INV0
6	REAL*8 DSQRT,CDABS,DABS,DFLOAT	INV0
7	INTEGER IABS	RNV0
8	LOGICAL*1 SELECT(N)	INV0
9	COMPLEX*16 Z3,DCMPLX	INV0
10	REAL*8 OREAL,ODIMAG	INV0
11 C		INV0
12	MACHEP = 16.**(-13)	INV0
13 C		INV0
14	IERR = 0	INV0
15	UK = 0	RNV0
16	S = 1	INV0
17 C	***** IP = 0, REAL EIGENVALUE	INV0
18 C	1, FIRST OF CONJUGATE COMPLEX PAIR	INV0
19 C	-1, SECOND OF CONJUGATE COMPLEX PAIR *****	INV0
20	IP = 0	INV0
21	N1 = N - 1	RNV0
22 C		INV0
23	DO 980 K = 1, N	INV0
24	IF (WI(K) .EQ. 0.000 .OR. IP .LT. 0) GO TO 100	INV0
25	IP = 1	INV0
26	IF (SELECT(K) .AND. SELECT(K+1)) SELECT(K+1) = .FALSE.	INV0
27 100	IF (.NOT. SELECT(K)) GO TO 960	INV0
28	IF (WI(K) .NE. 0.000) S = S + 1	INV0
29	IF (S .GT. MM) GO TO 1000	INV0
30	IF (UK .GE. K) GO TO 200	INV0
31 C	***** CHECK FOR POSSIBLE SPLITTING *****	INV0
32	DO 120 UK = K, N	INV0
33	IF (UK .EQ. N) GO TO 140	INV0
34	IF (A(UK+1,UK) .EQ. 0.000) GO TO 140	INV0
35 120	CONTINUE	INV0
36 C	***** COMPUTE INFINITY NORM OF LEADING UK BY UK	INV0
37 C	(HESSENBERG) MATRIX *****	INV0
38 140	NORM = 0.000	INV0
39	MP = 1	INV0
40 C		INV0
41	DO 180 I = 1, UK	INV0
42	X = 0.000	INV0
43 C		INV0
44	DO 160 J = MP, UK	INV0
45 160	X = X + DABS(A(I,J))	INV0
46 C		INV0
47	IF (X .GT. NORM) NORM = X	INV0
48	MP = I	INV0
49 180	CONTINUE	INV0
50 C	***** EPS3 REPLACES ZERO PIVOT IN DECOMPOSITION	INV0
51 C	AND CLOSE ROOTS ARE MODIFIED BY EPS3-*****	RNV0
52	IF (NORM .EQ. 0.000) NORM = 1.000	INV0
53	EPS3 = MACHEP * NORM	INV0
54 C	***** GROWTO IS THE CRITERION FOR THE GROWTH *****	INV0
55	UKROOT = DSQRT(DFLOAT(UK))	INV0
56	GROWTO = 1.00-1 / UKROOT	INV0
57 200	RLAMB0 = WR(K)	INV0
58	ILAMB0 = WI(K)	INV0
59	IF (K .EQ. 1) GO TO 280	INV0
60	KM1 = K - 1	INV0
61	GO TO 240	INV0
62 C	***** PEPTURB EIGENVALUE IF IT IS CLOSE	INV0

63	C		TO ANY PREVIOUS EIGENVALUE *****	RNV0
64		220	RLAMBD = RLAMBD + EPS3	INV0
65	C		***** FOR I=K-1 STEP -1 UNTIL 1 DO -- *****	INV0
66		240	DO 260 II = 1, KMI	INV0
67			I = K - II	INV0
68			IF (SELECT(I) .AND. DABS(WR(I)-RLAMBD) .LT. EPS3 .AND.	INV0
69		X	DABS(WI(I)-ILAMBD) .LT. EPS3) GO TO 220	INV0
70		260	CONTINUE	INV0
71	C			INV0
72			WR(K) = RLAMBD	INV0
73	C		***** PERTURB CONJUGATE EIGENVALUE TO MATCH *****	INV0
74			IP1 = K + IP	INV0
75			WR(IP1) = RLAMBD	INV0
76	C		***** FORM UPPER HESSENBERG A-RLAMBD*I (TRANPOSED)	RNV0
77	C		AND INITIAL REAL VECTOR *****	INV0
78		280	MP = 1	INV0
79	C			INV0
80			DO 320 I = 1, UK	INV0
81	C			RNV0
82			DO 300 J = MP, UK	INV0
83		300	RM1(J,I) = A(I,J)	INV0
84	C			INV0
85			RM1(I,I) = RM1(I,I) - RLAMBD	INV0
86			MP = I	INV0
87			RV1(I) = EPS3	RNV0
88		320	CONTINUE	INV0
89	C			INV0
90			ITS = 0	INV0
91			IF (ILAMBD .NE. 0.000) GO TO 520	INV0
92	C		***** REAL EIGENVALUE.	INV0
93	C		TRIANGULAR DECOMPOSITION WITH INTERCHANGES,	INV0
94	C		REPLACING ZERO PIVOTS BY EPS3 *****	INV0
95			IF (UK .EQ. 1) GO TO 420	INV0
96	C			INV0
97			DO 400 I = 2, UK	INV0
98			MP = I - 1	INV0
99			IF (DABS(RM1(MP,I)) .LE. DABS(RM1(MP,MP))) GO TO 360	INV0
100	C			INV0
101			DO 340 J = MP, UK	INV0
102			Y = RM1(J,I)	INV0
103			RM1(J,I) = RM1(J,MP)	INV0
104			RM1(J,MP) = Y	INV0
105		340	CONTINUE	INV0
106	C			INV0
107		360	IF (RM1(MP,MP) .EQ. 0.000) RM1(MP,MP) = EPS3	INV0
108			X = RM1(MP,I) / RM1(MP,MP)	INV0
109			IF (X .EQ. 0.000) GO TO 400	INV0
110	C			INV0
111			DO 380 J = I, UK	INV0
112		380	RM1(J,I) = RM1(J,I) - X * RM1(J,MP)	INV0
113	C			INV0
114		400	CONTINUE	INV0
115	C			INV0
116		420	IF (RM1(UK,UK) .EQ. 0.000) RM1(UK,UK) = EPS3	INV0
117	C		***** BACK SUBSTITUTION FOR REAL VECTOR	INV0
118	C		FOR I=UK STEP -1 UNTIL 1 DO -- *****	RNV0
119		440	DO 500 II = 1, UK	INV0
120			I = UK + 1 - II	INV0
121			Y = RV1(I)	INV0
122			IF (I .EQ. UK) GO TO 480	INV0
123			IP1 = I + 1	INV0
124	C			INV0
125			DO 460 J = IP1, UK	INV0

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126	460	Y = Y - RM1(J,I) * RV1(J)	INVO
127	C		INVO
128	480	RV1(I) = Y / RM1(I,I)	INVO
129	500	CONTINUE	INVO
130	C		INVO
131		GO TO 740	INVO
132	C	***** COMPLEX EIGENVALUE.	INVO
133	C	TRIANGULAR DECOMPOSITION WITH INTERCHANGES,	RNVO
134	C	REPLACING ZERO PIVOTS BY EPS3. STORE IMAGINARY	INVO
135	C	PARTS IN UPPER TRIANGLE STARTING AT (1,3) *****	INVO
136	520	NS = N - S	RNVO
137		Z(1,S-1) = -ILAMBD	INVO
138		Z(1,S) = 0.000	INVO
139		IF (N.EQ. 2) GO TO 550	INVO
140		RM1(1,3) = -ILAMBD	INVO
141		Z(1,S-1) = 0.000	INVO
142		IF (N.EQ. 3) GO TO 550	INVO
143	C		INVO
144		DO 540 I = 4, N	INVO
145	540	RM1(1,I) = 0.000	INVO
146	C		INVO
147	550	DO 640 I = 2, UK	INVO
148		MP = I - 1	INVO
149		W = RM1(MP,I)	INVO
150		IF (I.LT. N) T = RM1(MP,I+1)	INVO
151		IF (I.EQ. N) T = Z(MP,S-1)	INVO
152		X = RM1(MP,MP) * RM1(MP,MP) + T * T	INVO
153		IF (W * W.LE. X) GO TO 580	INVO
154		X = RM1(MP,MP) / W	INVO
155		Y = T / W	INVO
156		RM1(MP,MP) = W	INVO
157		IF (I.LT. N) RM1(MP,I+1) = 0.000	INVO
158		IF (I.EQ. N) Z(MP,S-1) = 0.000	INVO
159	C		INVO
160		DO 560 J = I, UK	INVO
161		W = RM1(J,I)	INVO
162		RM1(J,I) = RM1(J,MP) - X * W	INVO
163		RM1(J,MP) = W	INVO
164		IF (J.LT. N1) GO TO 555	INVO
165		L = J - NS	INVO
166		Z(I,L) = Z(MP,L) - Y * W	INVO
167		Z(MP,L) = 0.000	INVO
168		GO TO 560	INVO
169	555	RM1(I,J+2) = RM1(MP,J+2) - Y * W	INVO
170		RM1(MP,J+2) = 0.000	INVO
171	560	CONTINUE	INVO
172	C		INVO
173		RM1(I,I) = RM1(I,I) - Y * ILAMBD	INVO
174		IF (I.LT. N1) GO TO 570	INVO
175		L = I - NS	INVO
176		Z(MP,L) = -ILAMBD	INVO
177		Z(I,L) = Z(I,L) + X * ILAMBD	INVO
178		GO TO 640	INVO
179	570	RM1(MP,I+2) = -ILAMBD	RNVO
180		RM1(I,I+2) = RM1(I,I+2) + X * ILAMBD	INVO
181		GO TO 640	INVO
182	580	IF (X.NE. 0.000) GO TO 600	INVO
183		RM1(MP,MP) = EPS3	INVO
184		IF (I.LT. N) RM1(MP,I+1) = 0.000	INVO
185		IF (I.EQ. N) Z(MP,S-1) = 0.000	INVO
186		T = 0.000	INVO
187		X = EPS3 * EPS3	INVO
188	600	W = W / X	INVO

189		X = RM1(MP,MP) * W	INV01
190		Y = -T * W	INV01
191	C		INV01
192		DO 620 J = 1, UK	INV01
193		IF (J .LT. N1) GO TO 610	INV01
194		L = J - NS	INV01
195		T = Z(MP,L)	INV01
196		Z(I,L) = -X * T - Y * RM1(J,MP)	INV01
197		GO TO 615	INV01
198	610	T = RM1(MP,J+2)	INV01
199		RM1(I,J+2) = -X * T - Y * RM1(J,MP)	INV02
200	615	RM1(J,I) = RM1(J,I) - X * RM1(J,MP) + Y * T	INV02
201	620	CONTINUE	INV02
202	C		INV02
203		IF (I .LT. N1) GO TO 630	INV02
204		L = I - NS	INV02
205		Z(I,L) = Z(I,L) - ILAMBD	INV02
206		GO TO 640	INV02
207	630	RM1(I,I+2) = RM1(I,I+2) - ILAMBD	INV02
208	640	CONTINUE	INV02
209	C		INV02
210		IF (UK .LT. N1) GO TO 650	INV02
211		L = UK - NS	INV02
212		T = Z(UK,L)	INV02
213		GO TO 655	INV02
214	650	T = RM1(UK,UK+2)	INV02
215	655	IF (RM1(UK,UK) .EQ. 0.000 .AND. T .EQ. 0.000) RM1(UK,UK) = EPS3	INV02
216	C	***** BACK SUBSTITUTION FOR COMPLEX VECTOR	INV02
217	C	FOR I=UK STEP -1 UNTIL 1 DO -- *****	INV02
218	660	DO 720 II = 1, UK	INV02
219		I = UK + 1 - II	INV02
220		X = RV1(I)	INV02
221		Y = 0.000	INV02
222		IF (I .EQ. UK) GO TO 700	INV02
223		IP1 = I + 1	INV02
224	C		INV02
225		DO 680 J = IP1, UK	INV02
226		IF (J .LT. N1) GO TO 670	INV02
227		L = J - NS	INV02
228		T = Z(I,L)	INV02
229		GO TO 675	INV02
230	670	T = RM1(I,J+2)	INV02
231	675	X = X - RM1(J,I) * RV1(J) + T * RV2(J)	INV02
232		Y = Y - RM1(J,I) * RV2(J) - T * RV1(J)	INV02
233	680	CONTINUE	INV02
234	C		INV02
235	700	IF (I .LT. N1) GO TO 710	INV02
236		L = I - NS	INV02
237		T = Z(I,L)	INV02
238		GO TO 715	INV02
239	710	T = RM1(I,I+2)	INV02
240	715	Z3 = DCMPLEX(X,Y) / DCMPLEX(RM1(I,I),T)	INV02
241		RV1(I) = DREAL(Z3)	INV02
242		RV2(I) = DIMAG(Z3)	INV02
243	720	CONTINUE	INV02
244	C	***** ACCEPTANCE TEST FOR REAL OR COMPLEX	INV02
245	C	EIGENVECTOR AND NORMALIZATION *****	INV02
246	740	ITS = ITS + 1	INV02
247		NORM = 0.000	INV02
248		NORMV = 0.000	INV02
249	C		INV02
250		DO 780 I = 1, UK	INV02
251		IF (ILAMBD .EQ. 0.000) X = DABS(RV1(I))	INV02

252		IF (ILAMBD .NE. 0.000) X = COABS(DCMPLX(RV1(I),RV2(I)))	INV01
253		IF (NORMV .GE. X) GO TO 760	INV02
254		NORMV = X	INV02
255		J = I	INV01
256	760	NORM = NORM + X	INV02
257	780	CONTINUE	INV02
258	C		INV01
259		IF (NORM .LT. GROWTO) GO TO 840	INV01
260	C	***** ACCEPT VECTOR *****	INV02
261		X = RV1(J)	INV02
262		IF (ILAMBD .EQ. 0.000) X = 1.000 / X	INV01
263		IF (ILAMBD .NE. 0.000) Y = RV2(J)	RNV02
264	C		INV02
265		DO 820 I = 1, UK	/0
266		IF (ILAMBD .NE. 0.000) GO TO 800	INV01
267		Z(I,S) = RV1(I) * X	INV02
268		GO TO 820	INV01
269	800	Z3 = DCMPLX(RV1(I),RV2(I)) / DCMPLX(X,Y)	INV01
270		Z(I,S-1) = DREAL(Z3)	RNV02
271		Z(I,S) = DIMAG(Z3)	INV02
272	820	CONTINUE	INV01
273	C		INV02
274		IF (UK .EQ. N) GO TO 940	INV02
275		J = UK + 1	INV01
276		GO TO 900	INV01
277	C	***** IN-LINE PROCEDURE FOR CHOOSING	INV02
278	C	A NEW STARTING VECTOR *****	INV01
279	840	IF (ITS .GE. UK) GO TO 880	INV01
280		X = UKROOT	INV02
281		Y = EPS3 / (X + 1.000)	RNV02
282		RV1(1) = EPS3	INV01
283	C		INV01
284		DO 860 I = 2, UK	INV02
285	860	RV1(I) = Y	INV01
286	C		INV01
287		J = UK - ITS + 1	INV02
288		RV1(J) = RV1(J) - EPS3 * X	INV02
289		IF (ILAMBD .EQ. 0.000) GO TO 440	INV01
290		GO TO 660	INV02
291	C	***** SET ERROR == UNACCEPTED EIGENVECTOR *****	INV02
292	880	J = 1	INV01
293		IERR = -K	INV01
294	C	***** SET REMAINING VECTOR COMPONENTS TO ZERO *****	INV02
295	900	DO 920 I = J, N	INV02
296		Z(I,S) = 0.000	INV01
297		IF (ILAMBD .NE. 0.000) Z(I,S-1) = 0.000	INV02
298	920	CONTINUE	INV02
299	C		INV01
300	940	S = S + 1	INV01
301	960	IF (IP .EQ. (-1)) IP = 0	INV03
302		IF (IP .EQ. 1) IP = -1	INV01
303	980	CONTINUE	INV01
304	C		INV03
305		GO TO 1001	INV01
306	C	***** SET ERROR == UNDERESTIMATE OF EIGENVECTOR	INV01
307	C	SPACE REQUIRED *****	INV03
308	1000	IF (IERR .NE. 0) IERR = IERR - N	INV03
309		IF (IERR .EQ. 0) IERR = -(2 * N + 1)	INV01
310	1001	M = S - 1 - IABS(IP)	INV01
311		RETURN	INV03
312	C	***** LAST CARD OF INVIT *****	INV01
313		END	INV01

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0	SUBROUTINE ELMLBAK(NM,LOW,IGH,A,INT,M,Z)	ELM000
1	IMPLICIT REAL*8 (A-H,O-Z)	ELM000
2	INTEGER I,J,M,LA,MM,MP,NM,IGH,KP1,LOW,MP1	ELM000
3	DIMENSION A(NM,IGH),Z(NM,M)	ELM000
4 C	REAL X	ELM000
5	INTEGER INT(IGH)	ELM000
6 C		ELM000
7 C		ELM000
8	IF (M.EQ. 0) GO TO 200	ELM000
9	LA = IGH - 1	ELM000
10	KP1 = LOW + 1	ELM000
11	IF (LA.LT. KP1) GO TO 200	ELM001
12 C	***** FOR MP=IGH-1 STEP -1 UNTIL LOW+1 DO == *****	ELM001
13	DO 140 MM = KP1, LA	ELM001
14	MP = LOW + IGH - MM	ELM001
15	MP1 = MP + 1	ELM001
16 C		ELM001
17	DO 110 I = MP1, IGH	ELM001
18	X = A(I,MP-1)	ELM001
19	IF (X.EQ. 0.0) GO TO 110	ELM002
20 C		ELM002
21	DO 100 J = 1, M	ELM002
22 100	Z(I,J) = Z(I,J) + X * Z(MP,J)	ELM002
23 C		ELM002
24 110	CONTINUE	ELM002
25 C		ELM002
26	I = INT(MP)	ELM002
27	IF (I.EQ. MP) GO TO 140	ELM002
28 C		ELM002
29	DO 130 J = 1, M	ELM003
30	X = Z(I,J)	ELM003
31	Z(I,J) = Z(MP,J)	ELM003
32	Z(MP,J) = X	ELM003
33 130	CONTINUE	ELM003
34 C		ELM003
35 140	CONTINUE	ELM003
36 C		ELM003
37 200	RETURN	ELM003
38 C	***** LAST CARD OF ELMLBAK *****	ELM003
39	END	ELM004



0	SUBROUTINE BALBAK(NM,N,LOW,IGH,SCALE,M,Z)	BAL00
1	IMPLICIT REAL*8 (A-H,O-Z)	BAL00
2	INTEGER I,J,K,M,N,II,NM,IGH,LOW	BAL00
3	DIMENSION SCALE(N),Z(NM,M)	BAL00
4 C	REAL S	BAL00
5	IF (M.EQ. 0) GO TO 200	BAL00
6	IF (IGH.EQ. LOW) GO TO 120	BAL00
7 C		BAL00
8	DO 110 I = LOW, IGH	BAL00
9	S = SCALE(I)	BAL00
10 C	***** LEFT HAND EIGENVECTORS ARE BACK TRANSFORMED	BAL00
11 C	IF THE FOREGOING STATEMENT IS REPLACED BY	BAL00
12 C	S=1.0/SCALE(I). *****	BAL00
13	DO 100 J = 1, M	BAL00
14 100	Z(I,J) = Z(I,J) * S	BAL00
15 C		BAL00
16	110 CONTINUE	BAL00
17 C	***** FOR I=LOW-1 STEP -1 UNTIL 1,	BAL00
18 C	IGH+1 STEP 1 UNTIL N DO == *****	BAL00
19 120	DO 140 II = 1, N	BAL00
20	I = II	BAL00
21	IF (I.GE. LOW.AND. I.LE. IGH) GO TO 140	BAL00
22	IF (I.LT. LOW) I = LOW - II	BAL00
23	K = SCALE(I)	BAL00
24	IF (K.EQ. I) GO TO 140	BAL00
25 C		BAL00
26	DO 130 J = 1, M	BAL00
27	S = Z(I,J)	BAL00
28	Z(I,J) = Z(K,J)	BAL00
29	. Z(K,J) = S	BAL00
30 130	CONTINUE	BAL00
31 C		BAL00
32	140 CONTINUE	BAL00
33 C		BAL00
34 200	RETURN	BAL00
35 C	***** LAST CARD OF BALBAK *****	BAL00
36	END	BAL00

0		SUBROUTINE DETFAC(NMAX,N,A,IPIVOT,IDET,DETERM,ISCALE,WK,IERR)	DET00
1		IMPLICIT REAL*8 (A-H,O-Z)	DET00
2		DIMENSION A(NMAX,1),IPIVOT(1),WK(1)	DET00
3	C		DET00
4	C		DET00
5		ISCALE=0	DET00
6		NM1=N-1	DET00
7		IERR=0	DET00
8	C		DET00
9	C	DETERMINANT CALCULATION TEST	DET00
10	C		DET00
11		IF(IDET.EQ.1)GO TO 230	DET00
12	C		DET00
13	C	TEST FOR A SCALAR MATRIX	DET00
14	C		DET00
15		IF(NM1.GT.0)GO TO 20	DET00
16		DETERM=A(1,1)	DET00
17		RETURN	DET00
18	C		DET00
19	C	COMPUTE SCALING FACTORS	DET00
20	C		DET00
21	20	CONTINUE	DET00
22		DO 60 I=1,N	DET00
23		P=0.0	DET00
24		DO 30 J=1,N	DET00
25		Q=OMAX1(P,DABS(A(I,J)))	DET00
26		IF(Q.GT.P)P=Q	DET00
27	30	CONTINUE	DET00
28		IF(P)60,40,60	DET00
29	40	DETERM=0.0	DET00
30		IERR=1	DET00
31		RETURN	DET00
32	60	WK(I)=P	DET00
33	C		DET00
34		DO 210 M=1,NM1	DET00
35	C		DET00
36	C	PIVOTAL LOGIC SETUP	DET00
37	C		DET00
38		P=0.0	DET00
39		DO 110 I=M,N	DET00
40		Q=DABS(A(I,M)/WK(I))	DET00
41		IF(Q=P)110,110,100	DET00
42	100	P=Q	DET00
43		IP=I	DET00
44	110	CONTINUE	DET00
45	C		DET00
46		IPIVOT(M)=IP	DET00
47	C		DET00
48		IF(P.EQ.0.)GO TO 40	DET00
49		IF(M.EQ.IP)GO TO 155	DET00
50	C		DET00
51	C	PIVOT THE M-TH ROW OF THE A MATRIX	DET00
52	C		DET00
53		DO 150 I=1,N	DET00
54		P=A(IP,I)	DET00
55		A(IP,I)=A(M,I)	DET00
56	150	A(M,I)=P	DET00
57	C		DET00
58		P=WK(IP)	DET00
59		WK(IP)=WK(M)	DET00
60		WK(M)=P	DET00
61	C		DET00
62	155	MP1=M+1	DET00

63	C			DETO
64	C	L/U FACTORIZATION LOGIC		DETO
65	C			DETOO
66		P=A(M,M)		DETO
67		DO 180 I=MP1,N		DETO
68		A(I,M)=A(I,M)/P		DETOO
69		Q=A(I,M)		DETOO
70		DO 180 K=MP1,N		DETO
71	180	A(I,K)=A(I,K)-Q*A(M,K)		DETOO
72	C			DETOO
73	210	CONTINUE		DETO
74	C			DETO
75		IPIVOT(N)=N		DETOO
76		IF (A(N,N) .EQ. 0.0) GO TO 40		DETO
77	C			DETO
78	C	CALCULATION OF THE DETERMINANT OF A		DETOO
79	C			DETOO
80		IF(IDET.EQ.0)RETURN		DETO
81	C			DETO
82	230	SIGN=1.0		DETOO
83		DETERM=1.0		DETO
84	C			DETO
85	C	ADJUST SIGN OF DETERMINANT DUE TO PIVOTAL STRATEGY		DETOO
86	C			DETO
87		DO 250 I=1,NM1		DETO
88		IF(I-IPIVOT(I))240,250,240		DETO
89	240	SIGN=-SIGN		DETOO
90	250	CONTINUE		DETO
91	C			DETO
92		DO 340 I=1,N		DETOO
93		P=A(I,I)		DETO
94	C			DETO
95	260	CONTINUE		DETOO
96		IF(R1.GT.DABS(P))GO TO 280		DETOO
97		P=P*R2		DETO
98		ISCALE=ISCALE+1		DETO
99		GO TO 260		DETO1
100	C			DETO
101	280	CONTINUE		DETO
102		IF(R2.LT.DABS(P))GO TO 290		DETO1
103		P=P*R1		DETO
104		ISCALE=ISCALE-1		DETO
105		GO TO 280		DETO1
106	C			DETO1
107	290	DETERM=DETERM*P		DETO
108	C			DETO
109	300	CONTINUE		DETO1
110		IF(R1.GT.DABS(DETERM))GO TO 320		DETO
111		DETERM=DETERM*R2		DETO
112		ISCALE=ISCALE+1		DETO1
113		GO TO 300		DETO1
114	C			DETO
115	320	CONTINUE		DETO
116		IF(R2.LT.DABS(DETERM))GO TO 340		DETO1
117		DETERM=DETERM*R1		DETO
118		ISCALE=ISCALE-1		DETO
119		GO TO 320		DETO1
120	C			DETO
121	340	CONTINUE		DETO
122	C			DETO1
123		DETERM=DETERM*SIGN		DETO1
124	C			DETO
125		RETURN		DETO

ALL INFORMATION CONTAINED  
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DATE 10-10-2001 BY 60322

0	SUBROUTINE AXPXB(A,U,M,NA,NU,B,V,N,NB,NV,C,NC,EPSA,	AXP0
1	1EPSB,FAIL)	AXP0
2	IMPLICIT REAL*8 (A-H,O-Z)	AXP00
3	DIMENSION	AXP00
4	1A(NA,1),U(NU,1),B(NB,1),V(NV,1),C(NC,1)	AXP0
5	INTEGER	AXP00
6	C	AXP00
7	1 FAIL	AXP0
8	M1 = M+1	AXP0
9	MM1 = M-1	AXP00
10	N1 = N+1	AXP0
11	NM1 = N-1	AXP0
12	C IF REQUIRED, REDUCE A TO UPPER REAL SCHUR FORM.	AXP00
13	C	AXP00
14	IF(EPSA .LT. 0.) GO TO 35	AXP0
15	DO 10 I=1,M	AXP00
16	DO 10 J=I,M	AXP00
17	TEMP = A(I,J)	AXP0
18	A(I,J) = A(J,I)	AXP0
19	A(J,I) = TEMP	AXP00
20	10 CONTINUE	AXP00
21	CALL HSHLDR(A,M,NA)	AXP0
22	CALL BCKMLT(A,U,M,NA,NU)	AXP00
23	IF(MM1 .EQ. 0) GO TO 25	AXP00
24	DO 20 I=1,MM1	AXP0
25	A(I+1,I) = A(I,M1)	AXP0
26	20 CONTINUE	AXP00
27	CALL SCHUR(A,U,M,NA,NU,EPSA,FAIL)	AXP0
28	IF(FAIL .NE. 0) RETURN	AXP0
29	25 DO 30 I=1,M	AXP00
30	DO 30 J=I,M	AXP00
31	TEMP = A(I,J)	AXP0
32	A(I,J) = A(J,I)	AXP00
33	A(J,I) = TEMP	AXP00
34	30 CONTINUE	AXP0
35	C	AXP0
36	C IF REQUIRED, REDUCE B TO UPPER REAL SCHUR FORM.	AXP00
37	C	AXP00
38	35 IF(EPSB .LT. 0.) GO TO 45	AXP0
39	CALL HSHLDR(B,N,NB)	AXP00
40	CALL BCKMLT(B,V,N,NB,NV)	AXP00
41	IF(NM1 .EQ. 0) GO TO 45	AXP0
42	DO 40 I=1,NM1	AXP00
43	B(I+1,I) = B(I,N1)	AXP00
44	40 CONTINUE	AXP00
45	CALL SCHUR(B,V,N,NB,NV,EPSB,FAIL)	AXP00
46	FAIL = -FAIL	AXP00
47	IF(FAIL .NE. 0) RETURN	AXP00
48	C	AXP00
49	C TRANSFORM C.	AXP00
50	C	AXP00
51	45 DO 60 J=1,N	AXP00
52	DO 50 I=1,M	AXP00
53	A(I,M1) = 0.	AXP00
54	DO 50 K=1,M	AXP00
55	A(I,M1) = A(I,M1) + U(K,I)*C(K,J)	AXP00
56	50 CONTINUE	AXP00
57	DO 60 I=1,M	AXP00
58	C(I,J) = A(I,M1)	AXP00
59	60 CONTINUE	AXP00
60	DO 80 I=1,M	AXP00
61	DO 70 J=1,N	AXP00
62	B(N1,J) = 0.	AXP00

63	DO 70 K=1,N	AXP0
64	B(N1,J) = B(N1,J) + C(I,K)*V(K,J)	AXP0
65	70 CONTINUE	AXP0
66	DO 80 J=1,N	AXP0
67	C(I,J) = B(N1,J)	AXP0
68	80 CONTINUE	AXP0
69	C	AXP0
70	C SOLVE THE TRANSFORMED SYSTEM.	AXP0
71	C	AXP0
72	CALL SHRSLV(A,B,C,M,N,NA,NB,NC)	AXP0
73	C	AXP0
74	C TRANSFORM C BACK TO THE SOLUTION.	AXP0
75	C	AXP0
76	DO 100 J=1,N	AXP0
77	DO 90 I=1,M	AXP0
78	A(I,M1) = 0.	AXP0
79	DO 90 K=1,M	AXP0
80	A(I,M1) = A(I,M1) + U(I,K)*C(K,J)	AXP0
81	90 CONTINUE	AXP0
82	DO 100 I=1,M	AXP0
83	C(I,J) = A(I,M1)	AXP0
84	100 CONTINUE	AXP0
85	DO 120 I=1,M	AXP0
86	DO 110 J=1,N	AXP0
87	B(N1,J) = 0.	AXP0
88	DO 110 K=1,N	AXP0
89	B(N1,J) = B(N1,J) + C(I,K)*V(J,K)	AXP0
90	110 CONTINUE	AXP0
91	DO 120 J=1,N	AXP0
92	C(I,J) = B(N1,J)	AXP0
93	120 CONTINUE	AXP0
94	RETURN	AXP0
95	END	AXP0

0		SUBROUTINE SHRSLV(A,R,C,M,N,NA,NB,NC)	SHR00
1		IMPLICIT REAL*8 (A-H,O-Z)	SHR00
2		DIMENSION	SHR00
3		1A(NA,1),B(NB,1),C(NC,1)	SHR00
4		INTEGER	SHR00
5		1 DK,DL	SHR00
6		COMMON/SLVBLK/T(5,5),P(5),NSYS	SHR00
7		L = 1	SHR00
8	10	LM1 = L-1	SHR00
9		DL = 1	SHR00
10		IF(L .EQ. N) GO TO 15	SHR00
11		IF(B(L+1,L) .NE. 0.) DL = 2	SHR00
12	15	LL = L+DL-1	SHR00
13		IF(L .EQ. 1) GO TO 30	SHR00
14		DO 20 J=L,LL	SHR00
15		DO 20 I=1,M	SHR00
16		DO 20 IB=1,LM1	SHR00
17		C(I,J) = C(I,J) - C(I,IB)*B(IB,J)	SHR00
18	20	CONTINUE	SHR00
19	30	K = 1	SHR00
20	40	KM1 = K-1	SHR00
21		DK = 1	SHR00
22		IF(K .EQ. M) GO TO 45	SHR00
23		IF(A(K,K+1) .NE. 0.) DK = 2	SHR00
24	45	KK = K+DK-1	SHR00
25		IF(K .EQ. 1) GO TO 60	SHR00
26		DO 50 I=K,KK	SHR00
27		DO 50 J=L,LL	SHR00
28		DO 50 JA=1,KM1	SHR00
29		C(I,J) = C(I,J) - A(I,JA)*C(JA,J)	SHR00
30	50	CONTINUE	SHR00
31	60	IF(DL .EQ. 2) GO TO 80	SHR00
32		IF(DK .EQ. 2) GO TO 70	SHR00
33		T(1,1) = A(K,K) + B(L,L)	SHR00
34		IF(T(1,1) .EQ. 0.) STOP	SHR00
35		C(K,L) = C(K,L)/T(1,1)	SHR00
36		GO TO 100	SHR00
37	70	T(1,1) = A(K,K) + B(L,L)	SHR00
38		T(1,2) = A(K,KK)	SHR00
39		T(2,1) = A(KK,K)	SHR00
40		T(2,2) = A(KK,KK) + B(L,L)	SHR00
41		P(1) = C(K,L)	SHR00
42		P(2) = C(KK,L)	SHR00
43		NSYS = 2	SHR00
44		CALL SYSSLV	SHR00
45		C(K,L) = P(1)	SHR00
46		C(KK,L) = P(2)	SHR00
47		GO TO 100	SHR00
48	80	IF(DK .EQ. 2) GO TO 90	SHR00
49		T(1,1) = A(K,K) + B(L,L)	SHR00
50		T(1,2) = B(LL,L)	SHR00
51		T(2,1) = B(L,LL)	SHR00
52		T(2,2) = A(K,K) + B(LL,LL)	SHR00
53		P(1) = C(K,L)	SHR00
54		P(2) = C(K,LL)	SHR00
55		NSYS = 2	SHR00
56		CALL SYSSLV	SHR00
57		C(K,L) = P(1)	SHR00
58		C(K,LL) = P(2)	SHR00
59		GO TO 100	SHR00
60	90	T(1,1) = A(K,K) + B(L,L)	SHR00
61		T(1,2) = A(K,KK)	SHR00
62		T(1,3) = B(LL,L)	SHR00

63	T(1,4) = 0.	SHR00
64	T(2,1) = A(KK,K)	SHR00
65	T(2,2) = A(KK,KK) + B(L,L)	SHR00
66	T(2,3) = 0.	SHR00
67	T(2,4) = T(1,3)	SHR00
68	T(3,1) = B(L,LL)	SHR00
69	T(3,2) = 0.	SHR00
70	T(3,3) = A(K,K) + B(LL,LL)	SHR00
71	T(3,4) = T(1,2)	SHR00
72	T(4,1) = 0.	SHR00
73	T(4,2) = T(3,1)	SHR00
74	T(4,3) = T(2,1)	SHR00
75	T(4,4) = A(KK,KK) + B(LL,LL)	SHR00
76	P(1) = C(K,L)	SHR00
77	P(2) = C(KK,L)	SHR00
78	P(3) = C(K,LL)	SHR00
79	P(4) = C(KK,LL)	SHR00
80	NSYS = 4	SHR00
81	CALL SYSSLV	SHR00
82	C(K,L) = P(1)	SHR00
83	C(KK,L) = P(2)	SHR00
84	C(K,LL) = P(3)	SHR00
85	C(KK,LL) = P(4)	SHR00
86	100 K = K + DK	SHR00
87	IF(K .LE. M) GO TO 40	SHR00
88	L = L + DL	SHR00
89	IF(L .LE. N) GO TO 10	SHR00
90	RETURN	SHR00
91	END	SHR00



0	SUBROUTINE ATXPA(A,U,C,N,NA,NU,NC,EPS,FAIL)	ATX00
1	IMPLICIT REAL*8 (A-H,O-Z)	ATX00
2	DIMENSION	ATX00
3	1A(NA,1),U(NU,1),C(NC,1)	ATX00
4	INTEGER	ATX00
5	1 FAIL	ATX00
6	N1 = N+1	ATX00
7	NM1 = N-1	ATX00
8	C	ATX00
9	C IF REQUIRED, REDUCE A TO LOWER REAL SCHUR FORM.	ATX00
10	C	ATX00
11	IF(EPS .LT. 0.) GO TO 15	ATX00
12	CALL HSHLDR(A,N,NA)	ATX00
13	CALL BCKMLT(A,U,N,NA,NU)	ATX00
14	DO 10 I=1,NM1	ATX00
15	A(I+1,I) = A(I,N1)	ATX00
16	10 CONTINUE	ATX00
17	CALL SCHUR(A,U,N,NA,NU,EPS,FAIL)	ATX00
18	IF(FAIL .NE. 0) RETURN	ATX00
19	C	ATX00
20	C TRANSFORM C.	ATX00
21	C	ATX00
22	15 DO 20 I=1,N	ATX00
23	C(I,I)=C(I,I)/2.	ATX00
24	20 CONTINUE	ATX00
25	DO 40 I=1,N	ATX00
26	DO 30 J=1,N	ATX00
27	A(N1,J) = 0.	ATX00
28	DO 30 K=I,N	ATX00
29	A(N1,J) = A(N1,J) + C(I,K)*U(K,J)	ATX00
30	30 CONTINUE	ATX00
31	DO 40 J=1,N	ATX00
32	C(I,J) = A(N1,J)	ATX00
33	40 CONTINUE	ATX00
34	DO 60 J=1,N	ATX00
35	DO 50 I=1,N	ATX00
36	A(I,N1) = 0.	ATX00
37	DO 50 K=1,N	ATX00
38	A(I,N1) = A(I,N1) + U(K,I)*C(K,J)	ATX00
39	50 CONTINUE	ATX00
40	DO 60 I=1,N	ATX00
41	C(I,J) = A(I,N1)	ATX00
42	60 CONTINUE	ATX00
43	DO 70 I=1,N	ATX00
44	DO 70 J=I,N	ATX00
45	C(I,J) = C(I,J) + C(J,I)	ATX00
46	C(J,I) = C(I,J)	ATX00
47	70 CONTINUE	ATX00
48	C	ATX00
49	C SOLVE THE TRANSFORMED SYSTEM.	ATX00
50	C	ATX00
51	CALL SYMSLV(A,C,N,NA,NC)	ATX00
52	C	ATX00
53	C TRANSFORM C BACK TO THE SOLUTION.	ATX00
54	C	ATX00
55	DO 80 I=1,N	ATX00
56	C(I,I) = C(I,I)/2.	ATX00
57	80 CONTINUE	ATX00
58	DO 100 I=1,N	ATX00
59	DO 90 J=1,N	ATX00
60	A(N1,J) = 0.	ATX00
61	DO 90 K=I,N	ATX00
62	A(N1,J) = A(N1,J) + C(I,K)*U(J,K)	ATX00

63	90	CONTINUE	ATX00
64		DO 100 J=1,N	ATX00
65		C(I,J) = A(N1,J)	ATX00
66	100	CONTINUE	ATX00
67		DO 120 J=1,N	ATX00
68		DO 110 I=1,N	ATX00
69		A(I,N1) = 0.	ATX00
70		DO 110 K=1,N	ATX00
71		A(I,N1) = A(I,N1) + U(I,K)*C(K,J)	ATX00
72	110	CONTINUE	ATX00
73		DO 120 I=1,N	ATX00
74		C(I,J) = A(I,N1)	ATX00
75	120	CONTINUE	ATX00
76		DO 130 I=1,N	ATX00
77		DO 130 J=1,N	ATX00
78		C(I,J) = C(I,J) + C(J,I)	ATX00
79		C(J,I) = C(I,J)	ATX00
80	130	CONTINUE	ATX00
81		RETURN	ATX00
82		END	ATX00

0		SUBROUTINE SYMSLV(A,C,N,NA,NC)	SYMC
1		IMPLICIT REAL*8 (A-H,O-Z)	SYMC
2		DIMENSION	SYMC
3		1A(NA,1),C(NC,1)	SYMC
4		INTEGER	SYMC
5		1 DK,OL	SYMC
6		COMMON/SLVBK/T(5,5),P(5),NSYS	SYMC
7		L = 1	SYMC
8	10	DL = 1	SYMC
9		IF(L.EQ. N) GO TO 20	SYMC
10		IF(A(L+1,L).NE. 0.) DL = 2	SYMC
11	20	LL = L+DL-1	SYMC
12		K = L	SYMC
13	30	KM1 = K-1	SYMC
14		DK = 1	SYMC
15		IF(K.EQ. N) GO TO 35	SYMC
16		IF(A(K+1,K).NE. 0.) DK = 2	SYMC
17	35	KK = K+DK-1	SYMC
18		IF(K.EQ. L) GO TO 45	SYMC
19		DO 40 I=K,KK	SYMC
20		DO 40 J=L,LL	SYMC
21		DO 40 IA=L,KM1	SYMC
22		C(I,J) = C(I,J) - A(IA,I)*C(IA,J)	SYMC
23	40	CONTINUE	SYMC
24	45	IF(DL.EQ. 2) GO TO 60	SYMC
25		IF(DK.EQ. 2) GO TO 50	SYMC
26		T(1,1) = A(K,K) + A(L,L)	SYMC
27		IF(T(1,1).EQ. 0.) STOP	SYMC
28		C(K,L) = C(K,L)/T(1,1)	SYMC
29		GO TO 90	SYMC
30	50	T(1,1) = A(K,K) + A(L,L)	SYMC
31		T(1,2) = A(KK,K)	SYMC
32		T(2,1) = A(K,KK)	SYMC
33		T(2,2) = A(KK,KK) + A(L,L)	SYMC
34		P(1) = C(K,L)	SYMC
35		P(2) = C(KK,L)	SYMC
36		NSYS = 2	SYMC
37		CALL SYSSLV	SYMC
38		C(K,L) = P(1)	SYMC
39		C(KK,L) = P(2)	SYMC
40		GO TO 90	SYMC
41	60	IF(DK.EQ. 2) GO TO 70	SYMC
42		T(1,1) = A(K,K) + A(L,L)	SYMC
43		T(1,2) = A(LL,L)	SYMC
44		T(2,1) = A(L,LL)	SYMC
45		T(2,2) = A(K,K) + A(LL,LL)	SYMC
46		P(1) = C(K,L)	SYMC
47		P(2) = C(K,LL)	SYMC
48		NSYS = 2	SYMC
49		CALL SYSSLV	SYMC
50		C(K,L) = P(1)	SYMC
51		C(K,LL) = P(2)	SYMC
52		GO TO 90	SYMC
53	70	IF(K.NE. L) GO TO 80	SYMC
54		T(1,1) = A(L,L)	SYMC
55		T(1,2) = A(LL,L)	SYMC
56		T(1,3) = 0.	SYMC
57		T(2,1) = A(L,LL)	SYMC
58		T(2,2) = A(L,L) + A(LL,LL)	SYMC
59		T(2,3) = T(1,2)	SYMC
60		T(3,1) = 0.	SYMC
61		T(3,2) = T(2,1)	SYMC
62		T(3,3) = A(LL,LL)	SYMC

63		P(1) = C(L,L)/2.	SYM0
64		P(2) = C(LL,L)	SYM0
65		P(3) = C(LL,LL)/2.	SYM0
66		NSYS = 3	SYM0
67		CALL SYSSLV	SYM0
68		C(L,L) = P(1)	SYM0
69		C(LL,L) = P(2)	SYM0
70		C(L,LL) = P(2)	SYM0
71		C(LL,LL) = P(3)	SYM0
72		GO TO 90	SYM0
73	80	T(1,1) = A(K,K) + A(L,L)	SYM0
74		T(1,2) = A(KK,K)	SYM0
75		T(1,3) = A(LL,L)	SYM0
76		T(1,4) = 0.	SYM0
77		T(2,1) = A(K,KK)	SYM0
78		T(2,2) = A(KK,KK) + A(L,L)	SYM0
79		T(2,3) = 0.	SYM0
80		T(2,4) = T(1,3)	SYM0
81		T(3,1) = A(L,LL)	SYM0
82		T(3,2) = 0.	SYM0
83		T(3,3) = A(K,K) + A(LL,LL)	SYM0
84		T(3,4) = T(1,2)	SYM0
85		T(4,1) = 0.	SYM0
86		T(4,2) = T(3,1)	SYM0
87		T(4,3) = T(2,1)	SYM0
88		T(4,4) = A(KK,KK) + A(LL,LL)	SYM0
89		P(1) = C(K,L)	SYM0
90		P(2) = C(KK,L)	SYM0
91		P(3) = C(K,LL)	SYM0
92		P(4) = C(KK,LL)	SYM0
93		NSYS = 4	SYM0
94		CALL SYSSLV	SYM0
95		C(K,L) = P(1)	SYM0
96		C(KK,L) = P(2)	SYM0
97		C(K,LL) = P(3)	SYM0
98		C(KK,LL) = P(4)	SYM0
99	90	K = K + DK	SYM01
100		IF(K .LE. N) GO TO 30	SYM01
101		LDL = L + DL	SYM01
102		IF(LDL .GT. N) RETURN	SYM01
103		DO 120 J=LDL,N	SYM01
104		DO 100 I=L,LL	SYM01
105		C(I,J) = C(J,I)	SYM01
106	100	CONTINUE	SYM01
107		DO 120 I=J,N	SYM01
108		DO 110 K=L,LL	SYM01
109		C(I,J) = C(I,J) - C(I,K)*A(K,J) - A(K,I)*C(K,J)	SYM01
110	110	CONTINUE	SYM01
111		C(J,I) = C(I,J)	SYM01
112	120	CONTINUE	SYM01
113		L = LDL	SYM01
114		GO TO 10	SYM01
115		END	SYM01

0	SUBROUTINE HSHLDR(A,N,NA)	HSH0
1	IMPLICIT REAL*8 (A-H,O-Z)	HSH0
2	DIMENSION A(NA,1)	HSH0
3	REAL*8 MAX	HSH0
4	C	HSH0
5	NM2 = N-2	HSH0
6	N1 = N+1	HSH0
7	IF(N .EQ. 1) RETURN	HSH0
8	IF(N .GT. 2) GO TO 5	HSH0
9	A(1,N1) = A(2,1)	HSH0
10	RETURN	HSH0
11	5 DO 80 L=1,NM2	HSH0
12	L1 = L+1	HSH0
13	MAX = 0.	HSH0
14	DO 10 I=L1,N	HSH0
15	MAX = DMAX1(MAX,DABS(A(I,L)))	HSH0
16	10 CONTINUE	HSH0
17	IF(MAX .NE. 0.) GO TO 20	HSH0
18	A(L,N1) = 0.	HSH0
19	A(N1,L) = 0.	HSH0
20	GO TO 80	HSH0
21	20 SUM = 0.	HSH0
22	DO 30 I=L1,N	HSH0
23	A(I,L) = A(I,L)/MAX	HSH0
24	SUM = SUM + A(I,L)**2	HSH0
25	30 CONTINUE	HSH0
26	S = DSIGN(DSQRT(SUM),A(L1,L))	HSH0
27	A(L,N1) = -MAX*S	HSH0
28	A(L1,L) = S + A(L1,L)	HSH0
29	A(N1,L) = S*A(L1,L)	HSH0
30	DO 50 J=L1,N	HSH0
31	SUM = 0.	HSH0
32	DO 40 I=L1,N	HSH0
33	SUM = SUM + A(I,L)*A(I,J)	HSH0
34	40 CONTINUE	HSH0
35	P = SUM/A(N1,L)	HSH0
36	DO 50 I=L1,N	HSH0
37	A(I,J) = A(I,J) - A(I,L)*P	HSH0
38	50 CONTINUE	HSH0
39	DO 70 I=1,N	HSH0
40	SUM = 0.	HSH0
41	DO 60 J=L1,N	HSH0
42	SUM = SUM + A(I,J)*A(J,L)	HSH0
43	60 CONTINUE	HSH0
44	P = SUM/A(N1,L)	HSH0
45	DO 70 J=L1,N	HSH0
46	A(I,J) = A(I,J) - P*A(J,L)	HSH0
47	70 CONTINUE	HSH0
48	80 CONTINUE	HSH0
49	A(N-1,N1) = A(N,N-1)	HSH0
50	RETURN	HSH0
51	END	HSH0

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0	SUBROUTINE BCKMLT(A,U,N,NA,NU)	BCKO
1	IMPLICIT REAL*8 (A-H,O-Z)	BCKO
2	DIMENSION	BCKO
3	1A(NA,1),U(NU,1)	BCKO
4	C	BCKO
5	N1 = N+1	BCKO
6	NM1 = N-1	BCKO
7	NM2 = N-2	BCKO
8	U(N,N) = 1.	BCKO
9	IF(NM1 .EQ. 0) RETURN	BCKO
10	U(NM1,N) = 0.	BCKO
11	U(N,NM1) = 0.	BCKO
12	U(NM1,NM1) = 1.	BCKO
13	IF(NM2 .EQ. 0) RETURN	BCKO
14	DO 40 LL=1,NM2	BCKO
15	L = NM2-LL+1	BCKO
16	L1 = L+1	BCKO
17	IF(A(N1,L) .EQ. 0.) GO TO 25	BCKO
18	DO 20 J=L1,N	BCKO
19	SUM = 0.	BCKO
20	DO 10 I=L1,N	BCKO
21	SUM = SUM + A(I,L)*U(I,J)	BCKO
22	10 CONTINUE	BCKO
23	P = SUM/A(N1,L)	BCKO
24	DO 20 I=L1,N	BCKO
25	U(I,J) = U(I,J) - A(I,L)*P	BCKO
26	20 CONTINUE	BCKO
27	25 DO 30 I=L1,N	BCKO
28	U(I,L) = 0.	BCKO
29	U(L,I) = 0.	BCKO
30	30 CONTINUE	BCKO
31	U(L,L) = 1.	BCKO
32	40 CONTINUE	BCKO
33	RETURN	BCKO
34	END	BCKO

0	SUBROUTINE SCHUR(H,U,NN,NH,NU,EPS,FAIL)	SC
1	IMPLICIT REAL*8 (A-H,O-Z)	SC
2	DIMENSION	SC
3	1H(NH,1),U(NU,1)	SC
4	INTEGER	SC
5	1 FAIL	SC
6	LOGICAL	SC
7	1LAST	SC
8	N = NN	SC
9	HN = 0.	SC
10	DO 20 I=1,N	SC
11	JL = MAX0(1,I-1)	SC
12	RSUM = 0.	SC
13	DO 10 J=JL,N	SC
14	RSUM = RSUM + DABS(H(I,J))	SC
15	10 CONTINUE	SC
16	HN = DMAX1(HN,RSUM)	SC
17	20 CONTINUE	SC
18	TEST = EPS*HN	SC
19	IF(HN .EQ. 0.) GO TO 230	SC
20	30 IF(N .LE. 1) GO TO 230	SC
21	ITS = 0	SC
22	NA = N-1	SC
23	NM2 = N-2	SC
24	40 DO 50 LL=2,N	SC
25	L = N-LL+2	SC
26	IF(DABS(H(L,L-1)) .LE. TEST) GO TO 60	SC
27	50 CONTINUE	SC
28	L = 1	SC
29	GO TO 70	SC
30	60 H(L,L-1) = 0.	SC
31	70 IF(L .LT. NA) GO TO 72	SC
32	N = L-1	SC
33	GO TO 30	SC
34	72 X = H(N,N)/HN	SC
35	Y = H(NA,NA)/HN	SC
36	R = (H(N,NA)/HN)*(H(NA,N)/HN)	SC
37	IF(ITS .LT. 30) GO TO 75	SC
38	FAIL = N	SC
39	RETURN	SC
40	75 IF(ITS.EQ.10 .OR. ITS.EQ.20) GO TO 80	SC
41	S = X + Y	SC
42	Y = X*Y - R	SC
43	GO TO 90	SC
44	80 Y = (DABS(H(N,NA)) + DABS(H(NA,NM2)))/HN	SC
45	S = 1.5*Y	SC
46	Y = Y**2	SC
47	90 ITS = ITS + 1	SC
48	DO 100 MM=L,NM2	SC
49	M = NM2-MM+L	SC
50	X = H(M,M)/HN	SC
51	R = H(M+1,M)/HN	SC
52	Z = H(M+1,M+1)/HN	SC
53	P = X*(X-S) + Y + R*(H(M,M+1)/HN)	SC
54	Q = R*(X+Z-S)	SC
55	R = R*(H(M+2,M+1)/HN)	SC
56	W = DABS(P) + DABS(Q) + DABS(R)	SC
57	P = P/W	SC
58	Q = Q/W	SC
59	R = R/W	SC
60	IF(M .EQ. L) GO TO 110	SC
61	IF(DABS(H(M,M-1))*(DABS(Q)+DABS(R)) .LE. DABS(P)*TEST)	SC
62	GO TO 110	SC

63	100	CONTINUE	SCH00
64	110	M2 = M+2	SCH00
65		M3 = M+3	SCH00
66		DO 120 I=M2,N	SCH00
67		H(I,I-2) = 0.	SCH00
68	120	CONTINUE	SCH00
69		IF(M3 .GT. N) GO TO 140	SCH00
70		DO 130 I=M3,N	SCH00
71		H(I,I-3) = 0.	SCH00
72	130	CONTINUE	SCH00
73	140	DO 220 K=M,NA	SCH00
74		LAST = K.EQ.NA	SCH00
75		IF(K .EQ. M) GO TO 150	SCH00
76		P = H(K,K-1)	SCH00
77		Q = H(K+1,K-1)	SCH00
78		R = 0.	SCH00
79		IF(.NOT.LAST) R = H(K+2,K-1)	SCH00
80		X = DABS(P) + DABS(Q) + DABS(R)	SCH00
81		IF(X .EQ. 0.) GO TO 220	SCH00
82		P = P/X	SCH00
83		Q = Q/X	SCH00
84		R = R/X	SCH00
85	150	S = DSQRT(P**2 + Q**2 + R**2)	SCH00
86		IF(P .LT. 0.) S = -S	SCH00
87		IF(K .NE. M) H(K,K-1) = -S*X	SCH00
88		IF(K.EQ.M .AND. L.NE.M) H(K,K-1) = -H(K,K-1)	SCH00
89		P = P + S	SCH00
90		X = P/S	SCH00
91		Y = Q/S	SCH00
92		Z = R/S	SCH00
93		Q = Q/P	SCH00
94		R = R/P	SCH00
95		DO 170 J=K,NN	SCH00
96		P = H(K,J) + Q*H(K+1,J)	SCH00
97		IF(LAST) GO TO 160	SCH00
98		P = P + R*H(K+2,J)	SCH00
99		H(K+2,J) = H(K+2,J) - P*Z	SCH01
100	160	H(K+1,J) = H(K+1,J) - P*Y	SCH01
101		H(K,J) = H(K,J) - P*X	SCH01
102	170	CONTINUE	SCH01
103		J = MIN0(K+3,N)	SCH01
104		DO 190 I=1,J	SCH01
105		P = X*H(I,K) + Y*H(I,K+1)	SCH01
106		IF(LAST) GO TO 180	SCH01
107		P = P + Z*H(I,K+2)	SCH01
108		H(I,K+2) = H(I,K+2) - P*R	SCH01
109	180	H(I,K+1) = H(I,K+1) - P*Q	SCH01
110		H(I,K) = H(I,K) - P	SCH01
111	190	CONTINUE	SCH01
112		DO 210 I=1,NN	SCH01
113		P = X*U(I,K) + Y*U(I,K+1)	SCH01
114		IF(LAST) GO TO 200	SCH01
115		P = P + Z*U(I,K+2)	SCH01
116		U(I,K+2) = U(I,K+2) - P*R	SCH01
117	200	U(I,K+1) = U(I,K+1) - P*Q	SCH01
118		U(I,K) = U(I,K) - P	SCH01
119	210	CONTINUE	SCH01
120	220	CONTINUE	SCH01
121		GO TO 40	SCH01
122	230	FAIL = 0	SCH01
123		RETURN	SCH01
124		END	SCH01



0	SUBROUTINE SYSSLV	SYSO
1	IMPLICIT REAL*8 (A-H,O-Z)	SYSO
2	C	SYSO
3	COMMON/SLVBLK/A(5,5),B(5),N	SYSO
4	REAL*8 MAX	SYSO
5	1 NM1 = N - 1	SYSO
6	N1 = N+1	SYSO
7	C	SYSO
8	C COMPUTE THE LU FACTORIZATION OF A.	SYSO
9	DO 80 K=1,N	SYSO
10	KM1 = K-1	SYSO
11	IF(K.EQ.1) GO TO 20	SYSO
12	DO 10 I=K,N	SYSO
13	DO 10 J=1,KM1	SYSO
14	A(I,K) = A(I,K) - A(I,J)*A(J,K)	SYSO
15	10 CONTINUE	SYSO
16	20 IF(K.EQ.N) GO TO 100	SYSO
17	KP1 = K+1	SYSO
18	MAX = DABS(A(K,K))	SYSO
19	INTR = K	SYSO
20	DO 30 I=KP1,N	SYSO
21	AA = DABS(A(I,K))	SYSO
22	IF(AA .LE. MAX) GO TO 30	SYSO
23	MAX = AA	SYSO
24	INTR = I	SYSO
25	30 CONTINUE	SYSO
26	IF(MAX .EQ. 0.) STOP	SYSO
27	A(N1,K) = INTR	SYSO
28	IF(INTR .EQ. K) GO TO 50	SYSO
29	DO 40 J=1,N	SYSO
30	TEMP = A(K,J)	SYSO
31	A(K,J) = A(INTR,J)	SYSO
32	A(INTR,J) = TEMP	SYSO
33	40 CONTINUE	SYSO
34	50 DO 80 J=KP1,N	SYSO
35	IF(K.EQ.1) GO TO 70	SYSO
36	DO 60 I=1,KM1	SYSO
37	A(K,J) = A(K,J) - A(K,I)*A(I,J)	SYSO
38	60 CONTINUE	SYSO
39	70 A(K,J) = A(K,J)/A(K,K)	SYSO
40	80 CONTINUE	SYSO
41	C	SYSO
42	C INTERCHANGE THE COMPONENTS OF B.	SYSO
43	C	SYSO
44	100 DO 110 J=1,NM1	SYSO
45	INTR = A(N1,J)	SYSO
46	IF(INTR .EQ. J) GO TO 110	SYSO
47	TEMP = B(J)	SYSO
48	B(J) = B(INTR)	SYSO
49	B(INTR) = TEMP	SYSO
50	110 CONTINUE	SYSO
51	C	SYSO
52	C SOLVE LX = B.	SYSO
53	C	SYSO
54	200 B(1) = B(1)/A(1,1)	SYSO
55	DO 220 I=2,N	SYSO
56	IM1 = I-1	SYSO
57	DO 210 J=1,IM1	SYSO
58	B(I) = B(I) - A(I,J)*B(J)	SYSO
59	210 CONTINUE	SYSO
60	B(I) = B(I)/A(I,I)	SYSO
61	220 CONTINUE	SYSO
62	C	SYSO

63 C SOLVE UX = B.

64 C

65 300 DO 310 II=1,NM1

66 I = NM1-II+1

67 II = I+1

68 DO 310 J=II,N

69 B(I) = B(I) - A(I,J)\*B(J)

70 310 CONTINUE

71 RETURN

72 END

SYSD

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0	SUBROUTINE GAUSEL (MAX, N, A, NR, B, IERR)			GAU
1	IMPLICIT REAL*8 (A-H,O-Z)			GAU
2 C	FUNCTION	- COMPUTES SOLUTION TO A SET OF SIMULTANEOUS		GAU
3 C		LINEAR EQUATIONS (DOES NOT GIVE PIVOT OR		GAU
4 C		DETERMINANT DATA)		GAU
5 C	USAGE	- CALL GAUSEL (MAX,N,A,NR,B,IERR)		GAU
6 C	PARAMETERS	MAX	- MAXIMUM ROW DIMENSION OF B	GAU
7 C		N	- ORDER OF A	GAU
8 C		A(N,N)	- INPUT MATRIX OF COEFFICIENTS (DESTROYED)	GAU
9 C		NR	- NUMBER OF COLUMNS IN B	GAU
10 C		B(MAX,NR)	- MATRIX OF CONSTANTS (REPLACED BY SOLUTIONS)	GAU
11 C		IERR	- INTEGER ERROR CODE	GAU
12 C			= 0 NORMAL RETURN	GAU
13 C			= 2 INPUT MATRIX IS SINGULAR	GAU
14 C	REQUIRED ROUTINES	- NONE		GAU
15 C				GAU
16 C	SOURCE			GAU
17 C		NASA, LRC, ANALYSIS AND COMPUTATION DIVISION SUBPROGRAM		GAU
18 C		LIBRARY		GAU
19 C	****			GAU
20		DIMENSION A(N,N),B(MAX,NR)		GAU
21		NM1 = N-1		GAU
22		IF (NM1 .EQ. 0) GO TO 140		GAU
23 C	****			GAU
24 C		FIND LARGEST REMAINING ELEMENT IN I-TH COLUMN FOR PIVOT		GAU
25 C	****			GAU
26		DO 100 I=1,NM1		GAU
27		BIG = 0.		GAU
28		DO 20 K=I,N		GAU
29		TERM = DABS(A(K,I))		GAU
30		IF (TERM - BIG) 20,20,10		GAU
31	10	BIG = TERM		GAU
32		L = K		GAU
33	20	CONTINUE		GAU
34		IF (BIG) 40,30,40		GAU
35	30	IERR = 2		GAU
36		RETURN		GAU
37	40	IF (I=L) 50,80,50		GAU
38 C	****			GAU
39 C		PIVOT ROWS OF A AND B		GAU
40 C	****			GAU
41	50	CONTINUE		GAU
42		DO 60 J=1,N		GAU
43		TEMP = A(I,J)		GAU
44		A(I,J) = A(L,J)		GAU
45		A(L,J) = TEMP		GAU
46	60	CONTINUE		GAU
47		DO 70 J=1,NR		GAU
48		TEMP = B(I,J)		GAU
49		B(I,J) = B(L,J)		GAU
50		B(L,J) = TEMP		GAU
51	70	CONTINUE		GAU
52	80	CONTINUE		GAU
53 C	****			GAU
54 C		STORE PIVOT AND PERFORM COLUMN OPERATIONS ON A AND B		GAU
55 C	****			GAU
56		IP1 = I+1		GAU
57		DO 100 II=IP1,N		GAU
58		A(II,I) = A(II,I)/A(I,I)		GAU
59		X3 = A(II,I)		GAU
60		DO 90 K=IP1,N		GAU
61		A(II,K) = A(II,K) - X3*A(I,K)		GAU
62	90	CONTINUE		GAU

63	DO 100 K=1,NR	GAU0
64	B(II,K) = B(II,K) - X3*B(I,K)	GAU0
65	100 CONTINUE	GAU0
66	C ****	GAU0
67	C PERFORM BACK SUBSTITUTION	GAU0
68	C ****	GAU0
69	DO 110 IC=1,NR	GAU0
70	B(N,IC) = B(N,IC)/A(N,N)	GAU0
71	110 CONTINUE	GAU0
72	DO 130 KK=1,NM1	GAU0
73	I = N-KK	GAU0
74	IP1 = I+1	GAU0
75	DO 130 J=1,NR	GAU0
76	SUM = B(I,J)	GAU0
77	DO 120 K=IP1,N	GAU0
78	SUM = SUM - A(I,K)*B(K,J)	GAU0
79	120 CONTINUE	GAU0
80	B(I,J) = SUM/A(I,I)	GAU0
81	130 CONTINUE	GAU0
82	RETURN	GAU0
83	140 CONTINUE	GAU0
84	IF (A(1,1) .EQ. 0.) GO TO 300	GAU0
85	DO 150 J=1,NR	GAU0
86	B(1,J) = B(1,J)/A(1,1)	GAU0
87	150 CONTINUE	GAU0
88	RETURN	GAU0
89	300 IERR = 2	GAU0
90	RETURN	GAU0
91	END	GAU0

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0      SUBROUTINE PNCH (A,NA,NAM,IOP)
1 C IOP(1)=0, SKIP TITLE; IOP(2)=N, SKIP LINES; IOP(3)=1, TAB 25 SPACES.
2      IMPLICIT REAL*8 (A-H,O-Z)
3      DIMENSION A(1),IOP(4),NA(2)
4      NR=NA(1)
5      NC=NA(2)
6      NMAX=NR+NC
7      NSKIP=IOP(2)
8      IF (IOP(2).EQ.0) GO TO 205
9      DO 200 I=1,NSKIP
10     200 WRITE(7,150)
11     150 FORMAT(2X)
12     205 CONTINUE
13     IF (IOP(1).EQ.0) GO TO 210
14     WRITE(7,151) NAM,NR,NC
15     151 FORMAT(A4,/,2I5)
16     210 CONTINUE
17     DO 250 I=1,NR
18     IF (IOP(3).EQ.0) WRITE(7,152) (A(J),J=I,NMAX,NR)
19     IF (IOP(3).NE.0) WRITE(7,153) (A(J),J=I,NMAX,NR)
20     250 CONTINUE
21     152 FORMAT(6(1PD13.5))
22     153 FORMAT(25X,6(1PD13.5))
23     RETURN
24     END

```

0	FUNCTION DIMAG(Z)	DIMC
1	REAL*8 A(2),DIMAG	DIMC
2	COMPLEX*16 Z,B	DIMC
3	EQUIVALENCE (A,B)	DIMC
4	B=Z	DIMC
5	DIMAG=A(2)	DIMC
6	RETURN	DIMC
7	END	DIMC

0	FUNCTION DREAL(Z)	DRE00
1	REAL*8 A(2),DREAL	DRE00
2	COMPLEX*16 Z,B	DRE00
3	EQUIVALENCE (A,B)	DRE00
4	B*Z	DRE00
5	DREAL=A(1)	DRE00
6	RETURN	DRE00
7	END	DRE00

0	BLOCK DATA	MOD000
1	IMPLICIT REAL*4 (A-H,O-Z)	MOD000
2	COMMON/LINES/TITLE(10),TIL(3),NLP,LIN	MOD000
3	COMMON/FORM/FMT1(2),FMT2(2),NEPR	MOD000
4	COMMON/TOL/EPHAM,EPSEM,IACM	MOD000
5	COMMON/CONV/SUMCV,RICTCV,SERCV,MAXSUM	MOD000
6	DATA LIN,NLP/1,58/	MOD000
7	DATA NEPR,FMT1/7,8H(1P7D16.,8H7) /	MOD000
8	DATA TIL/AM ORA,8HCLS PRO,8HGRAM /	MOD000
9	DATA FMT2/8H(3X,1P7D,8H16.7) /	MOD000
10	DATA EPSAM/1.E-10/	MOD000
11	DATA EPSEM/1.E-10/	MOD000
12	DATA IACM/12/	
13	DATA SUMCV/1.E-8/	MOD000
14	DATA RICTCV/1.E-8/	MOD000
15	DATA SERCV/1.E-8/	MOD000
16	DATA MAXSUM/50/	MOD000
17	END	MOD000